

Durability of ITO-MgF₂ Films for Space-Inflatable Polymer Structures

Thomas W. Kerslake Glenn Research Center, Cleveland, Ohio

Deborah L. Waters QSS Group, Inc., Cleveland, Ohio

David A. Schieman Ohio Aerospace Institute, Brook Park, Ohio

Paul D. Hambourger Cleveland State University, Cleveland, Ohio Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA Scientific and Technical Information (STI) Program Office plays a key part in helping NASA maintain this important role.

The NASA STI Program Office is operated by Langley Research Center, the Lead Center for NASA's scientific and technical information. The NASA STI Program Office provides access to the NASA STI Database, the largest collection of aeronautical and space science STI in the world. The Program Office is also NASA's institutional mechanism for disseminating the results of its research and development activities. These results are published by NASA in the NASA STI Report Series, which includes the following report types:

- TECHNICAL PUBLICATION. Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA's counterpart of peerreviewed formal professional papers but has less stringent limitations on manuscript length and extent of graphic presentations.
- TECHNICAL MEMORANDUM. Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- CONTRACTOR REPORT. Scientific and technical findings by NASA-sponsored contractors and grantees.

- CONFERENCE PUBLICATION. Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or cosponsored by NASA.
- SPECIAL PUBLICATION. Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- TECHNICAL TRANSLATION. Englishlanguage translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services that complement the STI Program Office's diverse offerings include creating custom thesauri, building customized databases, organizing and publishing research results . . . even providing videos.

For more information about the NASA STI Program Office, see the following:

- Access the NASA STI Program Home Page at *http://www.sti.nasa.gov*
- E-mail your question via the Internet to help@sti.nasa.gov
- Fax your question to the NASA Access Help Desk at 301–621–0134
- Telephone the NASA Access Help Desk at 301–621–0390
- Write to: NASA Access Help Desk NASA Center for AeroSpace Information 7121 Standard Drive Hanover, MD 21076



Durability of ITO-MgF₂ Films for Space-Inflatable Polymer Structures

Thomas W. Kerslake Glenn Research Center, Cleveland, Ohio

Deborah L. Waters QSS Group, Inc., Cleveland, Ohio

David A. Schieman Ohio Aerospace Institute, Brook Park, Ohio

Paul D. Hambourger Cleveland State University, Cleveland, Ohio

Prepared for the First International Energy Conversion Engineering Conference cosponsored by the American Institute of Aeronautics and Astronautics (AIAA), the American Society of Mechanical Engineers (ASME), and the Institute of Electrical and Electronics Engineers (IEEE) Portsmouth, Virginia, August 17–21, 2003

National Aeronautics and Space Administration

Glenn Research Center

Acknowledgments

The authors wish to acknowledge Bruce Banks and Sharon Miller of NASA Glenn Research Center for their technical expertise and counsel regarding thin film deposition and characterization. Cleveland State University work supported by NASA Cooperative Agreements NCC3–740, NCC3–1023, and NCC3–1033.

This report is a formal draft or working paper, intended to solicit comments and ideas from a technical peer group.

This report contains preliminary findings, subject to revision as analysis proceeds.

Trade names or manufacturers' names are used in this report for identification only. This usage does not constitute an official endorsement, either expressed or implied, by the National Aeronautics and Space Administration.

Note that at the time of printing, the NASA Lewis Research Center was undergoing a name change to the NASA John H. Glenn Research Center at Lewis Field. Both names appear in these proceedings.

Available from

NASA Center for Aerospace Information 7121 Standard Drive Hanover, MD 21076 National Technical Information Service 5285 Port Royal Road Springfield, VA 22100

Available electronically at http://gltrs.grc.nasa.gov

DURABILITY OF ITO-MgF₂ FILMS FOR SPACE-INFLATABLE POLYMER STRUCTURES

Thomas W. Kerslake National Aeronautics and Space Administration Glenn Research Center Cleveland, Ohio 44135

> Deborah L. Waters QSS Group, Inc. Cleveland, Ohio 44135

David A. Scheiman Ohio Aerospace Institute Brook Park, Ohio 44142

Paul D. Hambourger Cleveland State University Cleveland, Ohio 44115

Abstract

This paper presents results from ITO-MgF₂ film durability evaluations that included tape peel, fold, thermal cycle and AO exposure testing. Polymer coupon preparation is described as well as ITO-MgF₂ film deposition equipment, procedures and film characterization. Durability testing methods are also described. The pre- and post-test condition of the films is assessed visually, microscopically and electrically. Results show that at ~500Å ITO - 9 vol% MgF₂ film is suitable to protect polymer surfaces, such as those used in space-inflatable structures of the PowerSphere microsatellite concept, during a 1-year Earth orbiting mission. Future plans for ground-based and orbital testing of this film are also discussed.

