

Active Joint Connections

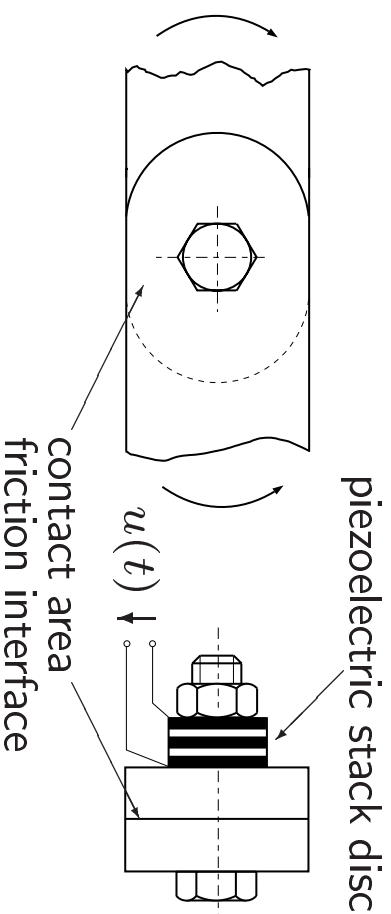
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April 25, 2000

Idea of an Active Joint

Using the normal force as control variable, one obtains a controllable friction moment.

Varying the normal force by means of a piezoelectric stack disc.



Active control theory will be used to vary properties of a passive element!

Applying active control theory to vary the normal force and, thus, the friction force \rightsquigarrow **Semi-Active Friction Damping**.

The idea of the *Active Joint* is patented in
Germany by L. Gaul under *DE 197 02 518*.

LuGre-Friction Model

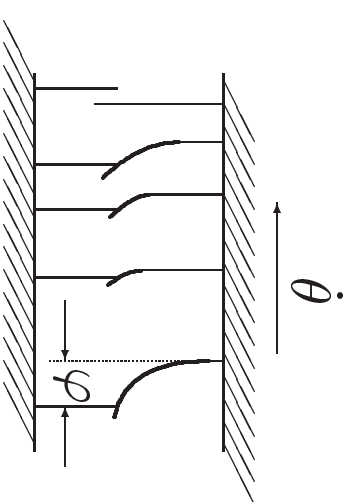
Friction interface is thought of as a contact between bristles.

$$M_f = r \overbrace{F_N}^{\equiv u} (\sigma_0 \varphi + \sigma_1 \dot{\varphi} + \sigma_2 \dot{\theta})$$

$$\equiv: r u \mu(\varphi, \dot{\varphi}, \dot{\theta}),$$

$$\dot{\varphi} = \dot{\theta} - \sigma_0 \frac{|\dot{\theta}|}{g(\dot{\theta})} \varphi$$

$$g(\dot{\theta}) = M_c + M_\Delta \exp\left(-\left(\dot{\theta}/\dot{\theta}_s\right)^2\right)$$



F_N actuator variable

i. e. u

$\dot{\theta}$ relative velocity

φ average deflection of the bristles

σ_i, M_j, v_s, r model parameters

Note: μ represents a kind of a state dependent friction coefficient.

