

Steady-State Operation of Fusion Plasmas - the Stellarator Project Wendelstein 7-X

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on behalf of the
enterprise Wendelstein 7-X



steady-state operation:

this is likely to be a requirement in a future FPP

Tokamak steady-state operation is a subject of current research

- $\beta_N \sim 4$ required - achieved only with advanced tokamak scenarios (ITB's)
- Control of pressure profiles, current profiles and instabilities required
- Several 100MW of CD required – efficiency only 20-40% must go up

Stellarators are steady-state „by nature“

- The control issue is much less a problem – only weak CD needed
- Plasma performance not yet satisfactory (esp. τ_E and β)
- Divertor solution and control of impurities required

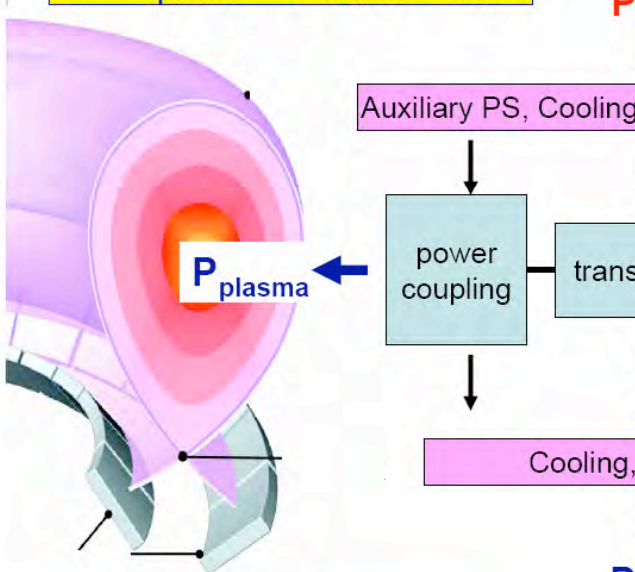
Several technologies must be developed in general

- Superconducting magnets (also HTSCs)
- Steady-state H&CD solutions
- Steady-state capable in-vessel components
- The right materials in general

EFDA
EUROPEAN FUSION DEVELOPMENT AGREEMENT

Current drive efficiency η_{CD} (1/5)

H&CD Wall Plug Efficiency Issues

$$\eta = P_{\text{plasma}} / (P_{\text{source}} + P_{\text{aux}})$$


SOFT 2008, DEMO R&D, J.Pamela

J. Pamela, SOFT 2008
www.soft2008.ipp.mpg.de

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SUMMARY ON DEMO R&D NEEDS

- Fuel cycle:
 - *Test Blanket Module programme on ITER essential*
 - Must be accompanied by R&D on T extraction and a programme aiming at a quasi-industrialized blanket concept
- Materials for in-vessel components:
 - He production by 14 MeV neutrons and structural or functional requirements drive fusion specific R&D
 - High T operation (required to optimise CoE) puts additional requirements on materials
- Heating and Current Drive systems:
 - The needs for R&D in this area have always been dramatically underestimated and under-financed; mistakes of the past should not be repeated.

Significant simplifications and developments required

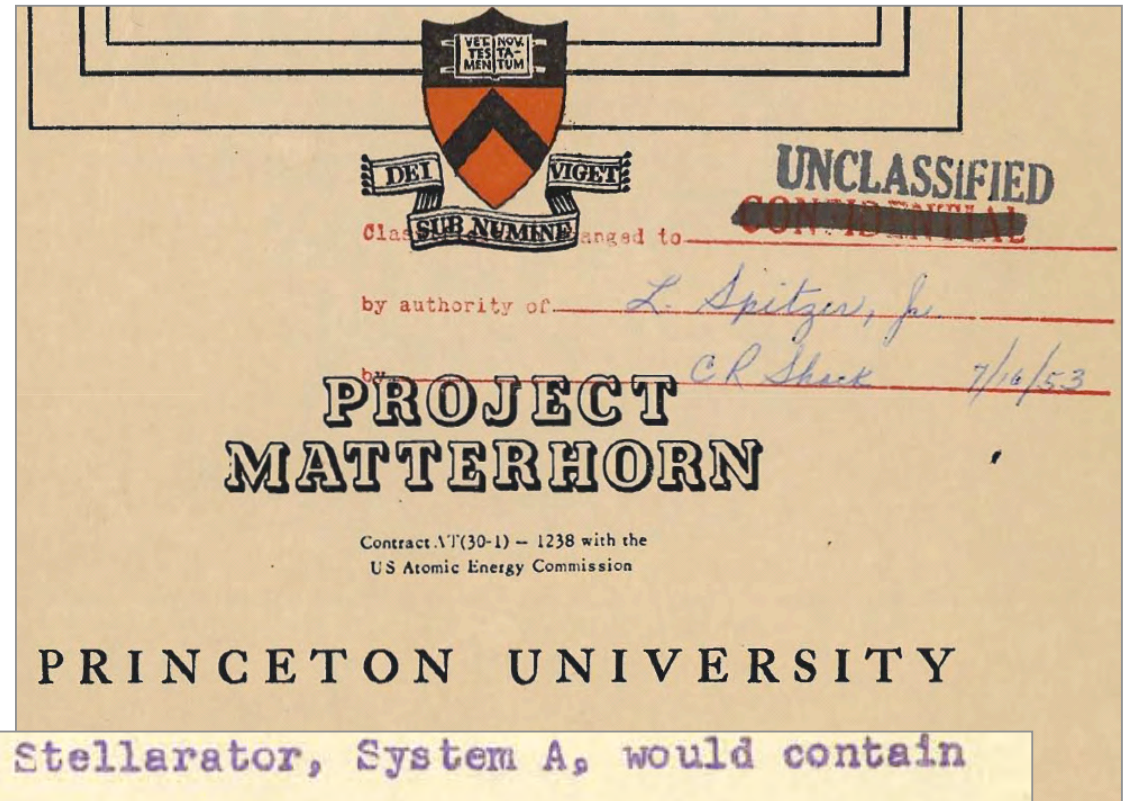
- Overall **efficiency** of H&CD systems (from plug to plasma) has to be increased from 20-30% today to 60-70%
- **Duty cycle** (from 10's of seconds to cw operation; reduced maintenance needs)
- very high **reliability under nuclear operation**

SOFT 2008, DEMO R&D, J.Pamela

- I. Principles**
- II. Island divertor**
- III. Plasma currents**
- IV. Performance**
- V. Construction status**



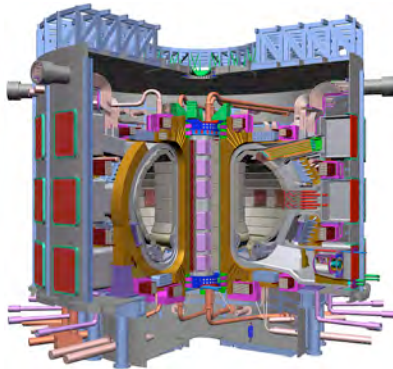
In stellarators
steady state
operation is
taken for granted.



The proposed Stellarator, System A, would contain about 0.03 grams of tritium, and would consume about ten kilograms of tritium a year in steady operation, liberating about 150,000 kilowatts of nuclear power in steady operation. Only a fraction of this power would be available

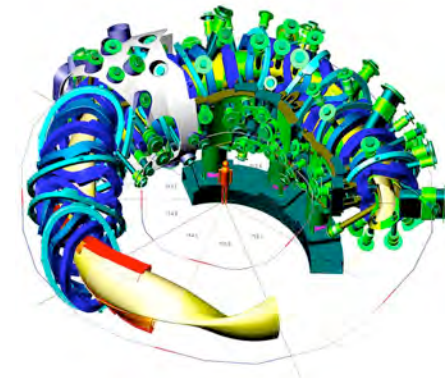
A very schematic comparison ...

- current in coils and plasma
- current-carrying plasma
- self-organized equilibrium



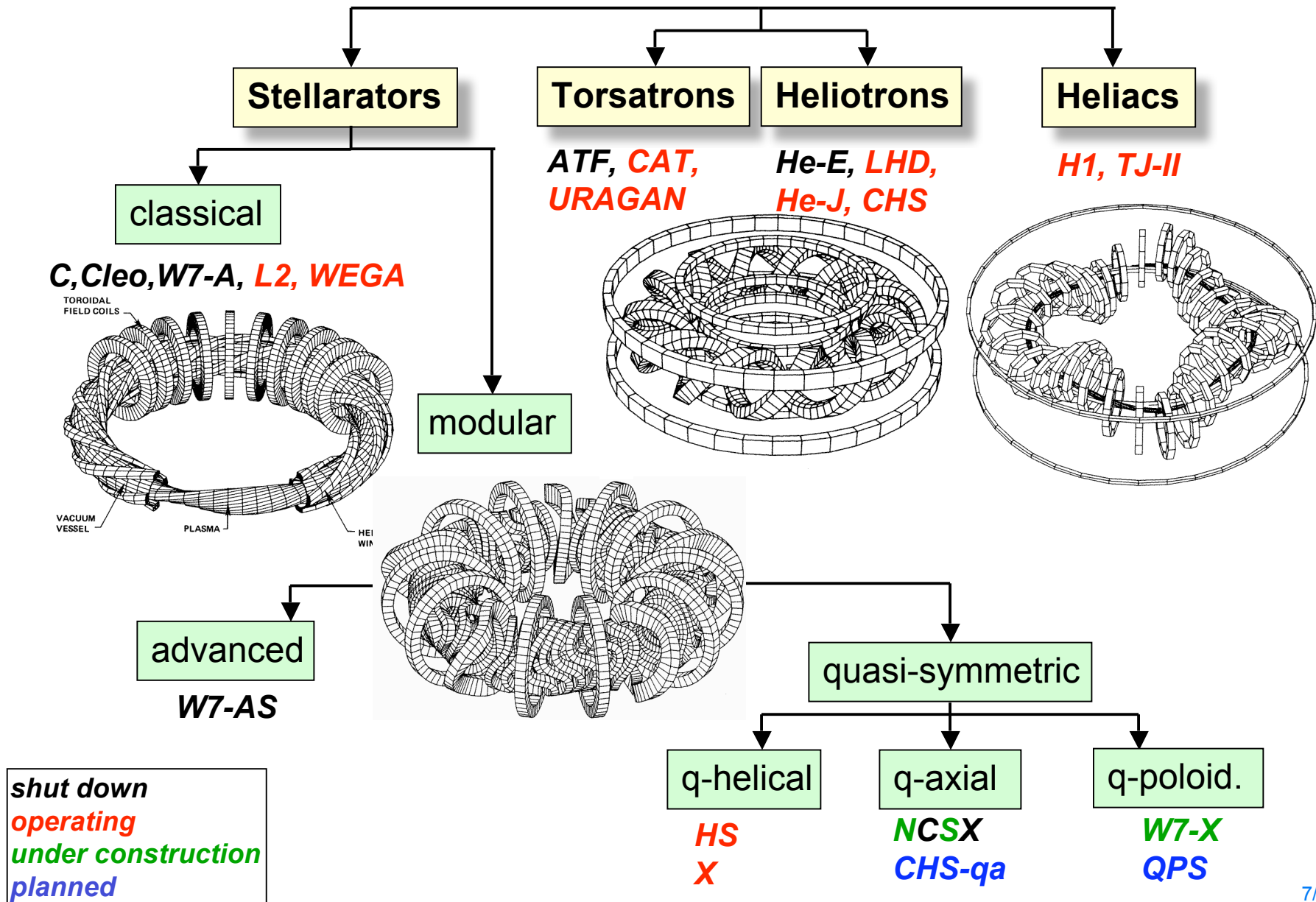
- ❖ good neoclassical confinement
- ❖ toroidal symmetry
- ◇ advanced scenarios and current drive
- ◇ active control of plasma instabilities

- current in the coils only
- very small plasma current
- field-defined equilibrium

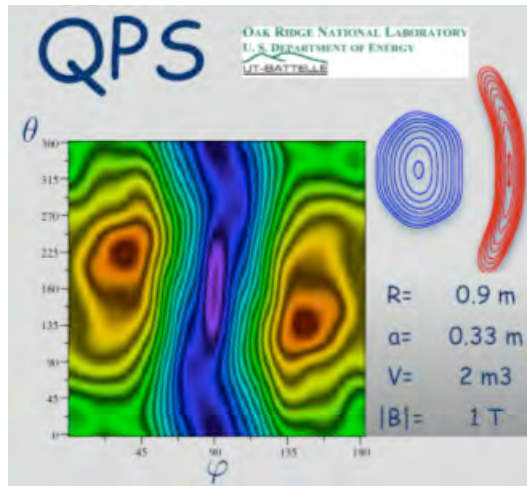


- ❖ good neoclassical confinement
- ◇ quasisymmetry
- ❖ steady state operation
- ❖ no current driven instabilities