Introduction

An increasing number of NASA missions will benefit from constellations of microsatellites (or microsats) to obtain broad-area, contemporaneous measurements. These multi-kilogram class microsats tend to be power poor due to limited spacecraft surface area to body-mount photovoltaic cells. At the same time, tracking planar solar array systems are mass prohibitive for this class of microsat. An elegant solution to this power pinch challenge is the PowerSphere (Lin, et al., 2003 and Simburger, et al., 2002) concept shown in Figure 1. The PowerSphere space-inflatable, geodetic solar array provides attitudeindependent microsat power with very low mass and efficient launch packaging to enable microsat constellation deployment from a single carrier spacecraft. Once inflated, an ultraviolet (UV) activated

resin impregnated in PowerSphere central columns and cylindrical solar cell connecting hinges is rigidized by exposure to sunlight and Earth albedo. These inflatable/rigidizable columns and hinges as well as thin-film solar cell substrates and encapsulants are all constructed of polymer materials. During operation in Earth orbit, virgin polymer surfaces could charge to high voltage leading to damaging electrostatic discharge (ESD). In addition, the presence of atomic oxygen (AO) in low Earth orbits leads to aggressive attack of unprotected polymers.



Figure 1. PowerSphere Concept

To address these design challenges, PowerSphere polymer surfaces will be coated with a thin protective film. This film must have suitable electrical sheet resistivity for ESD control, be transparent to UV and solar radiation, for photovoltaic cell operation and UV resin curing, in addition to being AO resistant. The film material selected is a co-sputtered, 91% indium oxide (In₂O₃) – 9% tin oxide (SnO₂) [a.k.a., ITO] and magnesium fluoride (MgF₂) (Dever, et al., 1996). The volume percentage of MgF₂ (typically 0-30%) can be chosen to achieve the desired sheet resistivity ($10^{8}\Omega/\Box$) and maximize film transmittance. The properties of these films have been the subject of research over the last decade, although the durability of this film for space-inflatable applications has not been addressed.

This paper presents results from film durability evaluations that included tape peel, fold, thermal cycle and AO exposure testing. In the following sections, polymer coupon preparation is described as well as $ITO-MgF_2$ film deposition equipment, procedures and film characterization. Durability testing methods and results are also discussed.

Coupon Preparation

Coupon Substrates

Two materials were coated with the ITO-MgF₂ films, both Mylar[®] and a Tefzel[®]-encapsulated amorphous silicon (a-Si) solar cell on Upilex[®] as shown in Figure 2. The 0.001 in. Mylar[®] samples were cut into 2 by 2 in. squares. Prior to deposition, two copper areas were deposited onto the surface for resistivity measurements. The 2 by 2 in. solar cell was cut in half in order to expose both sides for coating.

The target film thickness for the two depositions was 250 Angstroms and 500 Angstroms. For each deposition, two Mylar[®] samples were coated for testing. Tables 1 and 2 illustrate the sample nomenclature and applicable test plan, respectively.

Coupon	Material	Side	ITO-MgF ₂
ID		Exposed	Thickness
			(Å)
1m250p	Mylar®	Front	250
1m500p			500
2m250	Mylar®	Front	250
2m500			500
3au250	Upilex [®] /a-Si	Front	250
3au500	/Tefzel [®]		500
3bu250	Upilex [®] /a-	Back	250
3bu500	Si/ Tefzel [®]		500

Table 1. Coupon Summary

Coupon	Peel	Fold	AO Test	Thermal
ID	Test	Test		Cycling
1m250p	Yes	Yes	Yes	No
1m500p				
2m250	No	Yes	No	Yes
2m500				
3au250	Yes	No	No	Yes
3au500				
3bu250	Yes	No	No	Yes
3bu500				

Table 2. Coupon Tests

Film Deposition

An Ion Tech Dual Beam Facility was used to deposit the coatings. This facility uses two ion sources to clean the target, clean the substrate for enhanced adhesion and to carry out the deposition without breaking vacuum. The facility was run on argon as the feed gas in a background of air for more complete oxidation. The pressure during the depositions was less than 4.0E-4 Torr.