Some Notable Properties of the LuGre-Model

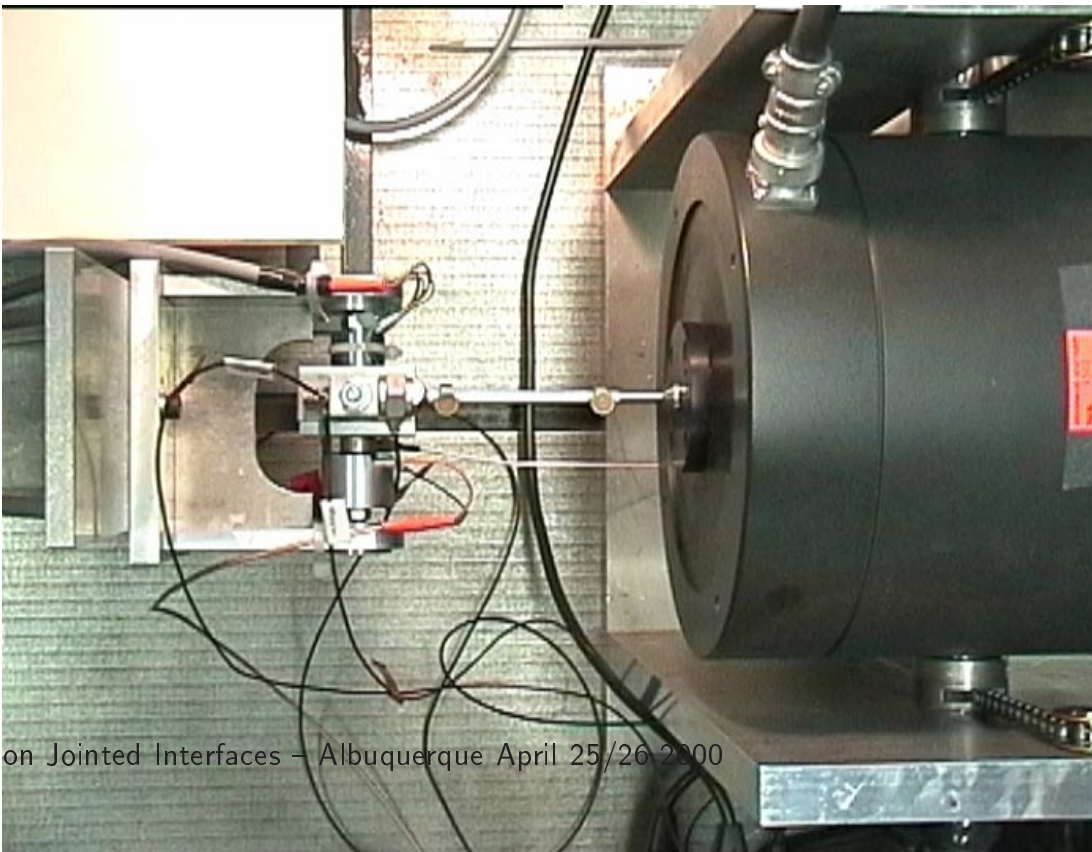