The stellarator family

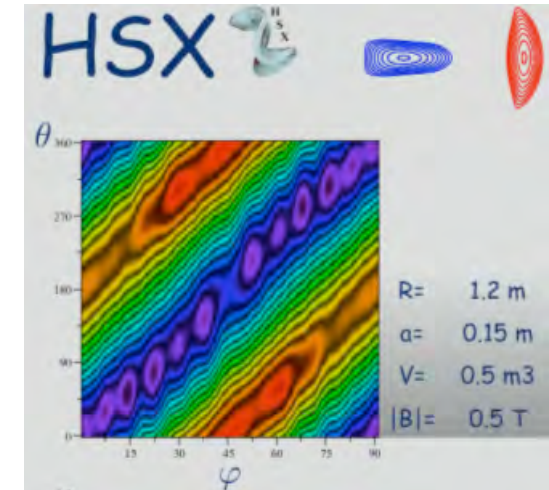


quasi-poloidal

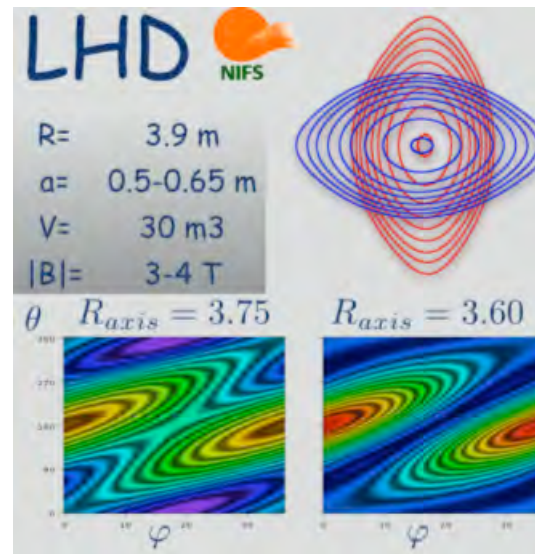


$|B|$

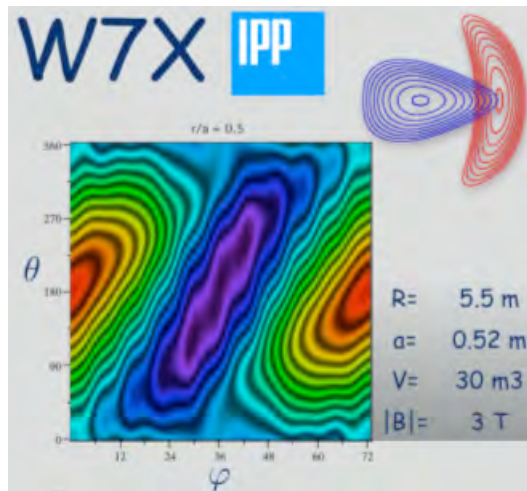
quasi-helical



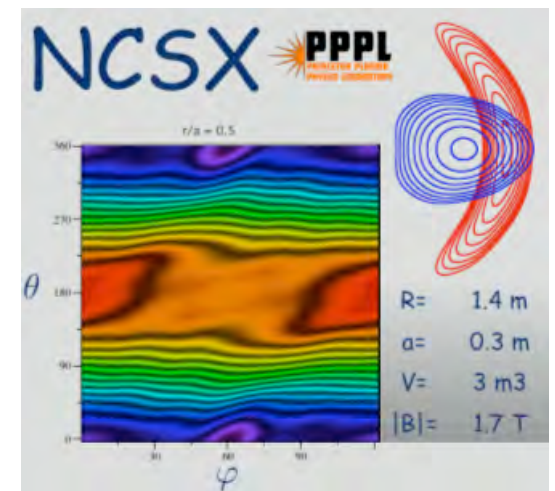
classical



quasi-isodynamic

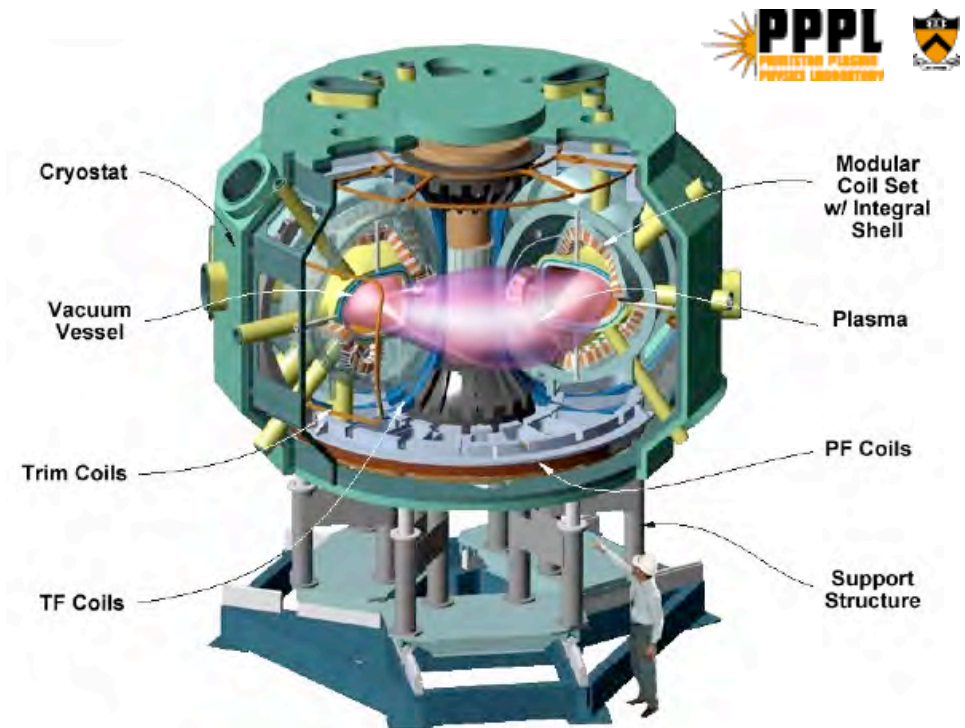


quasi-toroidal

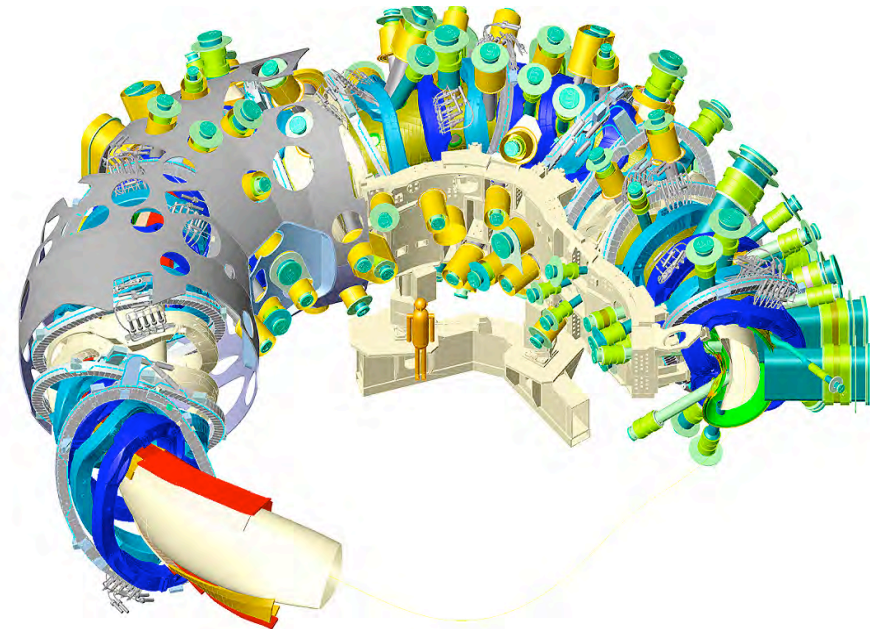
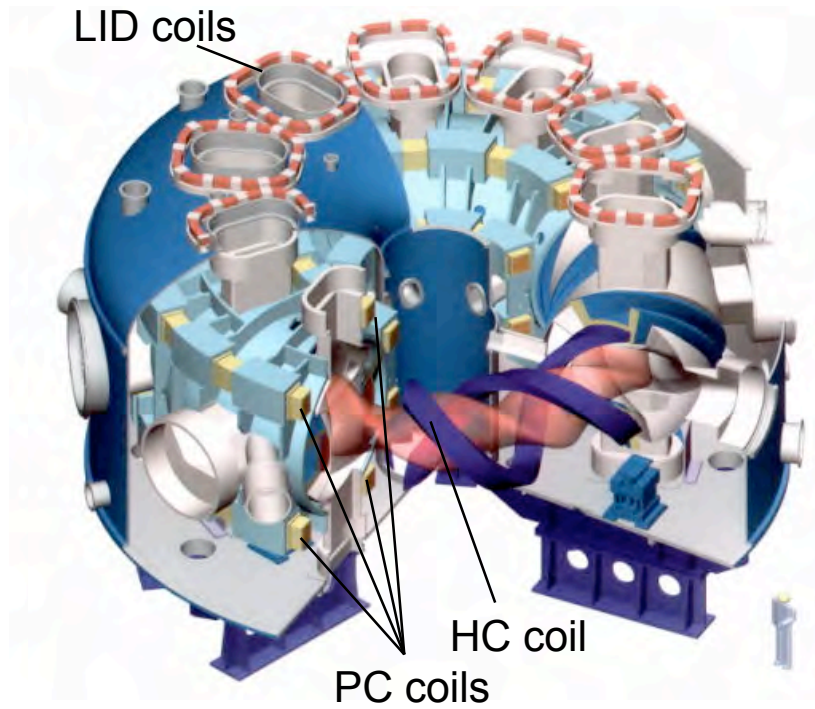


by courtesy of J. Sanchez

A missing link



- complete the physics understanding of quasi-symmetry
- development of compact stellarators
- a physics link to advanced tokamak operation
- let's advertise a revision of previous decisions



LHD

$$R_{ax} = 3.4 - 4.1 \text{ m}, a \leq 0.65 \text{ m}$$

$$V_{pl} = 30 \text{ m}^3$$

$$B \leq 2.9 \text{ T}, \iota(0) \geq 0.35, \iota(a) \leq 1.5$$

high shear, 10 field periods, $l = 2$

W7-X

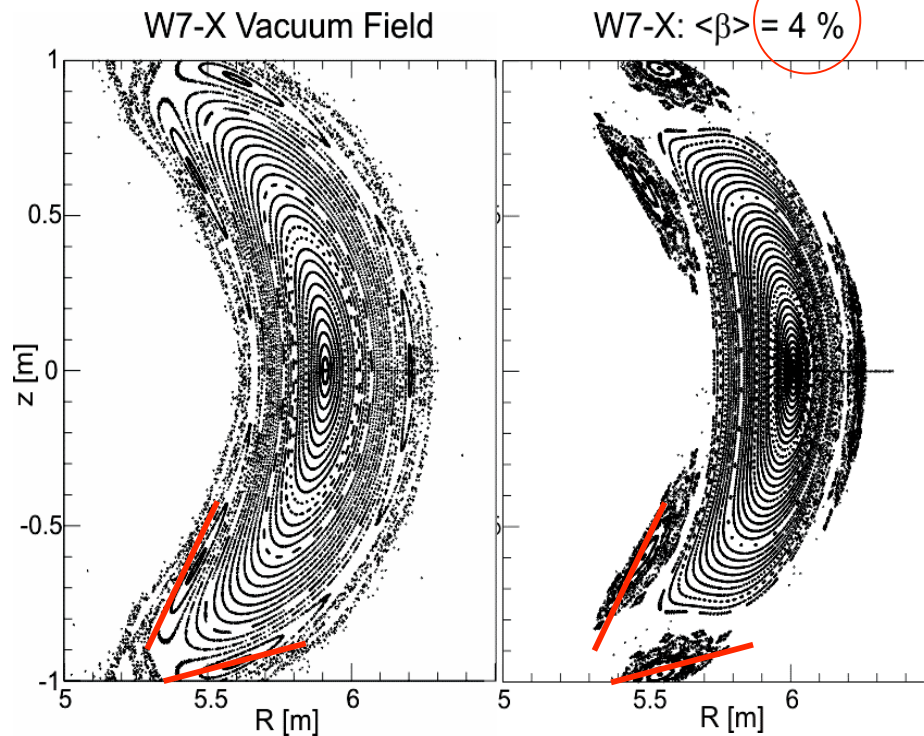
$$R_{ax} = 5.5 \text{ m}, a \leq 0.53 \text{ m}$$