In order to obtain a mixed target, the individual deposition rates had to be determined for the ITO target and the MgF₂ target independently. Once the individual rates were determined, an aluminized piece of Kapton[®] was used to determine the beam center. Knowing the individual rates and the beam center, the 9 vol% MgF₂ required composition could be translated into angled wedges sitting on top of the ITO target. The mixed target was verified to give the proper deposition rate prior to coating the samples. The sample coupons were then coated in two subsequent depositions.

Film Composition & Characterization

The coating composition was based on calculations yielding 91 vol% ITO - 9 vol% MgF₂. A quartz slide masked with Kapton[®] tape was used in all depositions as a witness for thickness determination. The coating thickness was determined using a "Dektak IIA Profilometer" by scanning from the tape protected region of the slide to the coated portion in four places. The target 250Å deposition resulted in 275Å \pm 24Å. The target 500Å deposition resulted in 535Å \pm 37Å.

Durability Test Procedures

During all coupon testing, samples were handled carefully with gloved hands and plastic tweezers to minimize contamination.





(b) Front (Top) and Back (Bottom)

Figure 2. Coupons With Pristine 535Å Films: (a) Mylar[®] and (b) Tefzel[®]-Encapsulated Amorphous Silicon Solar Cell on Upilex[®]

Tape Peel Testing

A paper was placed over half of the coupon area and then a 1-inch length of 1/2-inch wide Kapton[®] tape with 3M-Y9460 "Isotac" adhesive was applied to the coupon (see Figure 3). The tape was hand smoothed with moderate pressure. After waiting approximately 2 minutes, the tape was peeled back at a 180° angle and removed from the coupon in about 2 seconds. This test was to demonstrate good film adherence to the substrate.

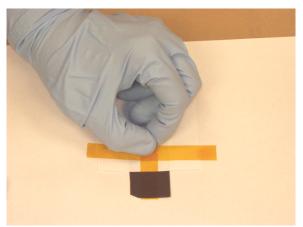


Figure 3. Film Tape Peel Test

Fold Testing

With the film-coated side outward, the Mylar[®] coupons were quarter-folded using tweezers. A block, approximately 2.5 cm by 2.5 cm, was gently placed on the folded coupon and then 6.8 kg of weights were gently placed upon the block to approximate an atmospheric pressure loading of 10^5 N/m² (see Figure 4). After about 2 minutes, the weights and block were removed and the coupon was gently unfolded for inspection. This test simulates pump-down on the PowerSphere center column and subsequent z-fold packaging. Similarly, solar cell inflatable hinges will be flattened for packaging creating single fold lines.



Figure 4. Film Fold Test

Thermal Cycling

After tape peel and fold testing, the film coated coupons were attached to the thermal cycling frame using Kapton[®] tape and mounted in the NASA Glenn Research Center thermal cycling facility (Scheiman, et al., 1990 and Scheiman and Smith, 1992) shown in Figure 5. While cycling, coupons are exposed to an ambient pressure, nitrogen atmosphere (chamber cold side liquid nitrogen boil-off). A single thermocouple was placed on the back of one coupon. The coupons were then cycled 5000 times between hot and cold chambers based on a measured hot temperature of 100°C and cold temperature of -128°C. About 250 thermal cycles were achieved per test day. 5000 thermal cycles is representative of 1-year of operation in low Earth orbit (LEO).