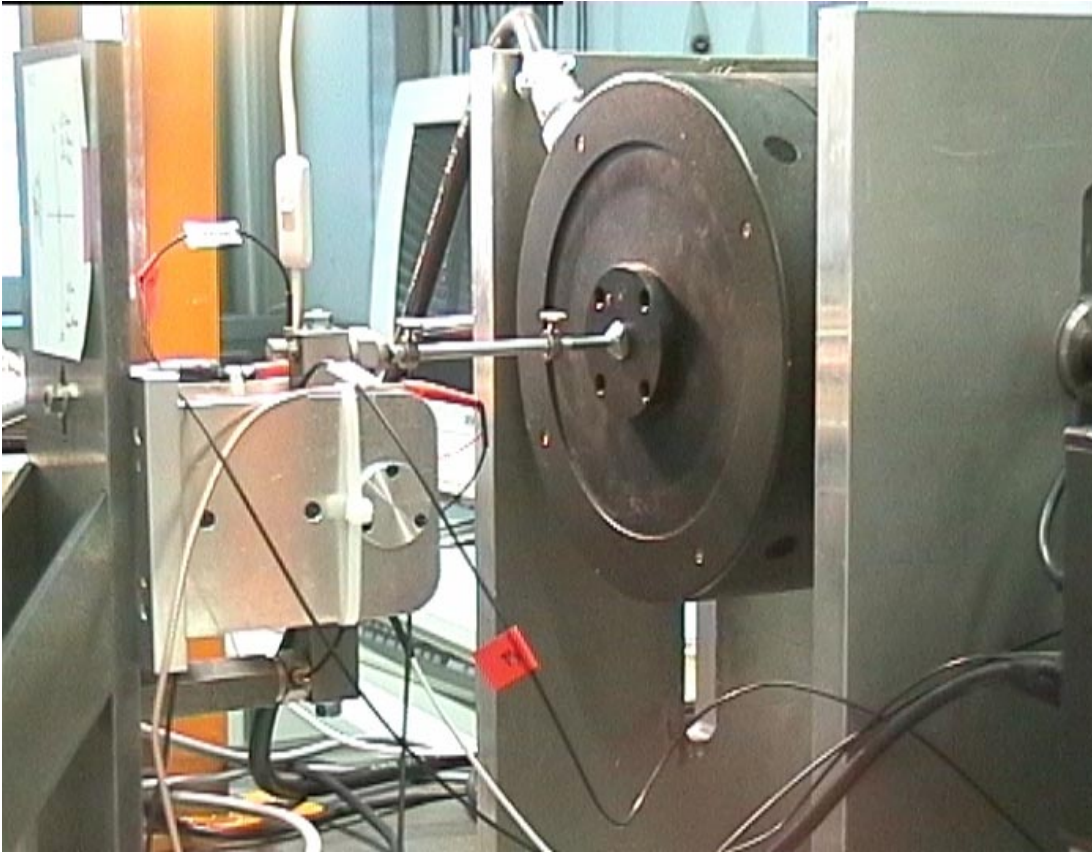
- Static behavior:

$$M_{ss} = \left[M_c + M_\Delta \exp\left(-(\dot{\theta}/\dot{\theta}_s)^2\right) \right] \operatorname{sgn}(\dot{\theta}) + \sigma_2 \dot{\theta}$$

↪ Four static parameters: M_c , M_Δ , $\dot{\theta}_s$, and σ_2 .

- Two dynamic parameters due to the dynamic bristle deflection:
 - ↪ σ_0 (stiffness of the bristles) and σ_1 (damping of the bristles)
- Boundedness of the bristle deflection *i.e.* φ .

Experimental Setup



Active Joint



System Identification

Model Equation

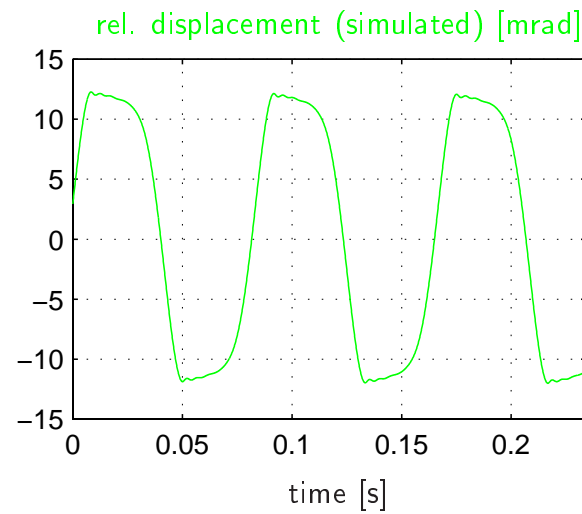
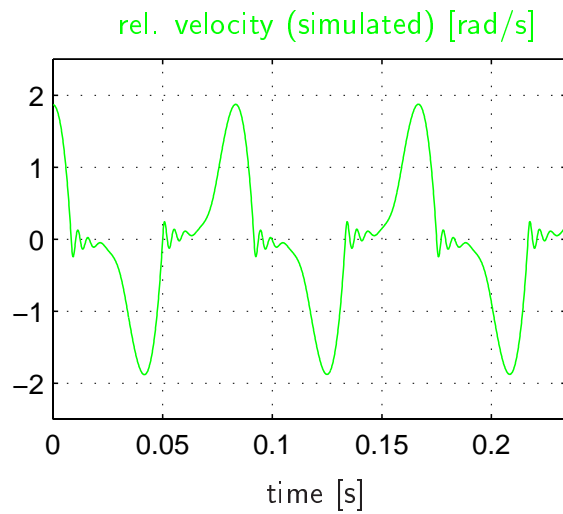
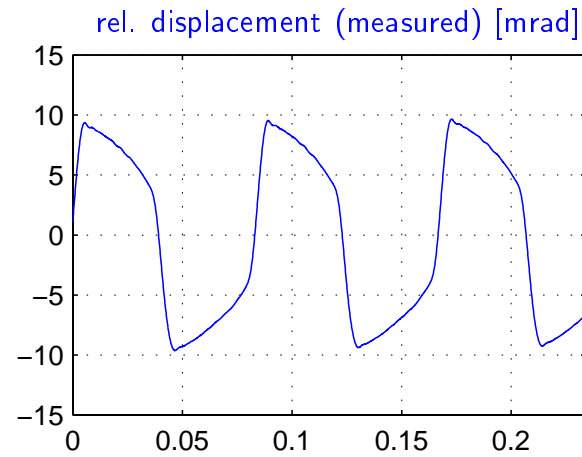
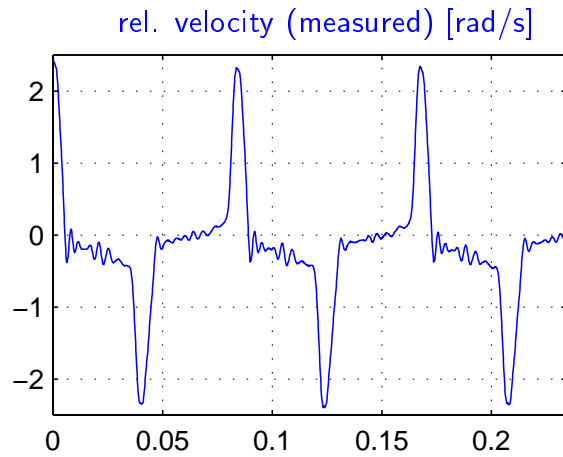
$$J\ddot{\theta} + d\dot{\theta} + c\theta + M_f = \rho f_{\text{ext}}$$