$$V_{pl} = 30 \text{ m}^3$$

$$B \leq 3.0 \text{ T}, \iota(0) \geq 0.88, \iota(a) \leq 0.97$$

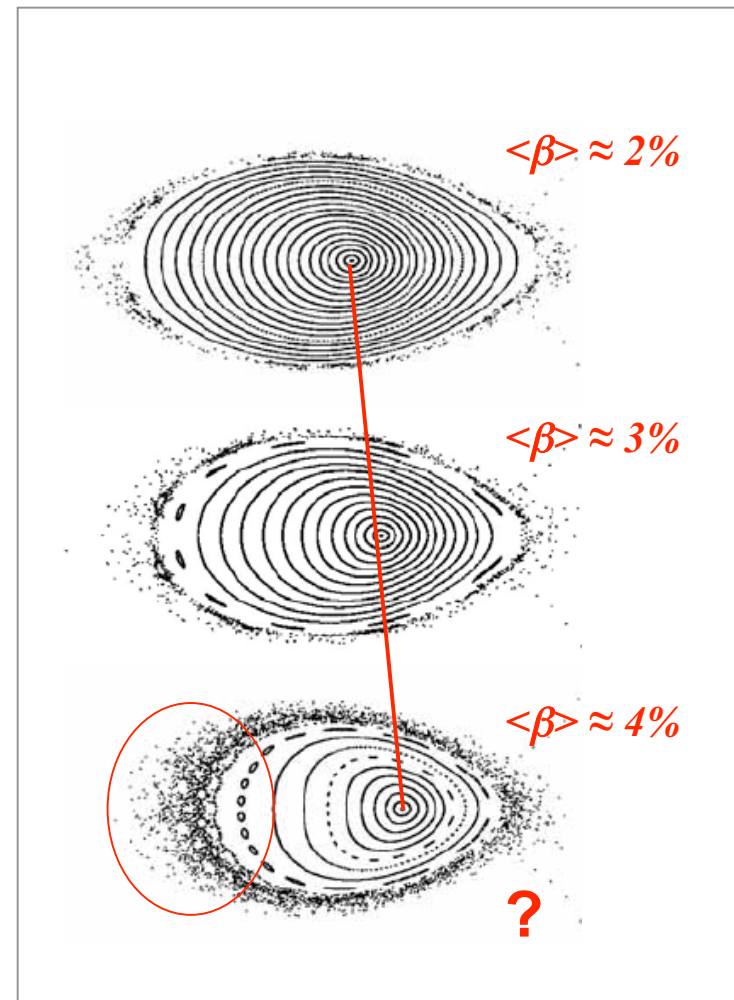
low shear, 5 field periods

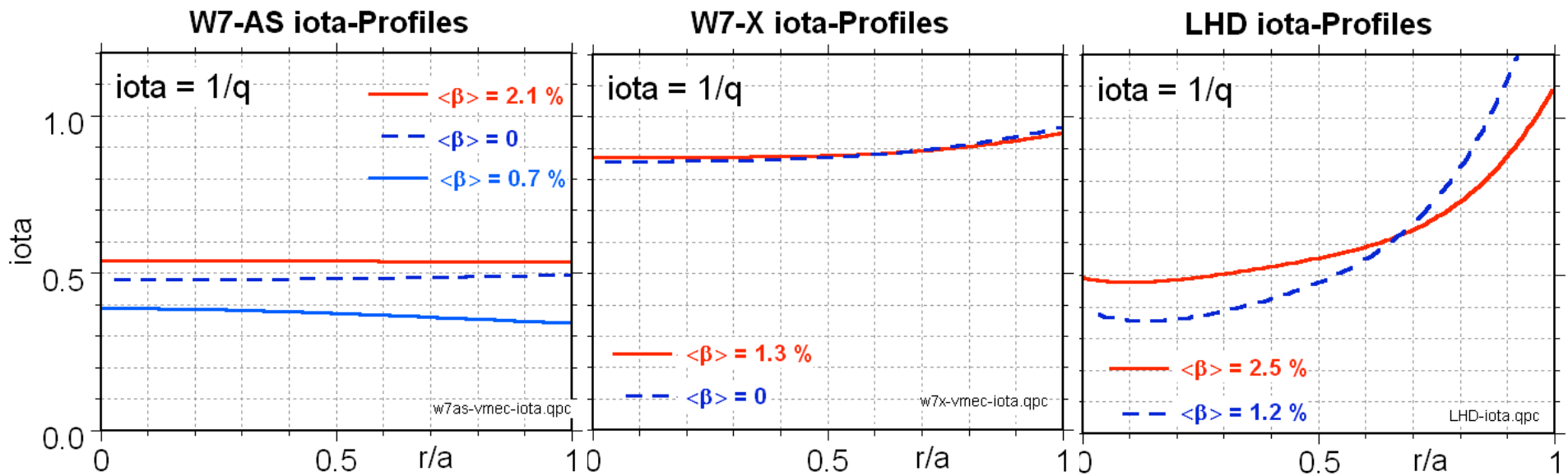
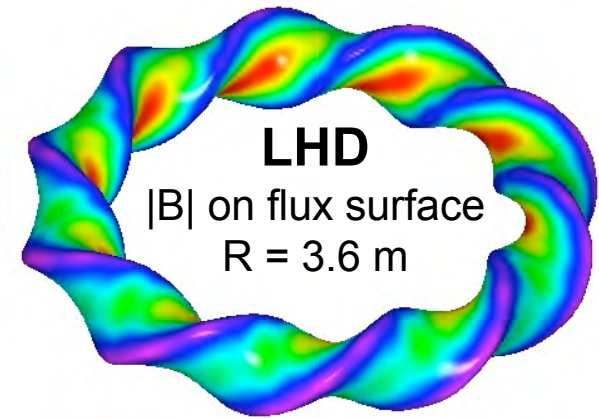
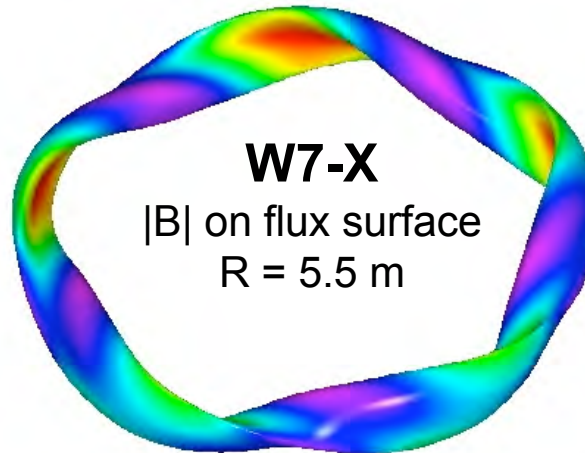
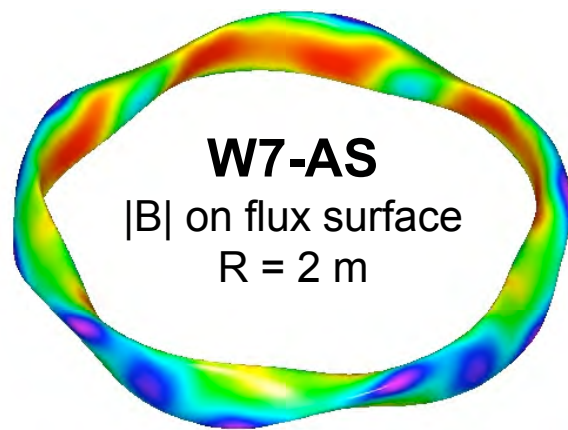
W7-X (PIES-Code)



- stable high-pressure equilibrium
- minimized stochastic layer formation
- required for reasonable divertor solution

LHD (HINT-Code)





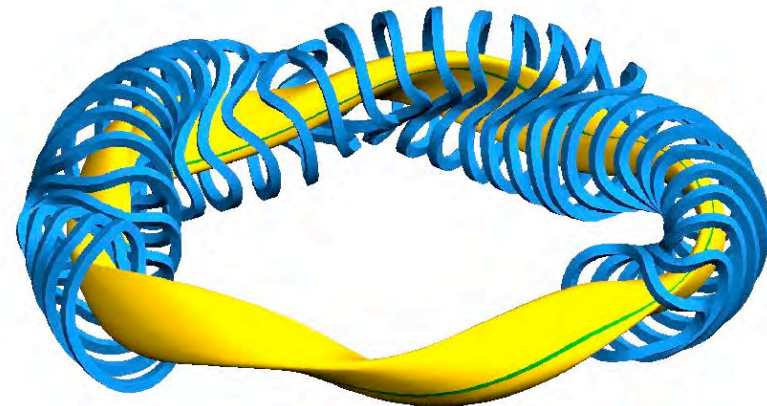
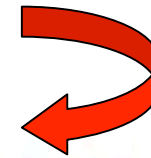
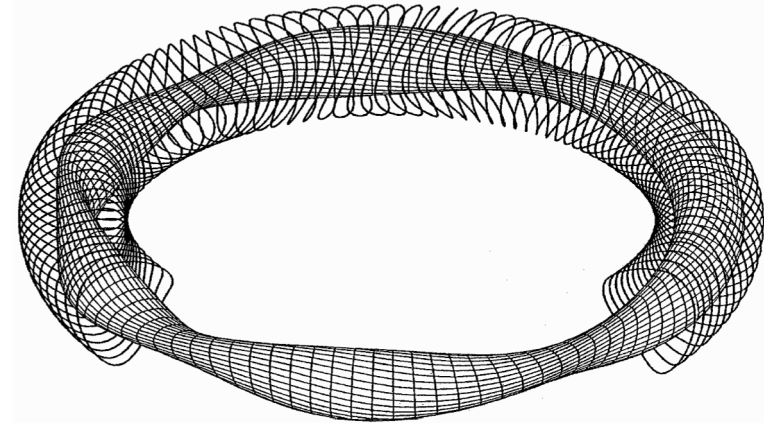
W7-line: avoid islands by low shear
LHD-heliotron: high shear, small islands

7 optimization criteria

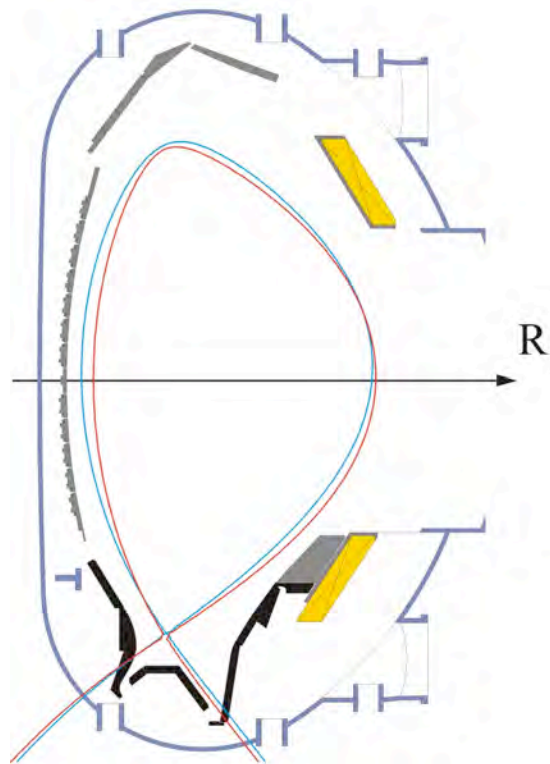
1. **feasible modular coils**
2. **good, nested magnetic surfaces**
3. **good finite- β equilibria**
4. **good MHD stability**
5. **small neoclassical transport**
6. **small bootstrap current**
7. **good confinement of fast particles**

development tasks

1. **optimum $nT\tau_E$ and high β discharges**
2. **steady state operation**
3. **plasma-wall interaction**
4. **island divertor operation**
5. **turbulent transport**

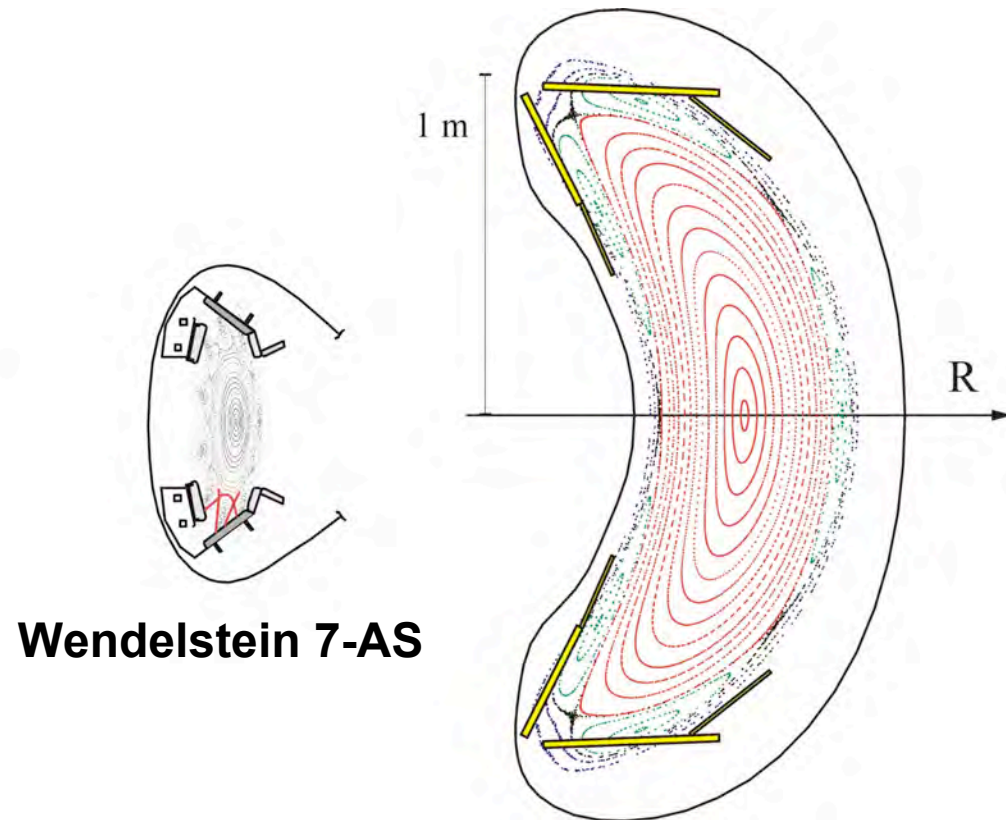


poloidal divertor



ASDEX upgrade

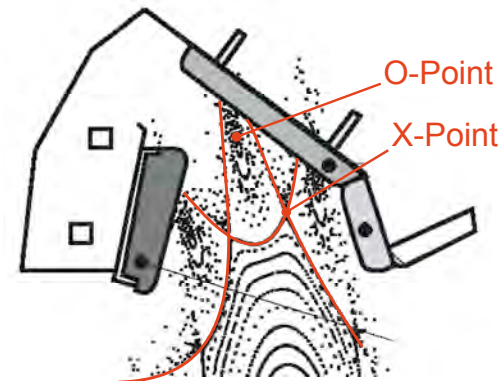
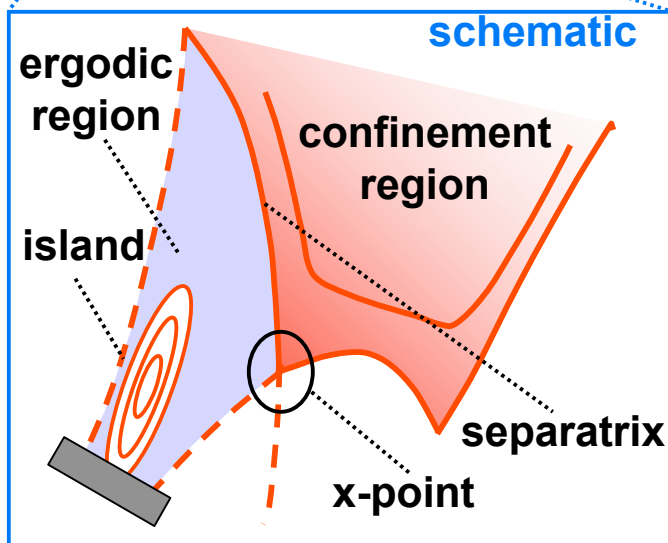
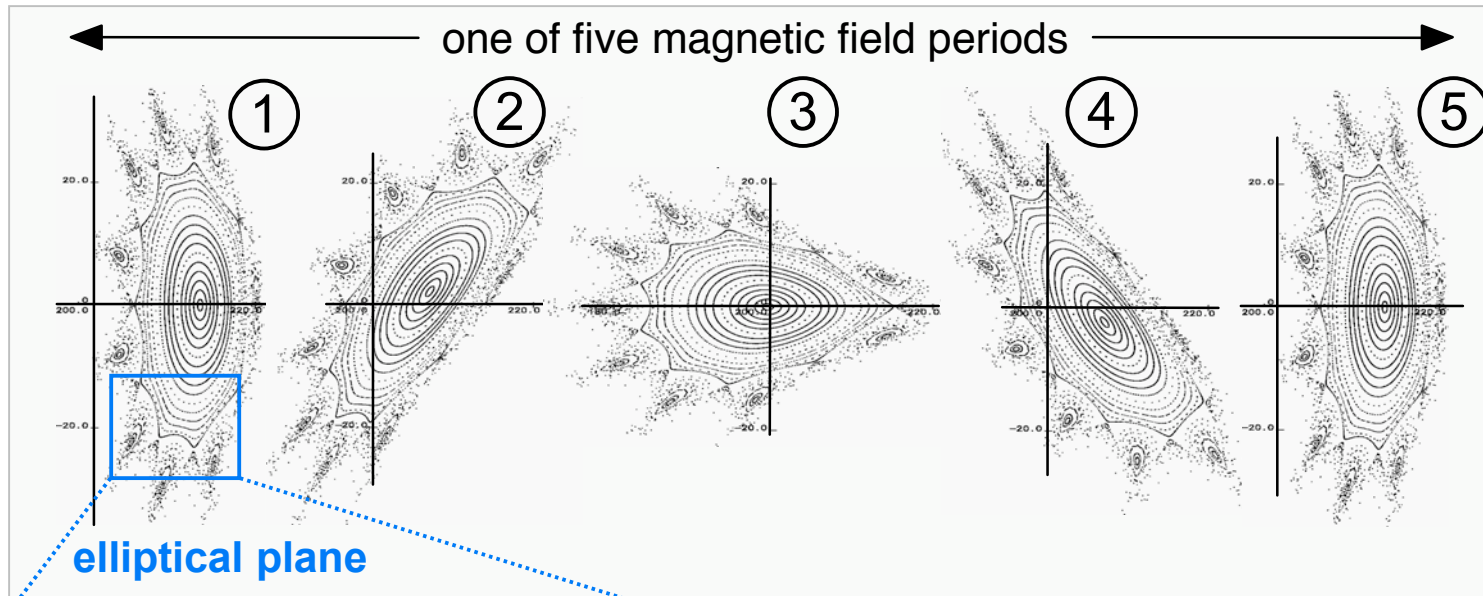
island divertor