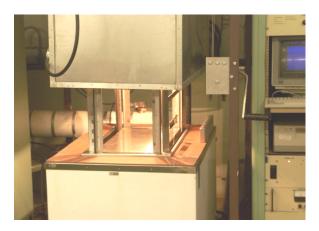


Figure 5. Thermal Cycle Chamber With Solar Cell Test Frame (Right), Hot Chamber (Top) and Cold Chamber (Bottom)

Atomic Oxygen Exposure

After fold testing, 2 Mylar[®] coupons, with film thicknesses of 275Å and 535Å, were placed in an SPI Plasma PrepTM II Etcher, a.k.a. "asher", which produces a plasma and atomic oxygen (AO) neutrals by radiofrequency excitation. The film coated coupons and a circular, bare Kapton-H[®] witness coupon were placed film side up on a glass plate and held flat by an openwire frame placed on top of the coupons (see Figure 6). The planned AO fluence was 1.66E21 atoms/cm² which



Figure 6. Atomic Oxygen Coupon Film Testing

simulates 1-year of exposure in LEO for a ram surface. To gage accumulated AO fluence, the Kapton-H[®] witness coupon, with a known AO erosion rate, was periodically removed from the asher and weighed.

Coupon Inspection Methods

The ITO-MgF₂ films were visually inspected, photographed and microscopically examined before and after durability testing. For the Mylar[®] coupons, film sheet resistivity was measured before and after fold testing (Cashman, et al., 2002). Mylar[®] coupon mass was measured before film AO durability testing.

Results and Discussion

Tape Peel Testing

Based on visual and microscopic examination of the Mylar[®] and a-Si solar cell coupons, the appearance of the both 275Å and 535Å ITO-MgF₂ films was unaffected by the tape peel test. The films appeared totally normal and undamaged. A typical photomicrograph of the 535Å ITO-MgF₂ film on Tefzel[®] is shown in Figure 7. Based on this finding, film sheet resistivity measurements were not obtained. The results indicate these sputtered films are generally robust and tenacious for the Mylar[®], Tefzel[®] and Upilex[®] polymer substrates.

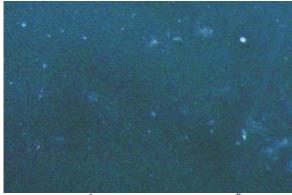


Figure 7. 535Å ITO-MgF₂ film on Tefzel[®] at 40X Magnification

Fold Testing

Based on visual inspection of the 275Å and 535Å thickness films along the single and double fold lines, the films appeared unaffected as a result of folding. Figure 8 shows a folded Mylar[®] coupon with 535Å ITO-MgF₂ film thickness.

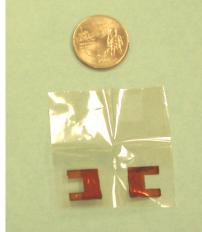


Figure 8. Folded Mylar[®] Coupon

Under magnifications of 15X, 40X, 80X, and 128X, no generalized film damage along fold lines was evident. Out of 4 coupons examined, only 2 isolated sites of film cracking were detected. Figure 9 shows a typical photomicrograph of the double fold region of a 535Å thick ITO-MgF₂ film on Mylar[®].

Thus, based on visual and microscopic inspections, the film appeared to be undamaged after fold testing. Film sheet resistivity measurements were then made. Prior to fold testing, the dark-stabilized, ambient, film sheet resistivity was measured at $10^{10} \Omega/\Box$ for 275Å

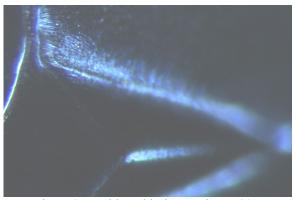


Figure 9. Double Fold Line Region at 80X Magnification; 535Å ITO-MgF₂ Film on Mylar[®]

films and $10^{06}~\Omega/\square$ for 535Å films. After fold testing, film sheet resistances for all films were insulating (a resistivity $>10^{13} \Omega/\Box$). This indicated that the films were substantially damaged (cracked) along the fold lines. Prior work (Banks et al., 1985) with a 500Å SiO2 film on Kapton[®] showed that about 2% strain in the film could be tolerated prior to brittle fracture. This strain level corresponded to a 3 mm bend radius. Although not measured, the bend radius of folded Mylar[®] coupons is likely much smaller resulting in excessively large film strains. Further testing is planned with a representative center column lay-up of materials, including ITO-MgF₂ coated Kynar-740 and typical z-folding. Under these conditions, a much larger bend radius is expected which should introduce much lower strain levels in the film and less film cracking. To ensure the proper ESD protection function of the ITO-MgF₂ film, a thin layer of copper (with high strain tolerance) will be deposited across fold lines to ensure electrical continuity of any isolated film segments. Since the film stays resident along fold lines, partial AO protection is afforded from a cracked film along a fold line. A more detailed discussion is given in the Atomic Oxygen Exposure section below.