$$M_f = r F_N(\sigma_0\varphi + \sigma_1\dot{\varphi} + \sigma_2\dot{\theta})$$

$$\dot{\varphi} = \dot{\theta} - \sigma_0 \frac{|\dot{\theta}|}{g(\dot{\theta})} \varphi \quad g(\dot{\theta}) = M_c + M_\Delta \exp\left(-\left(\dot{\theta}/\dot{\theta}_s\right)^2\right)$$

- The four *static* parameters: M_c , M_Δ , $\dot{\theta}_s$, and σ_2 are estimated using nonlinear least-square techniques with a minimal normal force in the friction interface of $F_N = 310$ N,
 \rightsquigarrow macro slip.
- The two *dynamic* parameters σ_0 and σ_1 are identified from data when the normal force was at it's maximum, *i.e.* $F_N = 690$ N,
 \rightsquigarrow micro slip.

System Identification



Controller Design

A controller was designed using Lyapunov-technique in order to maximize the energy dissipation due to friction in the joint.

$$V = \frac{1}{2}J\dot{\theta}^2 + \frac{1}{2}c\theta^2 \quad \rightsquigarrow \quad u = -\kappa \frac{dV}{dt}$$

$$W_d = 38.9 \text{ Nm} \cdot \text{mrad}$$

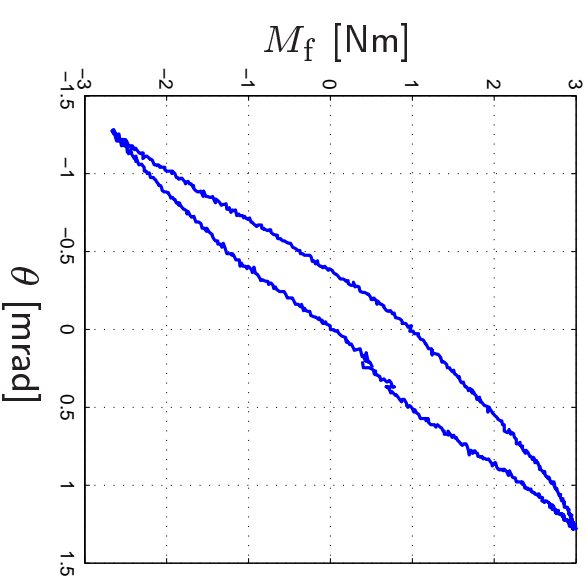
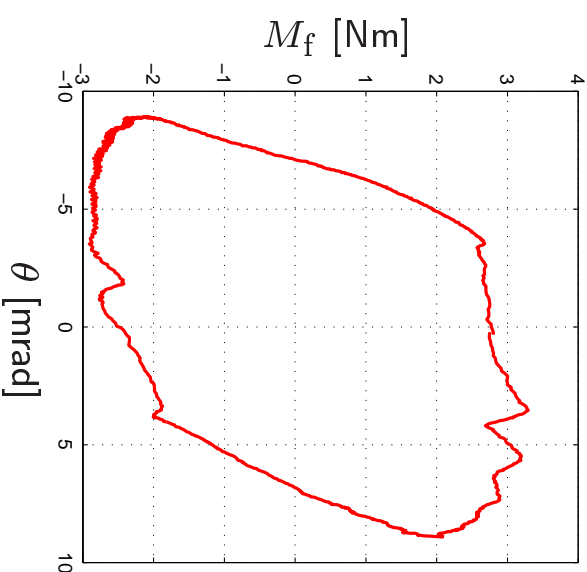
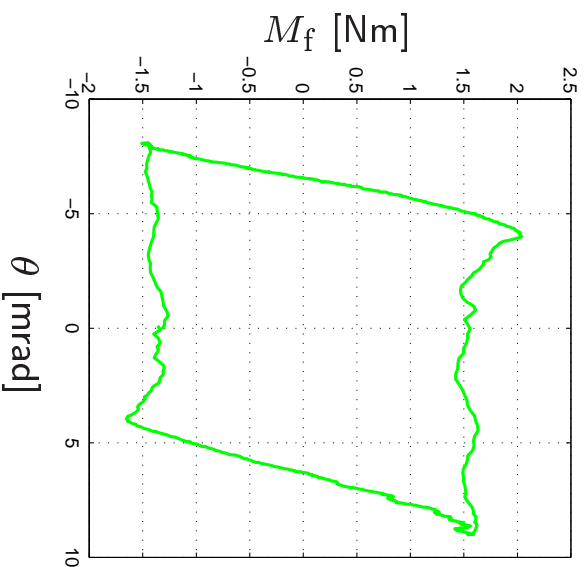
$$W_d = 72.7 \text{ Nm} \cdot \text{mrad}$$