Wendelstein 7-AS

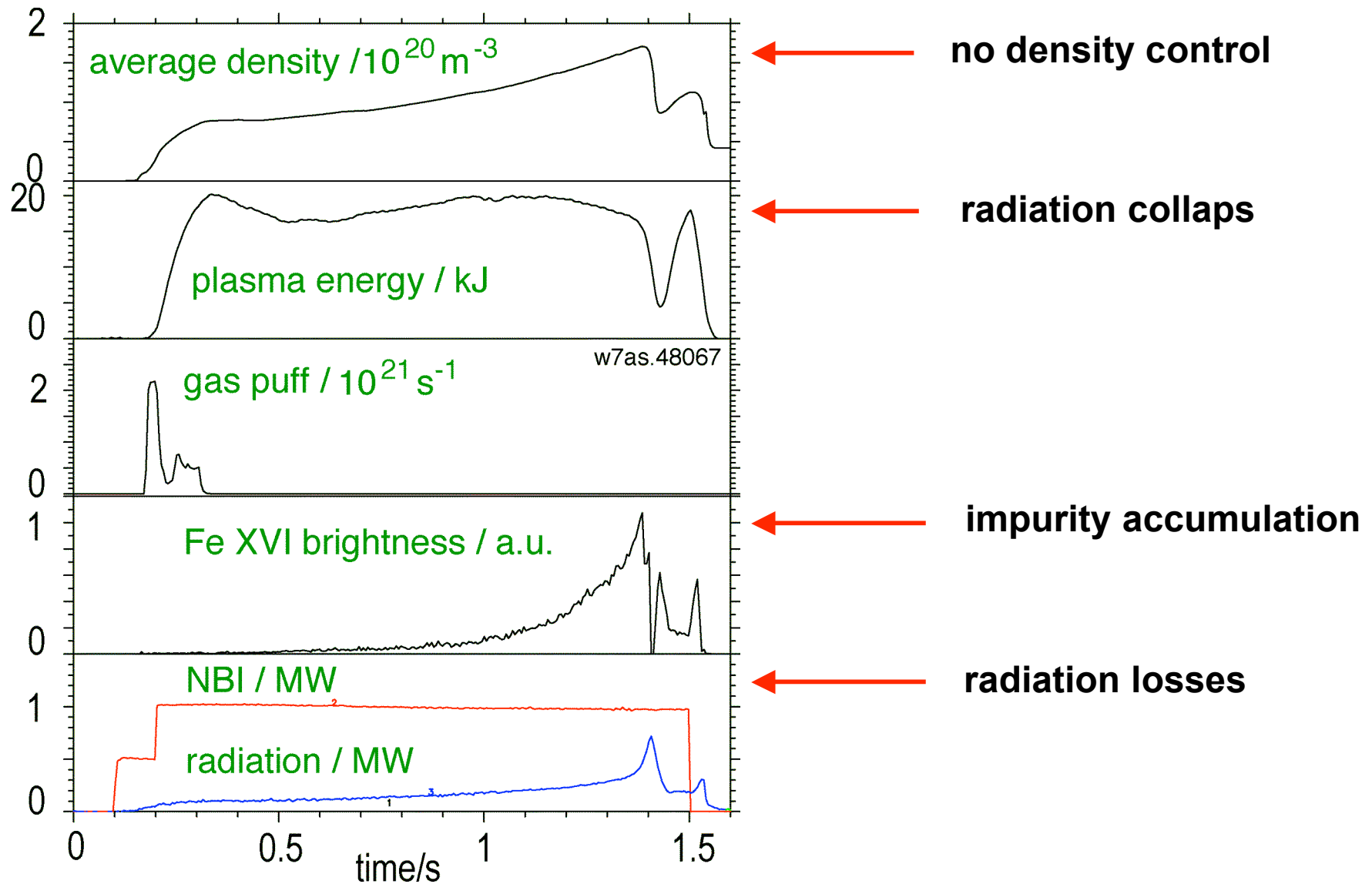
Wendelstein 7-X

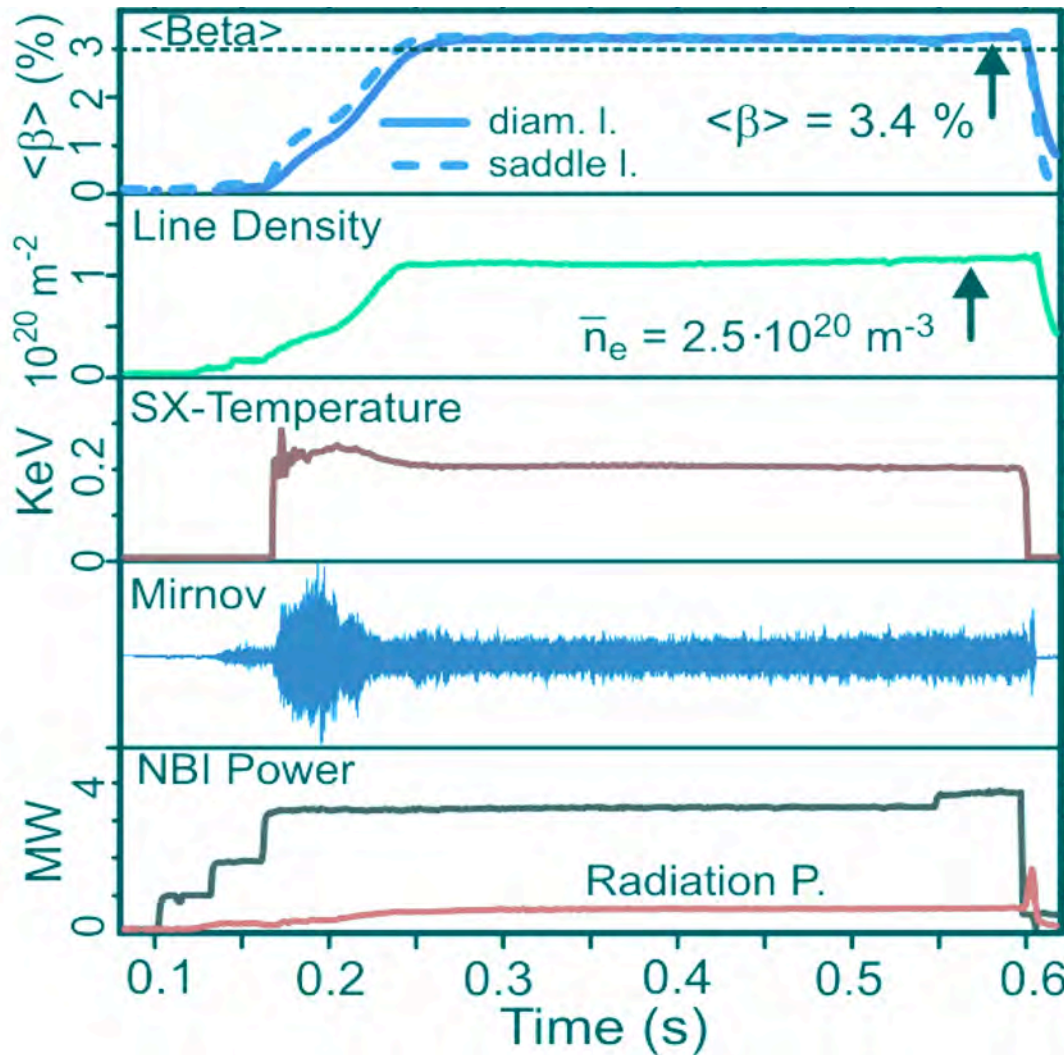
The W7-AS island divertor



the idea:

natural islands are intersected with target





high pressure

$$\beta = 3.4\%$$

$$\beta_N \sim 9.3$$

high density

$$n_e = 2.5 \cdot 10^{20} \text{ m}^{-3}$$

$$n_e/n_{eGW} = 2.5$$

confinement

$$H_{ISS95} = 1.4$$

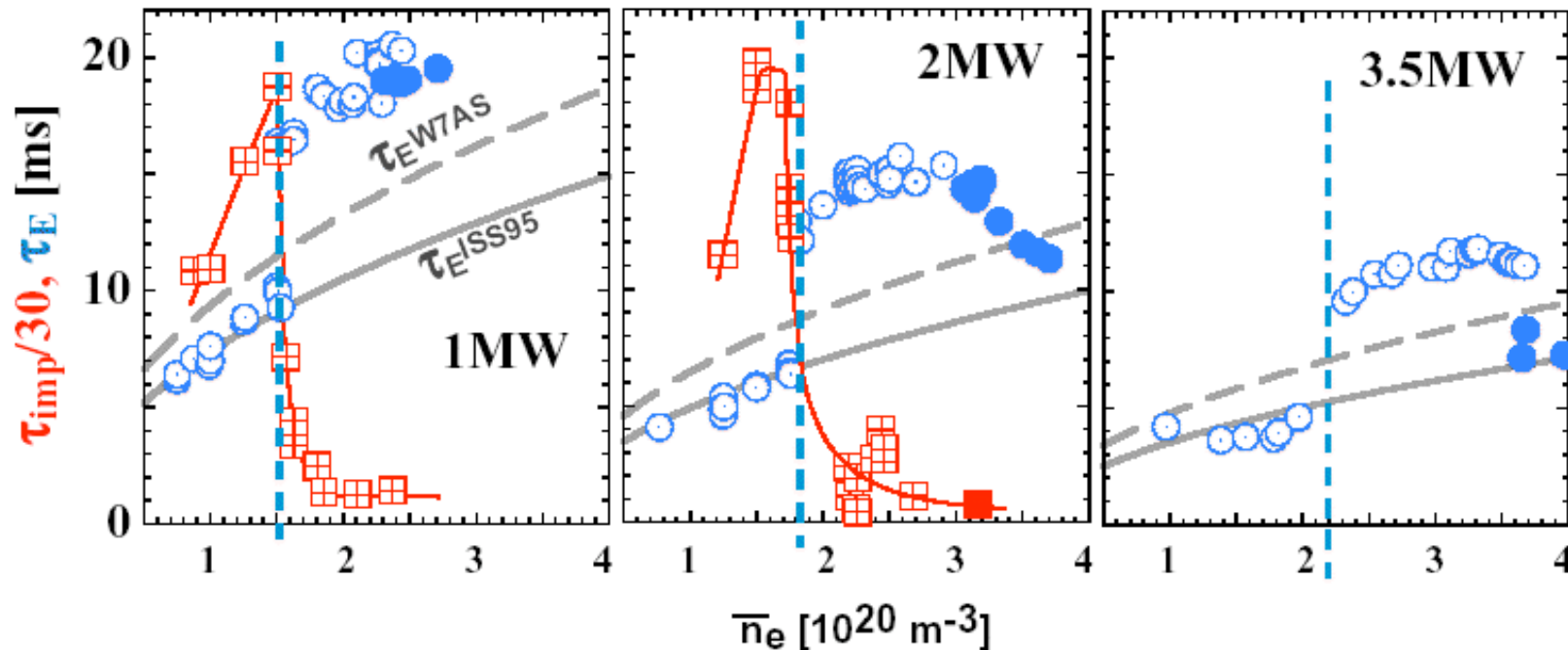
MHD stability

absorption

$$P_{abs} = 2.5 \text{ MW}$$

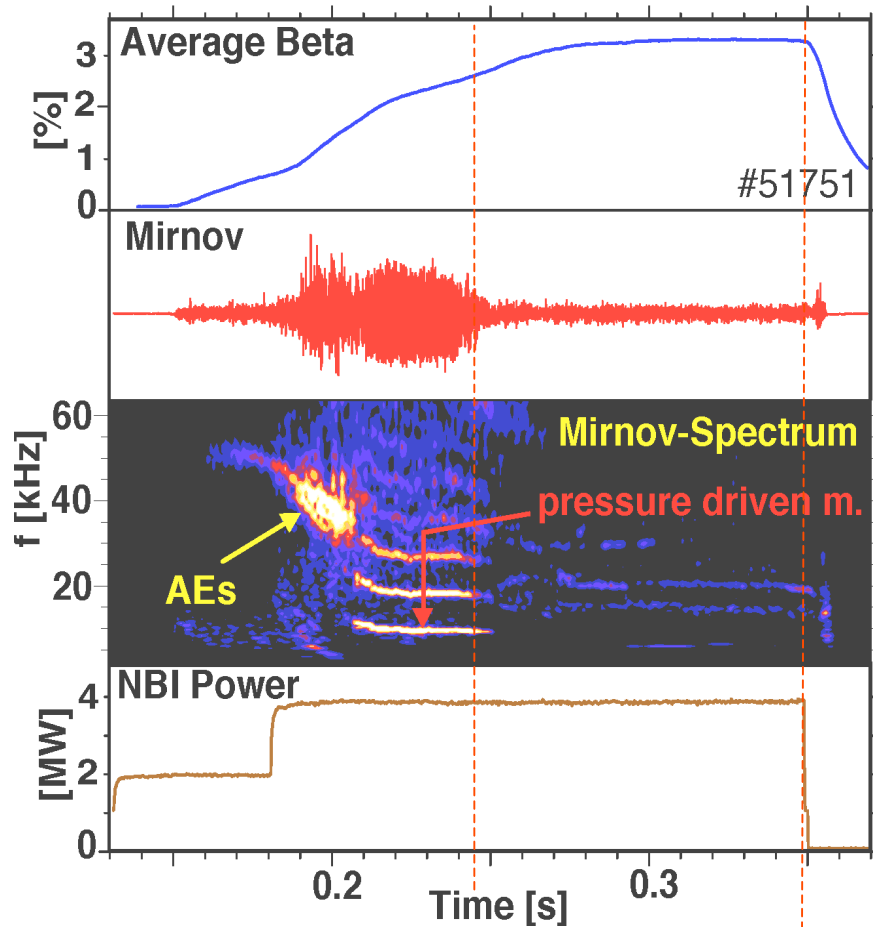
stationarity $T_{flattop} \sim 100 \tau_E$