Thermal Cycling

Based on visual and microscopic examination of the Mylar[®] and a-Si solar cell coupons, the appearance of both 275Å and 535Å ITO-MgF₂ films was unaffected by exposure to the 5000 thermal cycles. This finding held true for film virgin areas, film peel tested areas and along film fold lines. The films appeared totally normal and undamaged. Based on this finding, film sheet resistivity measurements were not obtained. These results indicate that these films, on Mylar[®], Tefzel[®] and

Upilex[®] polymer substrates, are robust and tenacious for at least 1-year in a LEO thermal cycling environment.

Atomic Oxygen Exposure

The folded Mylar[®] coupons were removed from the plasma asher after an accumulated AO fluence of only 0.66E21 atoms/cm² (0.4 years ram exposure in LEO). At this point, the coupons were obviously damaged. To the unaided eye, the coupon films appeared frosted (see Figure 10 below compared to pre-AO exposure in Figure 8) and have reduced mass and stiffness (more pronounced in coupon with 275Å ITO-MgF₂ film). The outward facing fold line substrate material was substantially severed with the 275Å film thickness and only partially severed on the coupon with the 535Å ITO-MgF₂ film. Uncoated Mylar[®] (area masked to keep the copper pad fingers pristine for electrical test purposes) was completely eroded away in both coupons. As a result of this unprotected material loss, meaningful coupon mass change measurements could not be made. Photomicrographs revealed the 275Å ITO-MgF₂ film on the copper pads was unaffected as a result of AO exposure. This film on Mylar[®], however, was found to exhibit generalized within film cracking and occasional pin hole defects and large, through film cracks near fold lines (see Figure 11).



Figure 10. Mylar[®] Coupon With 535Å ITO-MgF₂ Film Following AO Exposure

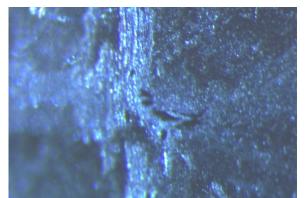


Figure 11. : 128X Magnification Photomicrograph of Mylar[®] Coupon Double Fold Line With 275Å ITO-MgF₂ Film Following AO Exposure

A similar frosty film appearance was obtained with the 535Å ITO-MgF₂ film coupon as shown in Figure 12 below (compare to pre-AO exposure condition shown in Figures 7 and 9). The cause for this frosty appearance is likely from the AO penetrating small film cracks, previously not visible, and attacking the Mylar[®] substrate. The resulting Mylar[®] cavity formed under the crack then scatters the light leading to the frosted appearance. Larger cracks allow the AO to completely erode away the local underlying Mylar[®] and thus create the appearance of black regions such as the dark pin hole defect in Figure 11. In this case, the Mylar[®] can no longer support the ITO-MgF₂ film and it collapses,

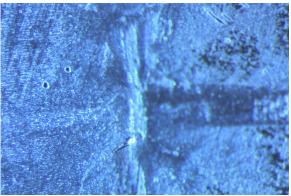


Figure 12. : 40X Magnification Photomicrograph of Mylar[®] Coupon Double Fold Line With 535Å ITO-MgF₂ Film Following AO Exposure

opening up the defect site for further undercutting AO attack of the Mylar[®] substrate. The source of the initial film cracks is likely the combination of fold test block compression forces and fold test handling with tweezers.