$$W_d = 1.6 \text{ Nm} \cdot \text{mrad}$$

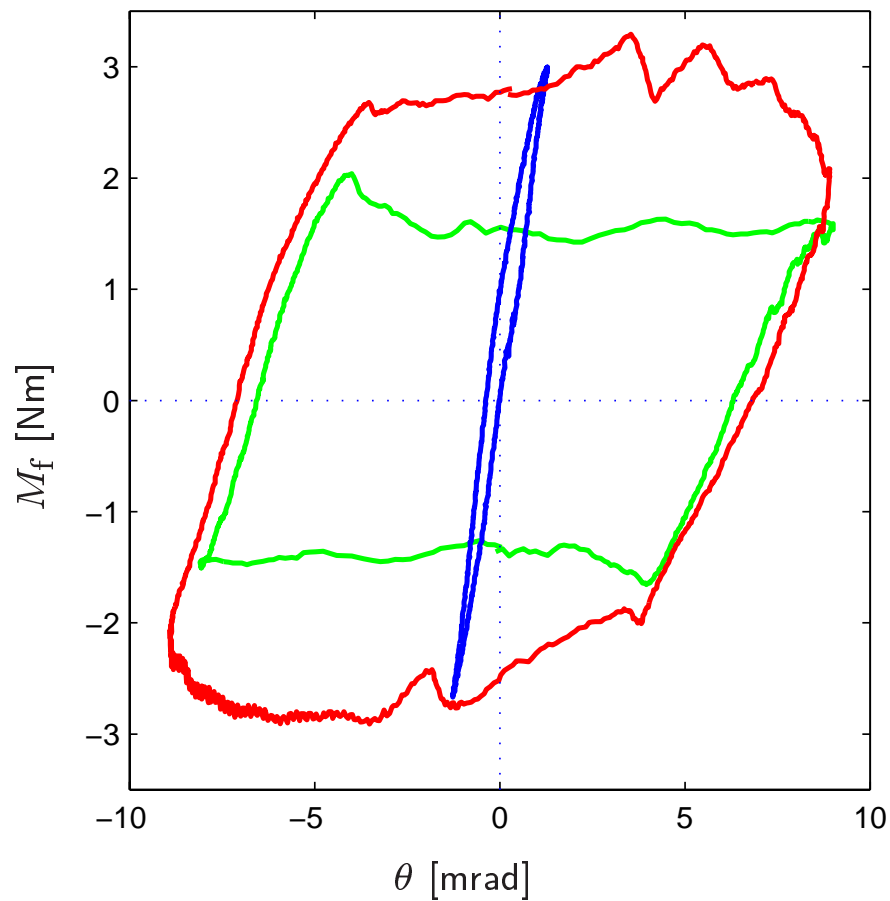
$$F_N = 310 \text{ N}$$

$$F_N = F_N(t)$$

$$F_N = 690 \text{ N}$$



Friction Hysteresis of the Active Joint



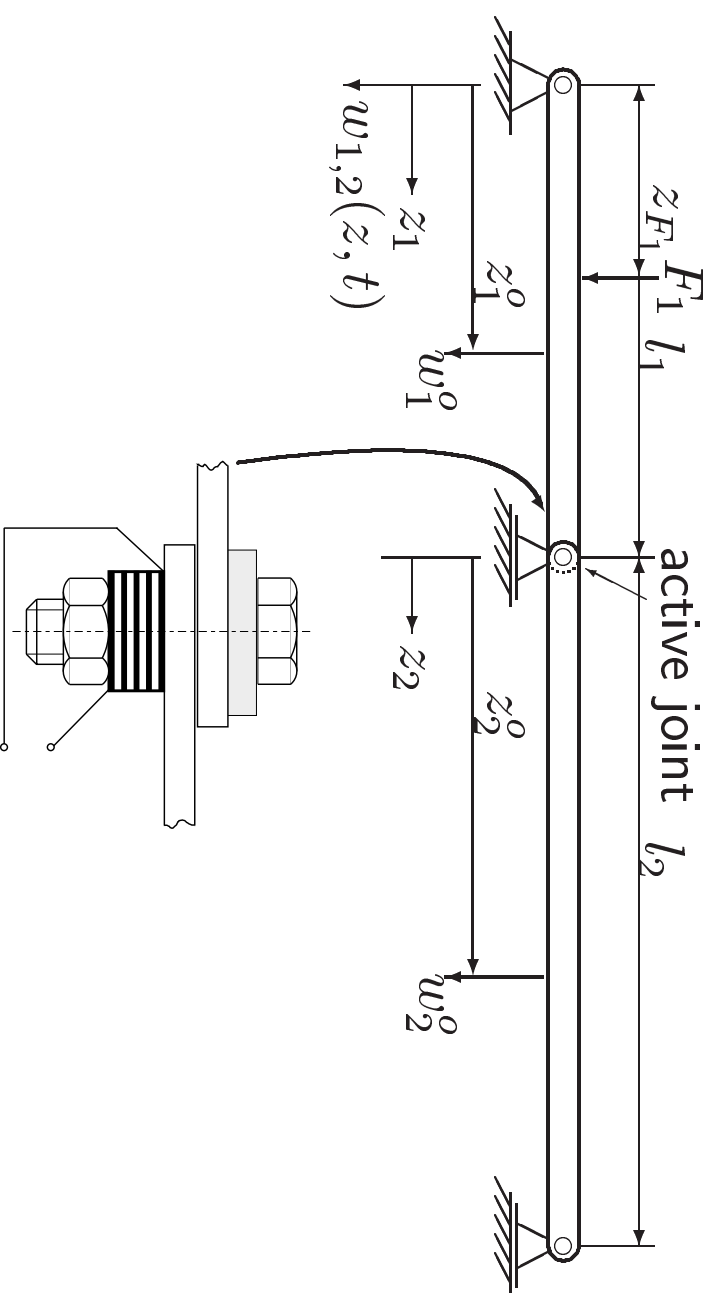
$F_N = 690\text{N}$
 $F_N = 310\text{N}$
 $F_N = F_N(t)$ controlled