the high-density high-confinement (HDH) mode was discovered in 2002 on W7-AS

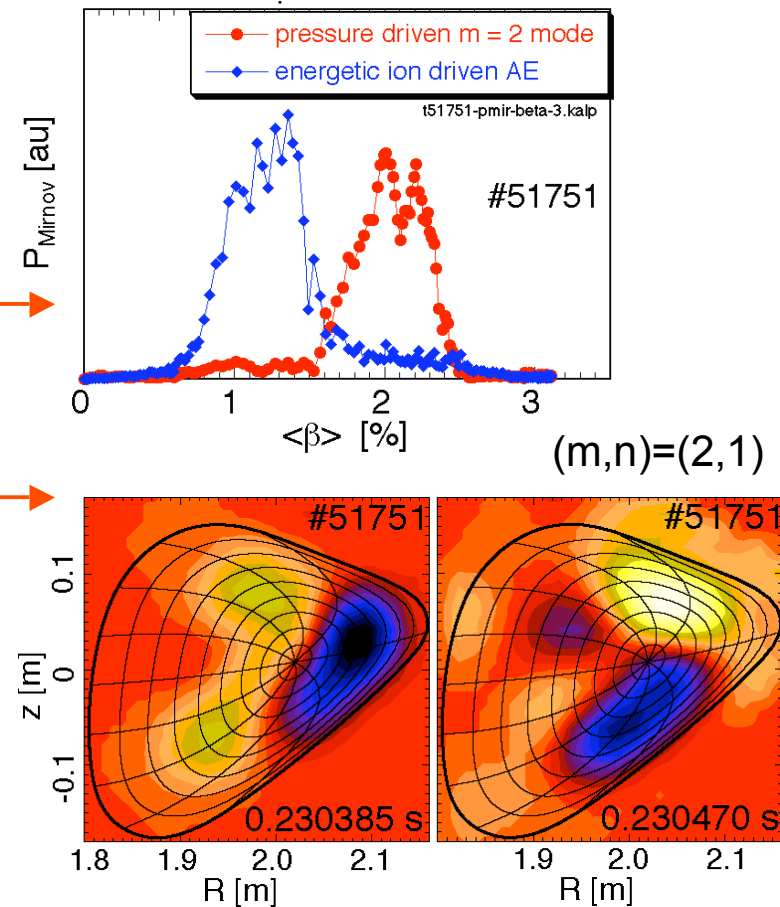


HDH-regime - a true bifurcation with hysteresis, profile differences, ...

- ▶ confinement of energy increases
- ▶ confinement of impurities deteriorates



MHD modes disappear at high β



- inwards shift of $\iota=1/2$ surface
 - formation of magnetic well
- } $\beta \rightarrow 3\%$

[Weller 2003]
[Werner 2003]

W7-AS Performance /w island divertor

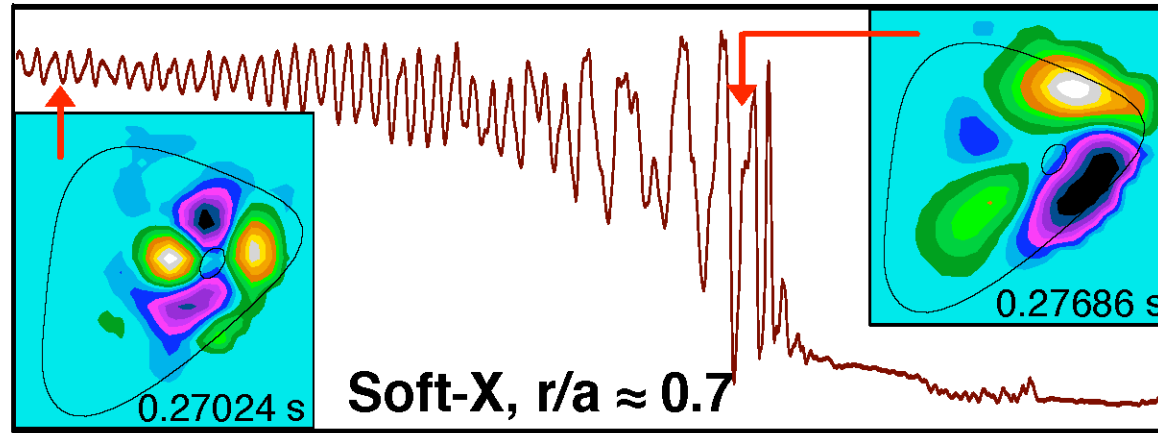
- **Based on resonant magnetic islands @ edge**
- **A viable divertor solution for stellarators**
- **Controlled heat and particle deposition**
- **Density control even at high plasma densities $\sim 2 \cdot 10^{20} \text{m}^{-3}$**
- **Establishment of High-density H-mode (HDH)**
 - **Establishes at $n \sim 1.5 \dots 2.5 \cdot 10^{20} \text{m}^{-3}$**
 - **Quiescent and MHD stable** ← **magnetic well formation**
 - **Different from ELM-free H-mode**
 - **Improved energy confinement**
 - **Impurity screening** ← **high edge densities**

	RFP	Tokamak	W7-X	LHD	NCSX
diamagnetic current	O (1)	O (1)	O (1)	O (1)	O (1)
Pfirsch-Schlüter current	0	O (1)	→ 0	O (1)	O(1)
bootstrap current	0	→ O (1)	→ 0	O (-1)...O (1)	O (1)
induced current	→ O (1)	O (1) → 0	0	0	0
plasma dynamo	O (1) → 0	0	0	0	0
current drive	0 → O (1)	0 → O (1)	0	0	0

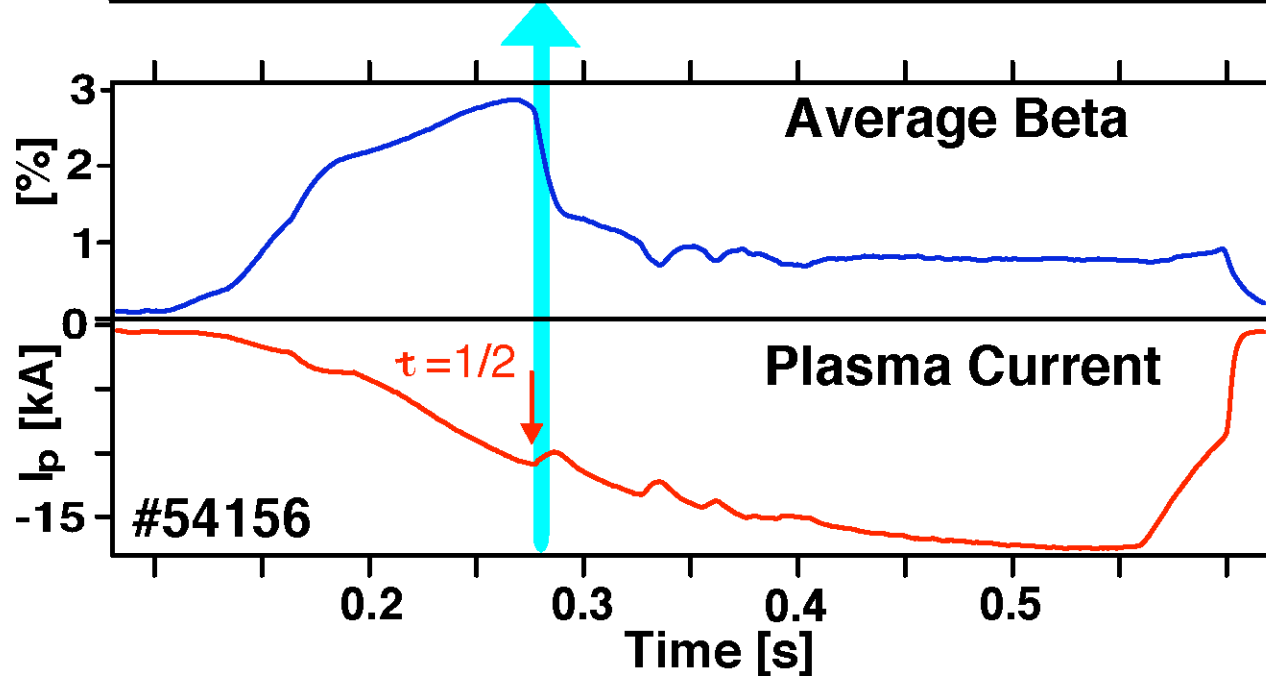
all currents are normalized to their respective frame

By courtesy of F. Wagner

It is possible to reduce systematically the currents in the plasma.



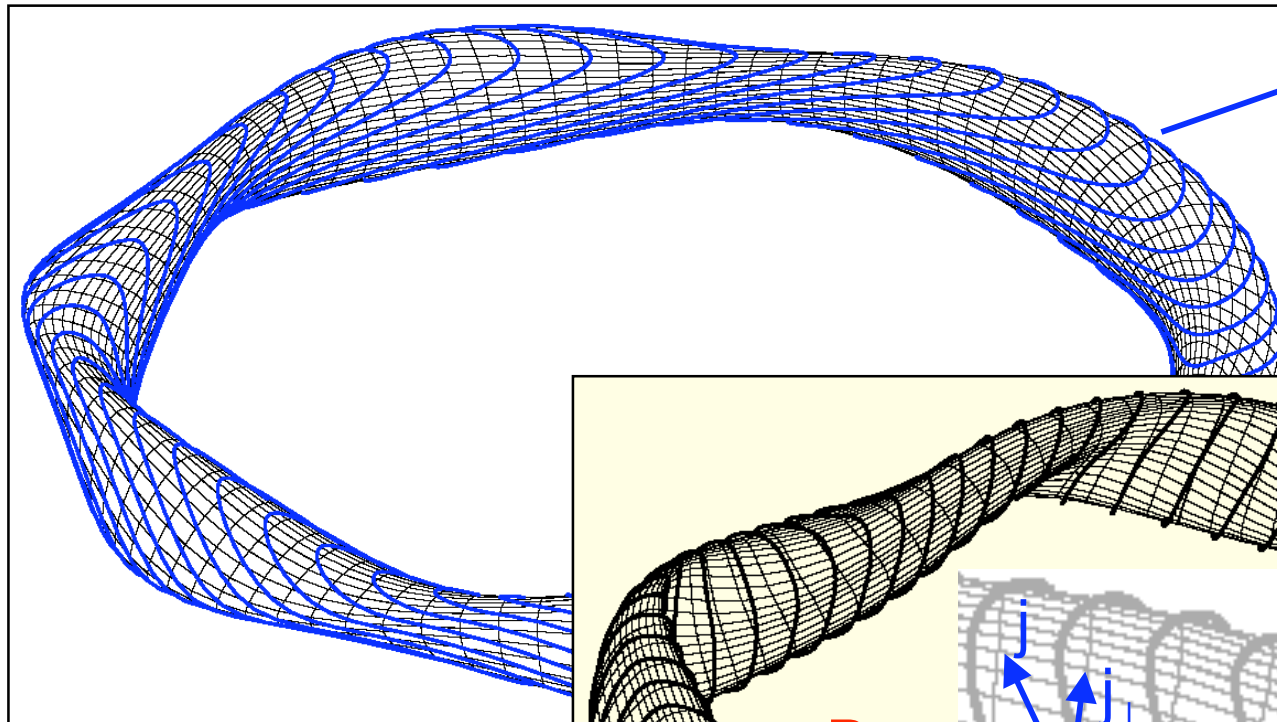
magnetic
fluctuations
and
soft-X radiation