These AO exposure tests indicate the 275Å film thickness is insufficient to protect the Mylar[®] along fold lines. The 535Å film remained largely intact and held up well on the copper pads (important for electrical continuity). Since the polymer films used on the inflatable center columns and solar cell hinges are only required for the first few hours of the mission, during inflatable structure rigidization, AO-induced frosting, and the concomitant changes in optical properties, is Given the more benign handling acceptable. requirements for solar cell films (i.e., no folding or large compressive loads), film cracking and subsequent frosting behavior is less likely than with the inflatable polymer surfaces. Even if some frosting occurs, scattered light will still reach the solar cell so performance should not be greatly reduced. Further AO exposure testing is planned for coupons reflecting the final design, materials and handling procedures for PowerSphere inflatable polymer structures. If required, the film thickness could be doubled to the 1000Å range for enhanced robustness. With twice the film thickness, the resulting loss in film solar transmittance, and hence solar cell current output, was estimated as 12%.

Film Sheet Resistivity Sensitivities

The sheet resistivity of ITO-MgF₂ coatings on Mylar[®] substrates was found to be sensitive to light, age, and film thickness. Following long exposure to ambient room light, the sheet resistivity increased by a factor of ~2 after 20 hours of dark soak and by a factor of ~3 after 70 hours of dark soak. When measured after ~20 hours of dark soak, sheet resistivity increased by a factor of 10-30 in the period 20 to 90 days after deposition. The sheet resistivity also showed substantial thickness dependence; samples ~250 Å thick had dark sheet resistivities ~2x10⁴ times larger than those ~500 Å thick. Qualitatively similar effects have been observed in ITO-MgF₂ films deposited by RF magnetron sputtering (Cashman, et al., 2002).

Concluding Remarks

275Å- and 535Å-thick films of ITO - 9 vol% MgF₂ were co-sputtered on space-inflatable structure polymer materials including Mylar[®], Tefzel[®] and Upilex[®]. The durability of these films was assessed by conducting a regiment of tests including tape peel testing, fold testing, thermal cycle exposure and AO exposure testing. The films were characterized by visual inspection, optical microscopy and electrical sheet resistivity. Tape peel tests and thermal cycle exposure tests demonstrated that the films were tenacious and robust. Fold testing cracked the film along fold lines creating electrically isolated film segments although the film remained intact and apparently undamaged based microscopic inspections. Subsequent AO exposure

produced a frosty appearance in the films presumably due to substrate attack below previously unseen film cracks. Fold lines on coupons with a 275Å thick film were mostly severed and thus it was deemed that this film thickness is insufficient. Although frosted, the 535Å thick film remained largely intact after AO exposure and should be acceptable for the PowerSphere inflatable structure polymer application. Further film durability testing with articles reflecting the final inflatable structure design, materials and handling will be conducted to ensure the performance and robustness of the ITO-MgF2 ESD/AO protective film. If necessary, a more robust 1000Å film thickness could be employed with acceptable solar cell performance impacts.

Future Work

Other ITO-MgF₂ film research is planned or in progress. This work includes film electron, proton and neutron irradiation tests on-going at The Aerospace Corporation. Film electrical and optical properties will be measured before and after the radiation exposures. Also, ITO-MgF₂ films will be deposited on prototypical PowerSphere solar cells with flex harness and included as part of the Materials International Space Station Experiment (MISSE-5) flight experiment to be launched to the International Space Station. After exposure to the LEO environment for a year or more, the MISSE-5 samples will be returned to Earth to allow ITO-MgF₂ film characterization testing. And lastly, research is underway at the Cleveland State University Department of Physics exploring the use of magnetron sputtering emission line spectroscopy for in-situ control of film resistivity.

References

Banks, Bruce A., et al., "Ion Beam Sputter-Deposited Thin Film Coatings for Protection of Spacecraft Polymers in Low Earth Orbit," NASA TM-87051, January 1985.

Cashman, T., et al., "Photoconductivity in Transparent Arcproof Coatings," 6th International Conference–Protection of Materials from Space Environment, Toronto, Canada, May 1-3, 2002.

Dever, Joyce A., et al., "Indium Tin Oxide-Magnesium Fluoride Co-Deposited Films for Spacecraft Applications," International Conference on Metallurgical Coatings and Thin Films, American Vacuum Society, San Diego, CA, April 24-26, 1996.

Lin, John K., et al., "Development, Design and Testing of PowerSphere Multifunctional Ultraviolet-Rigidizable Inflatable Structures," 4th AIAA Gossamer Spacecraft Forum, paper AIAA-2003-1707, Norfolk, VA, April 7-10, 2003. Scheiman, David A., et al., "Rapid Thermal Cycling of New Technology Solar Array Blanket Coupons," 25th Intersociety Energy Conversion Engineering Conference, Volume 1, p. 575-580, August 1990.