Conclusion

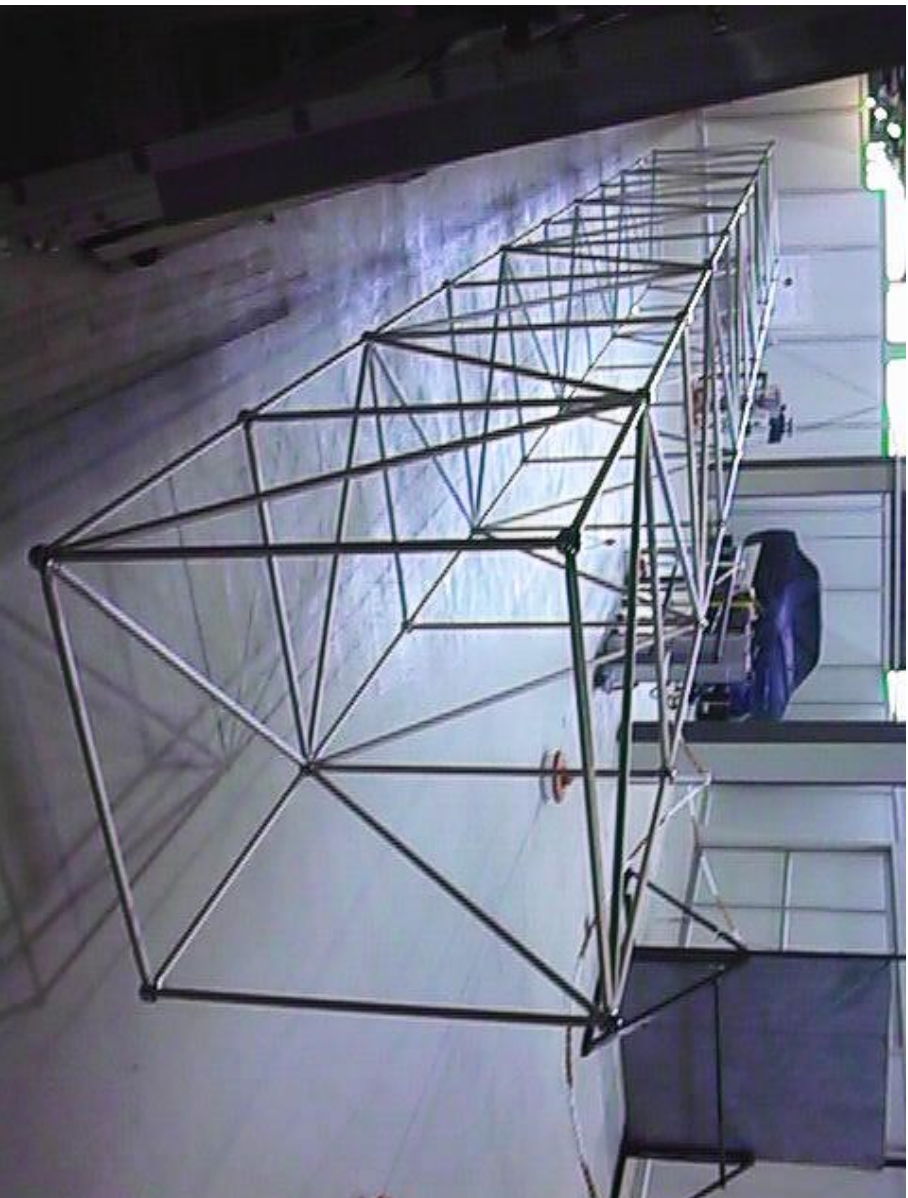
- An active joint was investigated by controlling the normal force in the friction interface: semi-active friction damping.
 - ↪ Loss of complete controllability.
- As energy is always dissipated, there will be no spillover instability caused by the controller.
- Semi-active joints are less massive than fully active damping concepts.
- Numerous joint connections available in LSS.

Future Work

- Experimental evaluation of the active joint connection in a simple flexible structure (Two Beam Structure).



- **Implementation in a large flexible structure.**



An Active Joint in a Flexible Structure