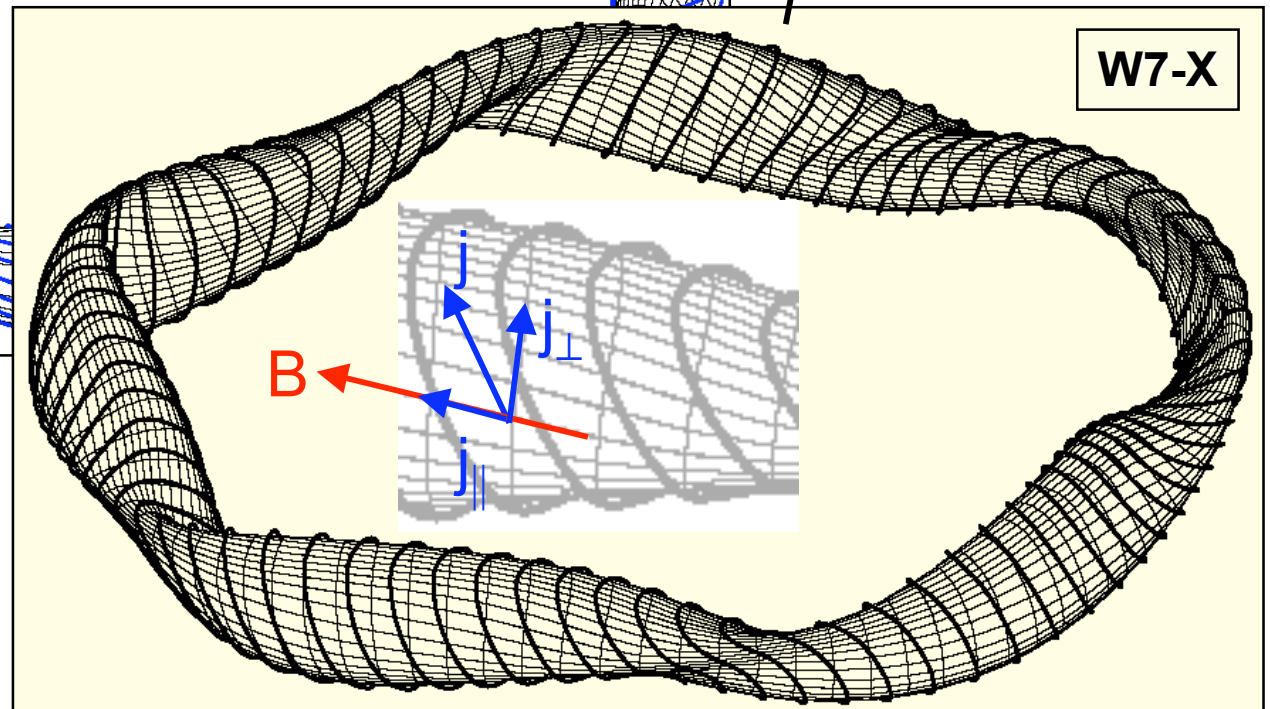
current driven
instability
tearing-mode type
onset at $iota = 1/2$

Non-inductive equilibrium currents

L = 2 stellarator



current lines



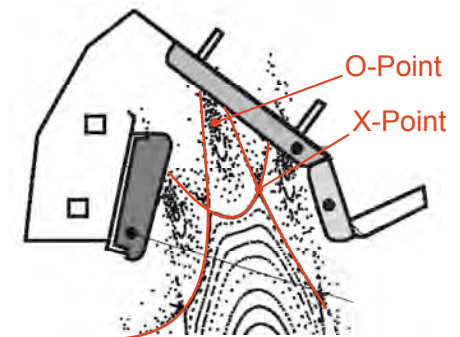
W7-X

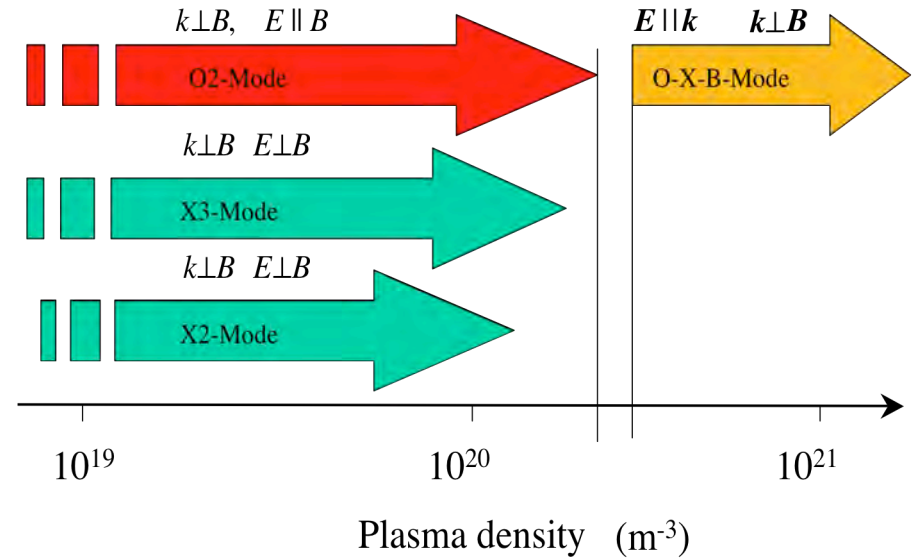
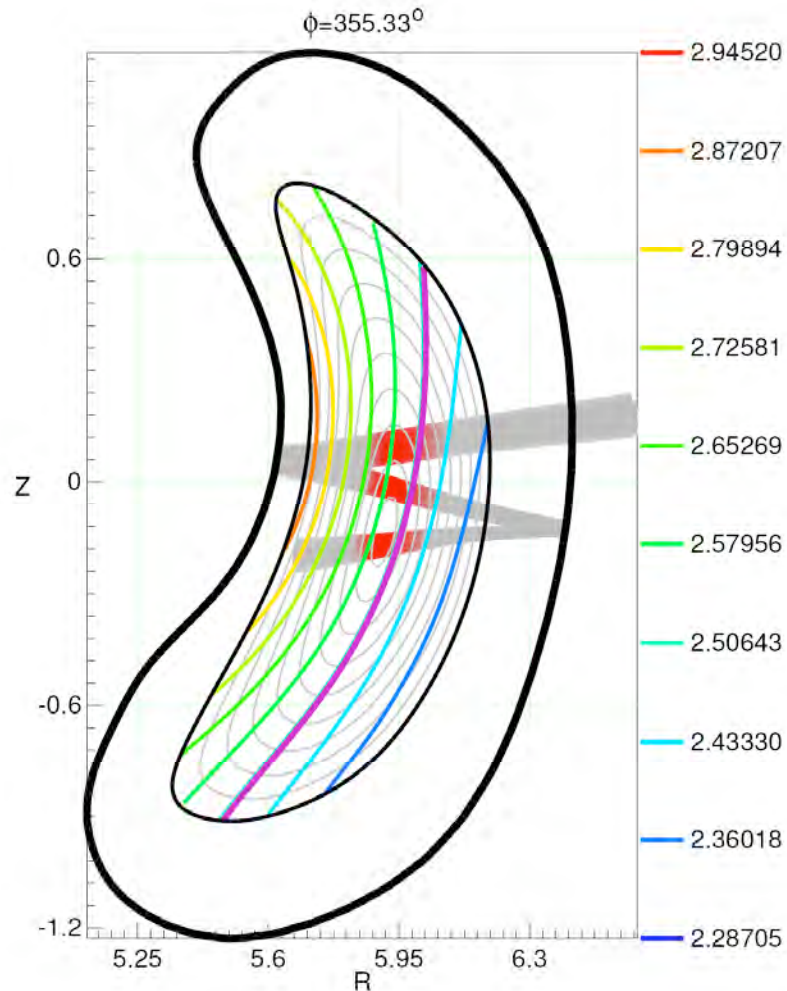
equilibrium current

$$J = J_{dia} + J_{PS} + J_{BS}$$

Ex:

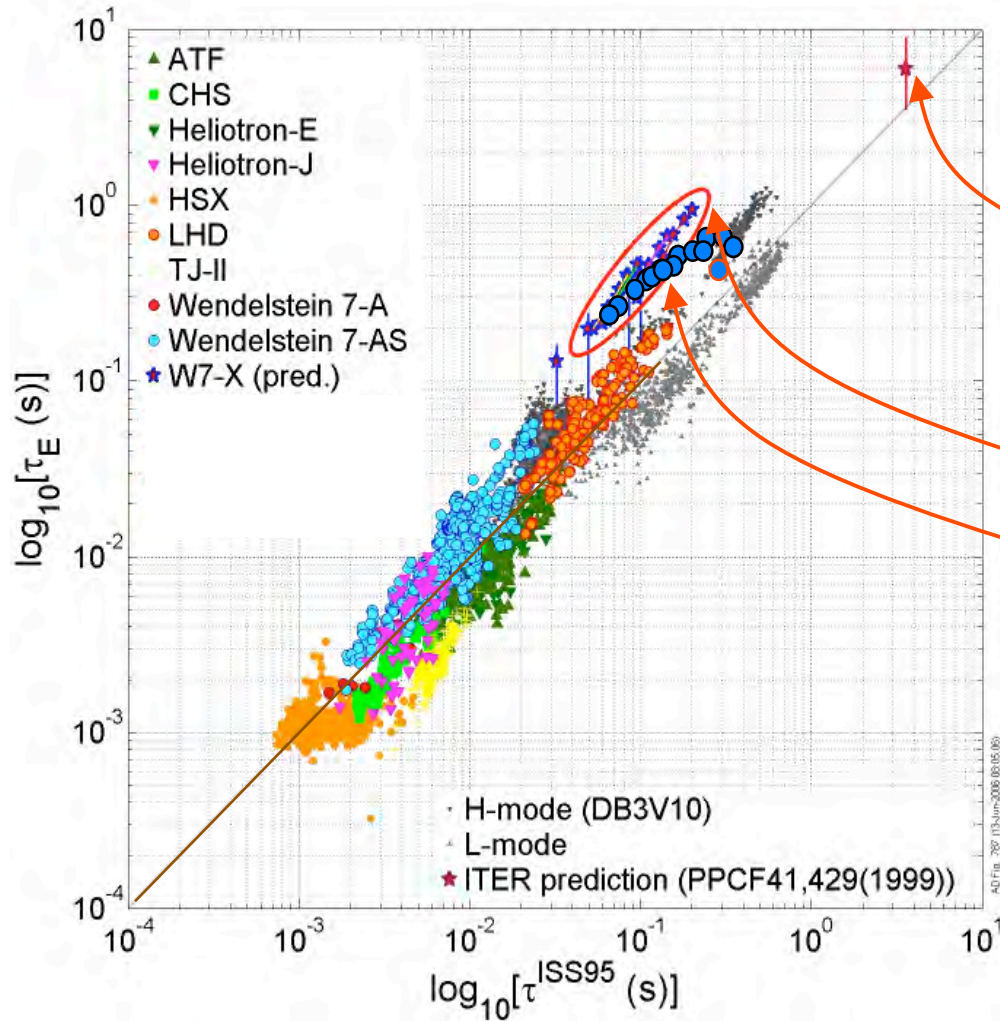
- 1d transport modelling coupled with ray-tracing code
- Off-axis X2-heating in standard configuration
- Current drive required for control of edge i_{ota}
- Current drive efficiency $P=10\text{MW}$ $\langle\beta\rangle=2.7\%$ $I_{CD}=-88\text{kA}$





- **O2-launch angle 12°**
- **Heating up to $2.1 \cdot 10^{20} \text{m}^{-3}$**
- **Single pass absorption drops to 50%**
- **Double pass with retro-reflectors**

Current drive in X2 and O2



ITER

10 MW ECRH

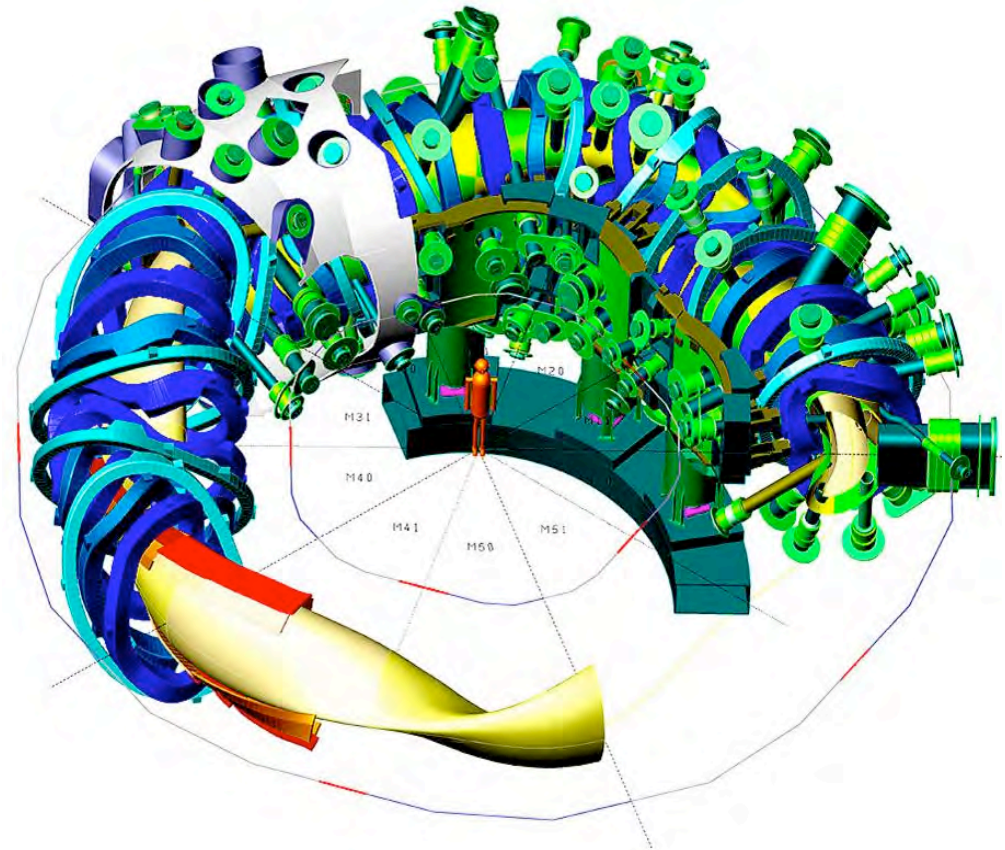
10 MW NBI (H⁺)