Scheiman, David A. and Smith, Bryan K., "Rapid Thermal Cycling of Solar Array Blanket Coupons for Space Station Freedom," ASME Solar Engineering, Volume 2, p. 817-823, April 1992. Simburger, Edward J., et al., "Development of a Multifunctional Inflatable Structure for the PowerSphere Concept," 3rd AIAA Gossamer Spacecraft Forum, paper AIAA-2002-1707, Denver, CO, April 22-25, 2002.

REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.						
1. AGENCY USE ONLY (Leave blank	() 2. REPORT DATE July 2003		3. REPORT TYPE AND DATES COVERED Technical Memorandum			
4. TITLE AND SUBTITLE	I	5	5. FUNDING NUMBERS			
Durability of ITO-MgF ₂ Fr	ilms for Space-Inflatable Polyme	r Structures	WBS-22-757-01-12			
6. AUTHOR(S)			WD3-22-757-01-12			
Thomas W. Kerslake, Debo and Paul D. Hambourger						
			8. PERFORMING ORGANIZATION REPORT NUMBER			
National Aeronautics and S	-					
John H. Glenn Research C Cleveland, Ohio 44135–3		E-14072				
9. SPONSORING/MONITORING AG		ין 	0. SPONSORING/MONITORING AGENCY REPORT NUMBER			
National Aeronautics and S	-		NASA TM-2003-212512			
Washington, DC 20546–0	0001		AIAA-2003-5919			
11. SUPPLEMENTARY NOTES Prepared for the First International Energy Conversion Engineering Conference cosponsored by the American Institute of Aeronautics and Astronautics (AIAA), the American Society of Mechanical Engineers (ASME), and the Institute of Electrical and Electronics Engineers (IEEE), Portsmouth, Virginia, August 17–21, 2003. Thomas W. Kerslake, NASA Glenn Research Center; Deborah L. Waters, QSS Group, Inc., Cleveland, Ohio 44135; David A. Schieman, Ohio Aerospace Institute, Brook Park, Ohio 44142; and Paul D. Hambourger, Cleveland State University, Cleveland, Ohio 44115, supported by NASA Cooperative Agreements NCC3–740, NCC3–1023, and NCC3–1033. Responsible person, Thomas W. Kerslake, organization code 6920, 216–433–5373.						
12a. DISTRIBUTION/AVAILABILITY	STATEMENT	1	2b. DISTRIBUTION CODE			
Unclassified - Unlimited Subject Categories: 18 and	20 Distrib	ution: Nonstandard				
Available electronically at http:	//altre are pasa aoy					
		formation. 301–621–0390.				
	This publication is available from the NASA Center for AeroSpace Information, 301–621–0390. 13. ABSTRACT (<i>Maximum 200 words</i>)					
This paper presents results from ITO-MgF ₂ film durability evaluations that included tape peel, fold, thermal cycle, and AO exposure testing. Polymer coupon preparation is described as well as ITO-MgF ₂ film deposition equipment, procedures and film characterization. Durability testing methods are also described. The pre- and post-test condition of the films is assessed visually, microscopically, and electrically. Results show that at ~500Å ITO - 9 vol% MgF ₂ film is suitable to protect polymer surfaces, such as those used in space-inflatable structures of the PowerSphere microsatellite concept, during a 1-year Earth orbiting mission. Future plans for ground-based and orbital testing of this film are also discussed.						
14. SUBJECT TERMS			15. NUMBER OF PAGES			
Films; Oxide films; Solar arrays; Durability; Polymers; Thermal cycling tests; Earth orbital environments			14 16. PRICE CODE			
17. SECURITY CLASSIFICATION	18. SECURITY CLASSIFICATION	19. SECURITY CLASSIFICAT	ION 20. LIMITATION OF ABSTRACT			
OF REPORT	OF THIS PAGE	OF ABSTRACT				
Unclassified	Unclassified	Unclassified				
NSN 7540-01-280-5500			Standard Form 298 (Rev. 2-89)			