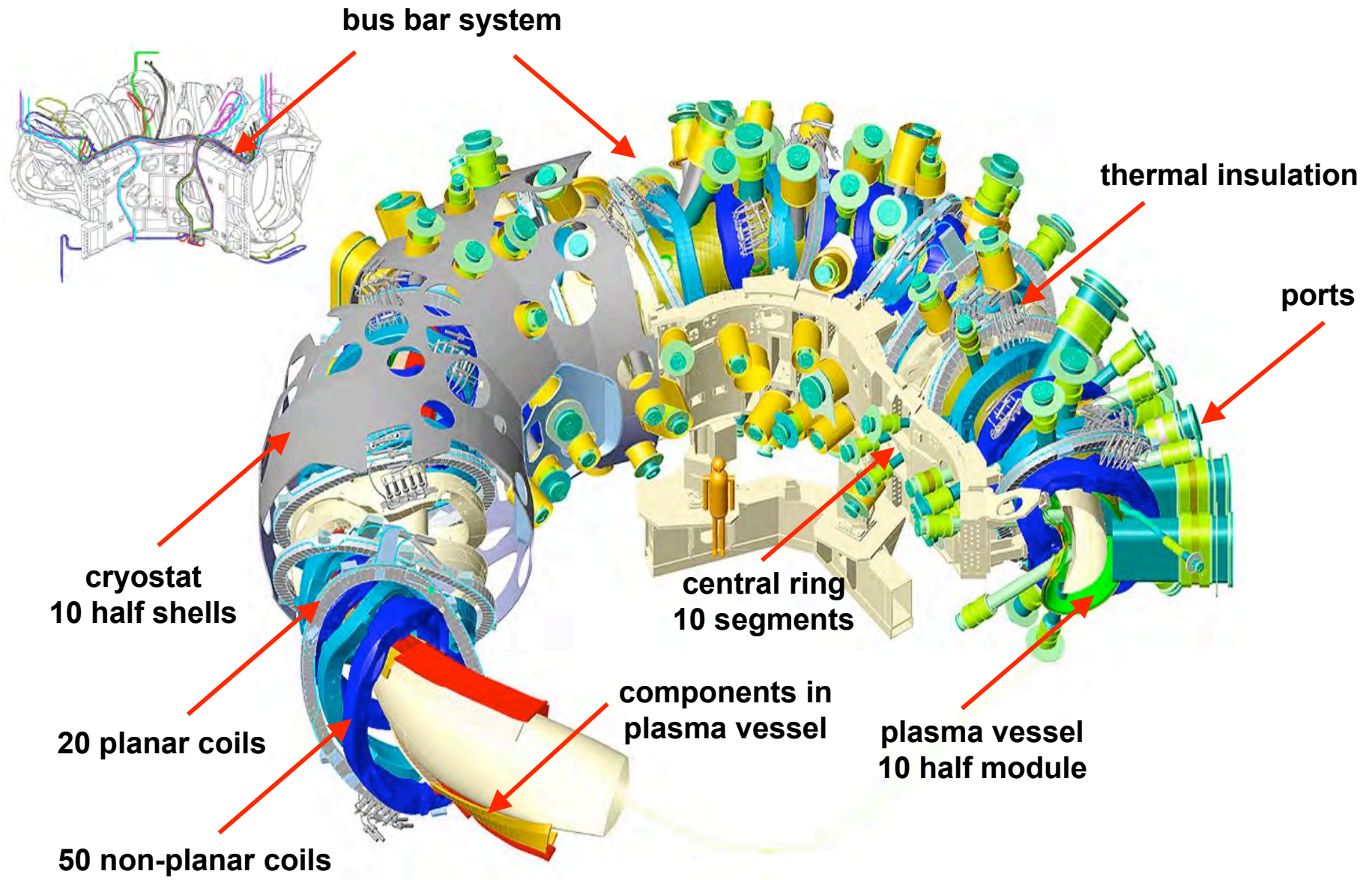
Numerical simulations:
much improved confinement

$$\tau^{\text{ISS95}} = 0.256 a^{2.21} R^{0.65} P^{-0.59} n_{20}^{0.51} B^{0.83} t_{2/3}^{0.4}$$

key parameters

major radius:	5.5 m
minor radius:	0.53 m
plasma volume	30 m ³
non-planar coils:	50
planar coils:	20
number of ports:	253
rot. transform:	5/6 - 5/4
induction on axis:	< 3T
stored energy:	600 MJ
heating power	15 - 30 MW
pulse length:	30 min
energy turn ar.:	18 GJ
machine height:	4.5 m
machine diameter:	16 m
machine mass:	725 t
cold mass:	425 t





the volume in the cryostat is very constrained ■



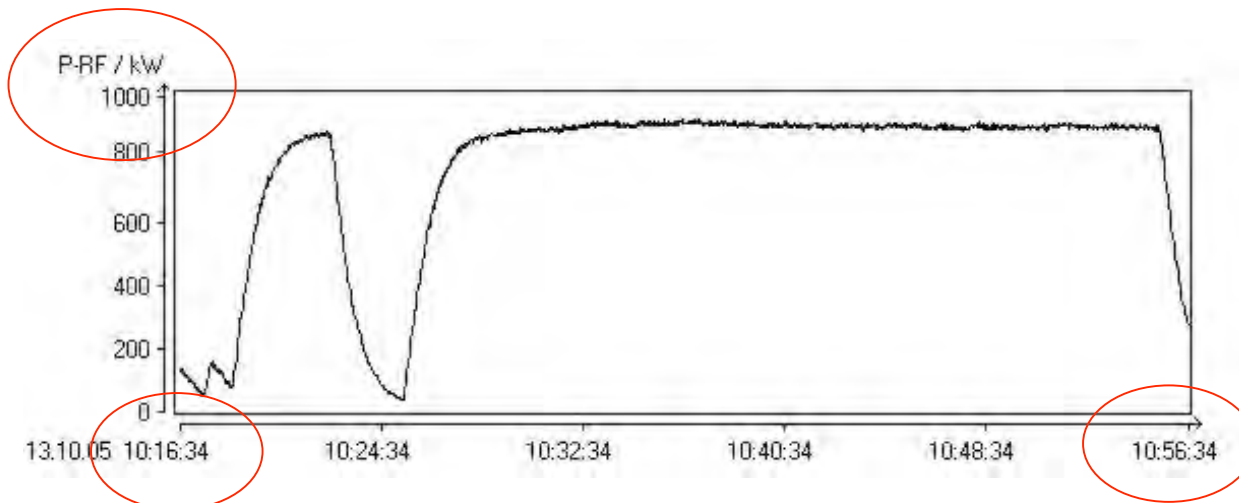
Forschungszentrum Karlsruhe
in der Helmholtz-Gemeinschaft



THALES

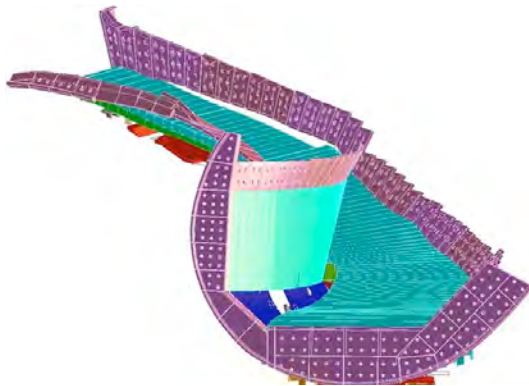
- power gyrotrons
- $10 \times 1\text{ MW } 140\text{ GHz}$
- pulse length 1800s
- quasi-optical duct

- world record shot
- integrated cw design
- series production?

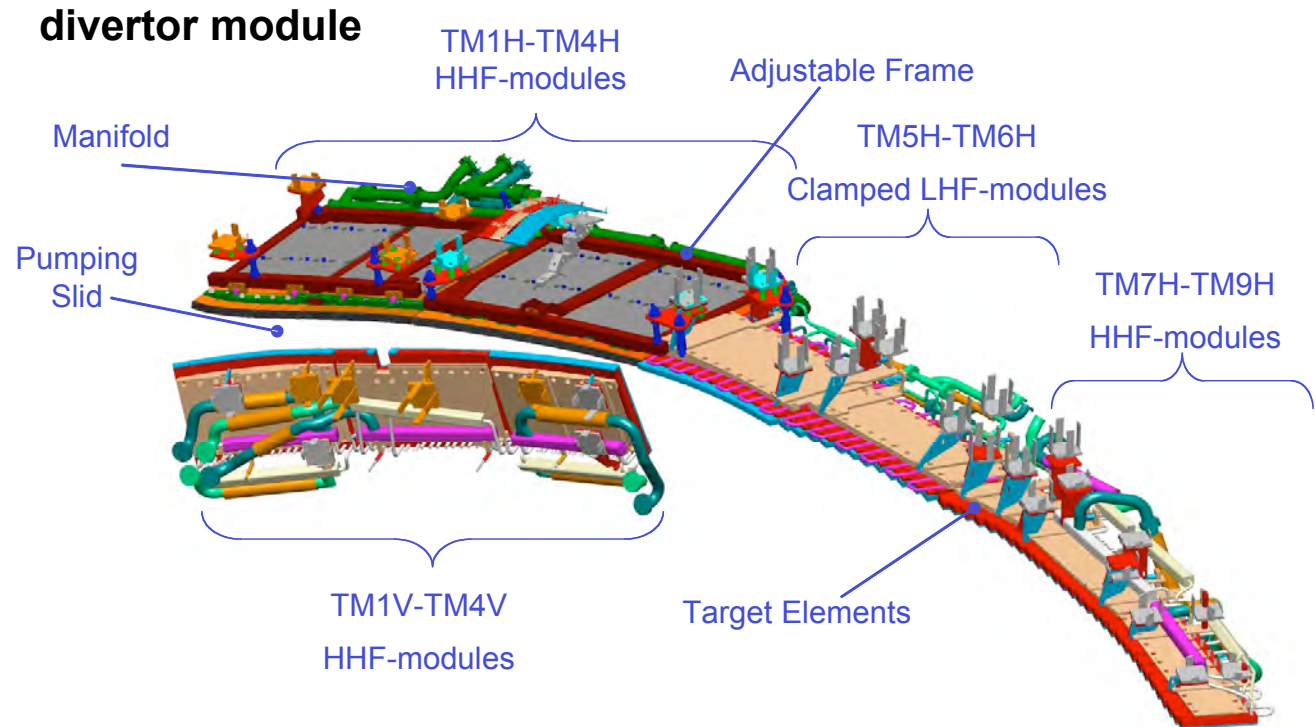




wall panel cooling



test divertor

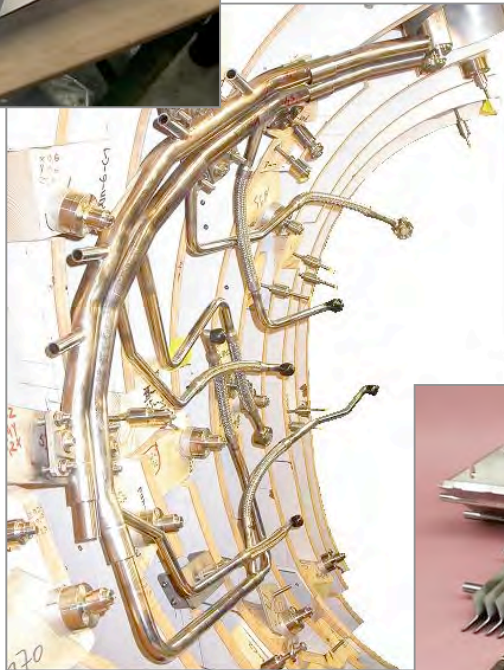
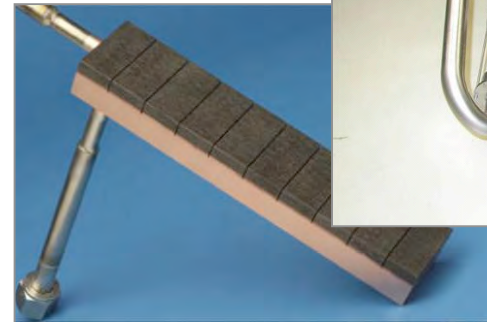


- target elements CFC sealed on cooled CuCrZr
- baffle elements graphite clamped on CuCrZr
- cryopumps and sweep coils
- about 250.000 parts w 130.000 being non-standard
- about 4km in-vessel water pipe lines
- start of operation with inertially cooled test divertor



**Heat shield
(IPP)**

**Target modules
(Plansee)**

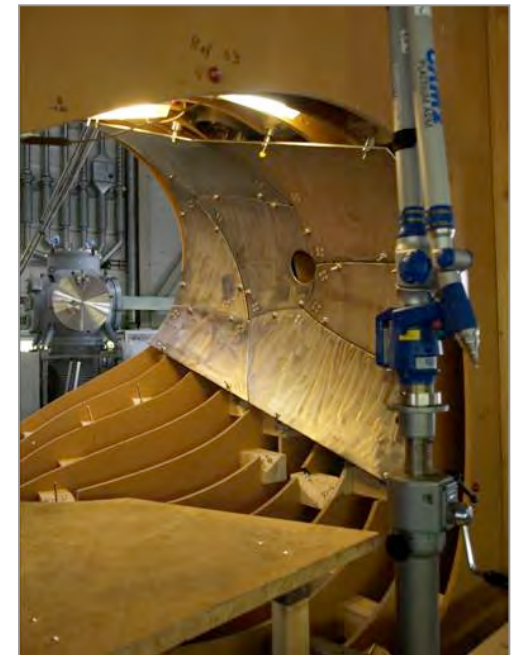


**Cooling pipes
(IPP and n.n.)**

**Wall pannels
(MAN DWE)**



**Cryo pumps
(IPP)**



CAD drawing non-planar coil



Status coil delivery

20 planar coils

50 non-planar coils

100M€ contract → consortium

100% manufactured

70% successfully cold tested

**plasma vessel
modules**



**assembly
progress**

outer vessel with domes



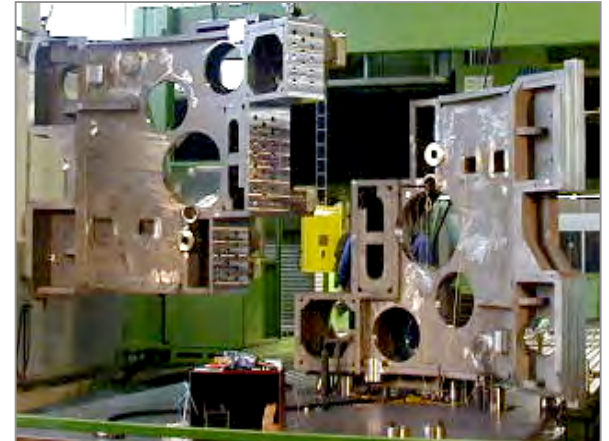
thermal insulation



assembly



central ring modules



The outer vessel



More than 1000 openings ~ thermal insulation laborious



Coil assembly



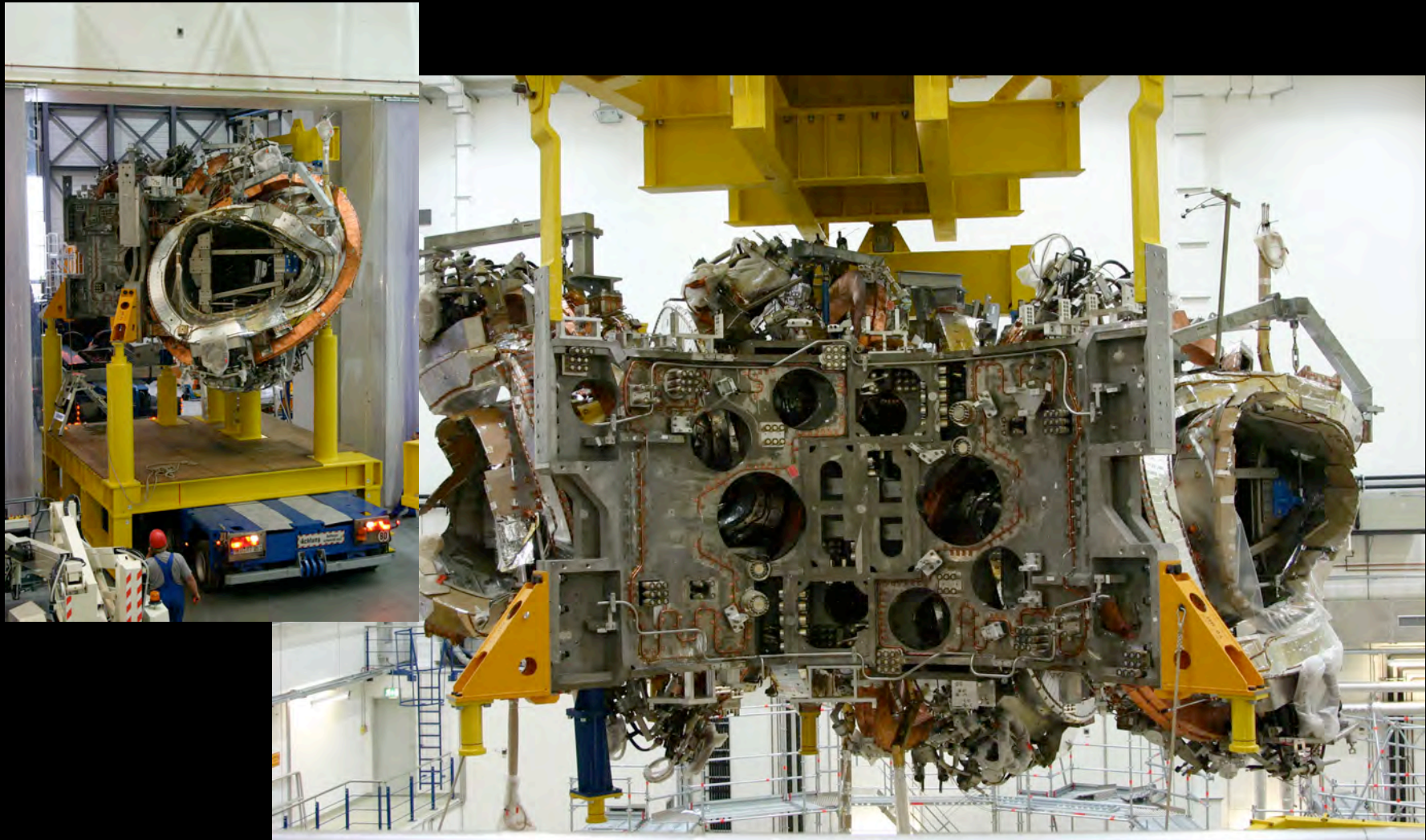
The 20 coils of first two modules assembled ■ – supports are welded



The five assembly stands are ready and fill step-wise (now 3/5)



Magnet module

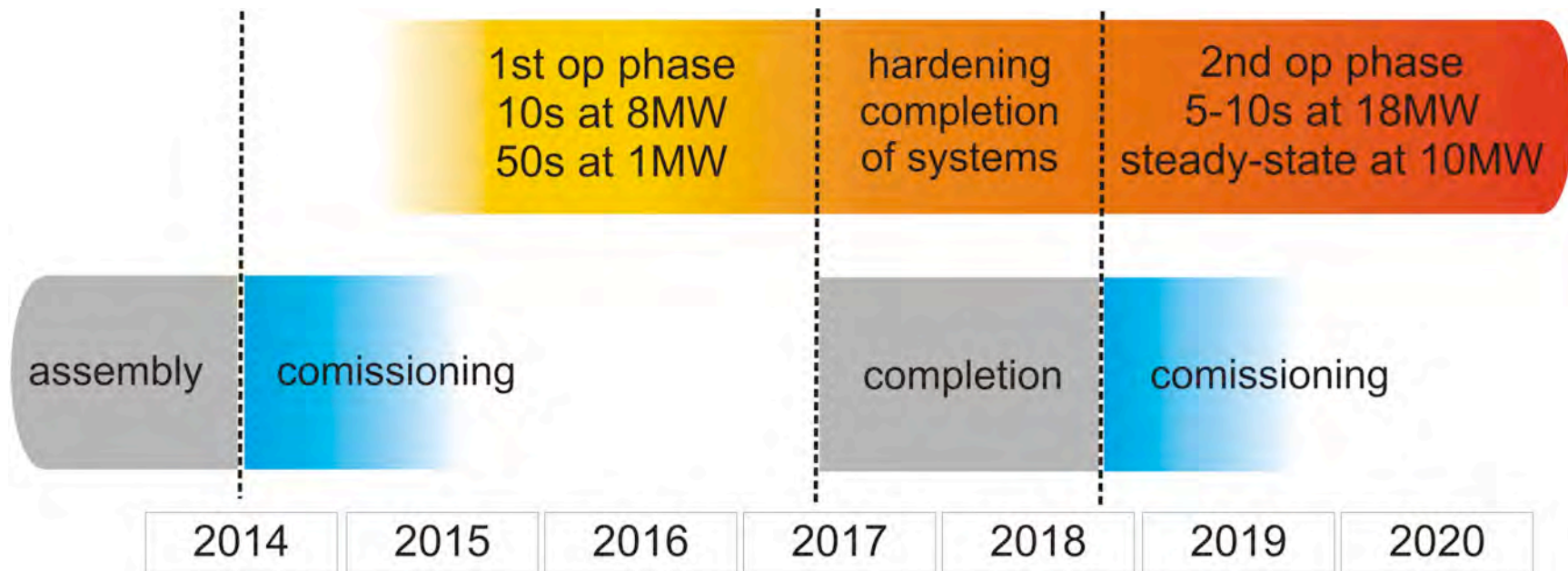


The completed first magnet module went into the next assembly stand

Schedule

- completion date 2014
- 68 weeks buffer time
- 29 milestones
- tight schedule control

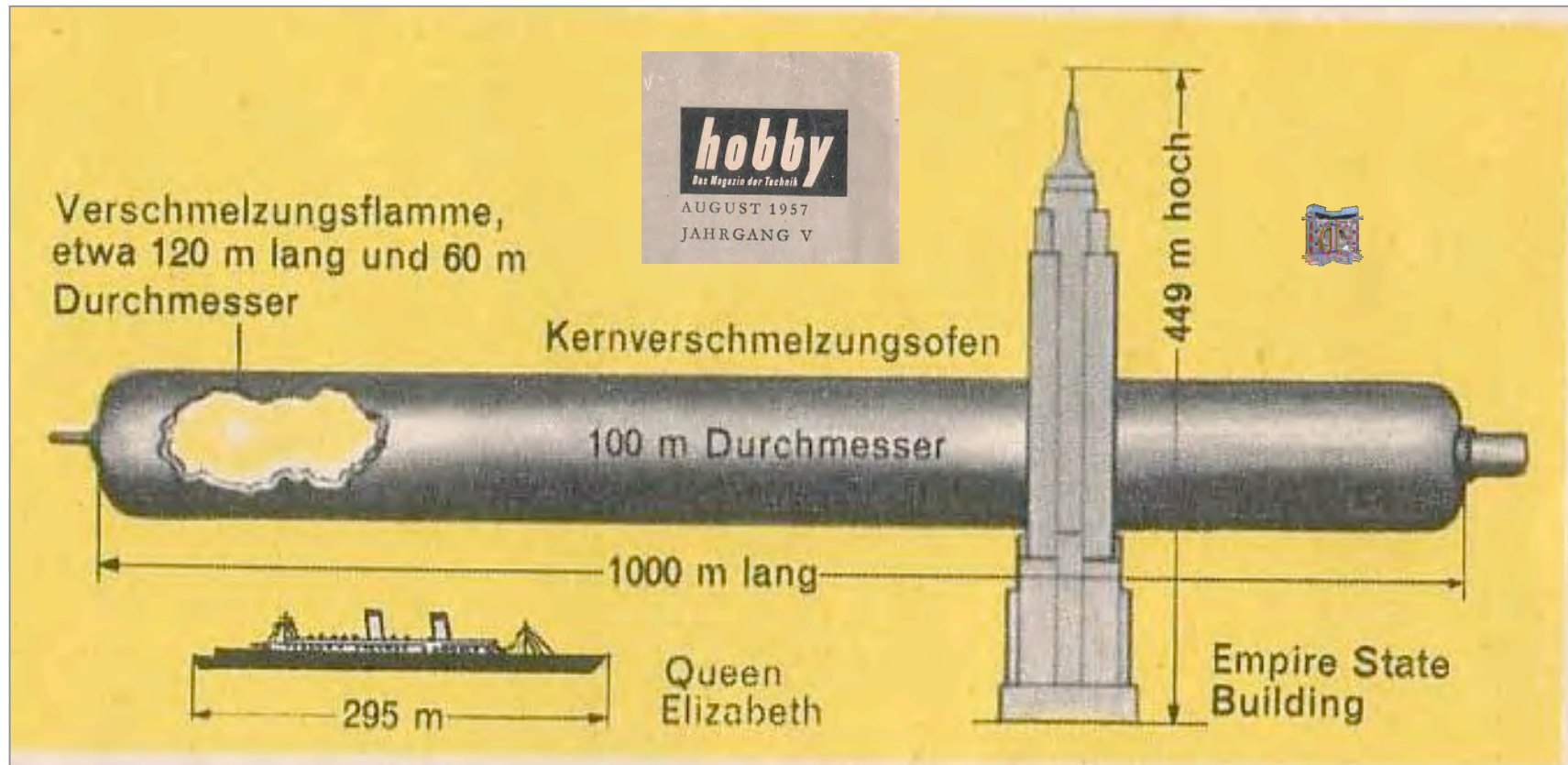
Nr.	Vorgangname	Anfang	Ende	Dauer	Timeline (2006-2020)																											
					06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	H2	H1	H2	H1	H2	H1	H2	H1	H2	H1	H2	H1	H2
0	Ablaufplan der Montage (Technologische Sequenz)	Mo 21.03.05	Mo 19.05.14	464,5 W	[Gantt bar]																											
1	MST 0: TOSKA operational	Di 01.04.08	Di 01.04.08	0 W	[Milestone diamond]																											
2	1. Module (#5)	Mo 21.03.05	Fr 14.12.12	393,5 W	[Gantt bar]																											
3	2. Module (#4)	Mo 21.03.05	Mi 13.02.08	150 W	[Gantt bar]																											
4	3. Module (#3)	Mo 09.05.05	Mi 06.02.08	142 W	[Gantt bar]																											
5	4. Module (#2)	Mi 13.02.08	Mi 05.03.08	3 W	[Gantt bar]																											
6	5. Module (#1)	Mi 05.03.08	Mi 05.03.08	0 W	[Gantt bar]																											
7	Final adjustment of modules	Mi 05.03.08	Mi 30.04.08	7,5 W	[Gantt bar]																											
8	Module connections (parallel work)	Mi 30.04.08	Di 26.08.08	16,5 W	[Gantt bar]																											
9	1-2 connection of modules #5-#1	Di 26.08.08	Mo 03.11.08	9,5 W	[Gantt bar]																											
10	1-3 connection of modules #5-#4	Mo 03.11.08	Sa 07.02.09	13 W	[Gantt bar]																											
11	4-2 connection of modules #1-#2	Sa 07.02.09	Sa 07.02.09	0 W	[Gantt bar]																											
12	4-5 connection of modules #2-#3	Sa 07.02.09	Sa 28.02.09	3 W	[Gantt bar]																											
13	5-3 connection of modules #4-#3	Sa 28.02.09	Sa 25.04.09	7,5 W	[Gantt bar]																											
14	Contingency module connection 5 W (from risk analysis)	Sa 25.04.09	Mo 18.05.09	3 W	[Gantt bar]																											
15	MST 5: All modules connected	Mo 18.05.09	Mo 18.05.09	0 W	[Milestone diamond]																											
16	Completion of torus	Mo 18.05.09	Mo 05.10.09	19,5 W	[Gantt bar]																											
17	Completion OV (ports and domes in support openings)	Mo 21.12.09	Mo 26.04.10	7,58 W	[Gantt bar]																											
18	MST 10: Completion of cryostat	Mo 26.04.10	Mo 26.04.10	0 W	[Milestone diamond]																											
19	Installation current leads	Mi 06.01.10	Fr 09.04.10	5,67 W	[Gantt bar]																											
20	Completion of Periphery (cables (25W), piping, vacuum...)	Mo 26.04.10	Do 01.07.10	4 W	[Gantt bar]																											
21	KIP 4. Part	Do 01.07.10	Do 05.08.10	5 W	[Gantt bar]																											
22	Contingency KIP (design not yet finished)	Do 05.08.10	Do 05.08.10	0 W	[Gantt bar]																											
23	MST 13: KIP assembly in 1st module finished (parts 1 and 2)	Do 05.08.10	Do 05.08.10	0 W	[Milestone diamond]																											
24	1. Module, part 3 of in-vessel components (module plane)	Do 22.11.12	Fr 14.12.12	1,42 W	[Gantt bar]																											
25	Module piping, vacuum	Mo 05.10.09	Di 15.12.09	10 W	[Gantt bar]																											
26	1. Module connection with supply systems	Mi 16.03.11	Mi 16.03.11	0 W	[Gantt bar]																											
27	2. Module (#1)	Mi 27.02.08	Mi 28.11.12	239,26 W	[Gantt bar]																											
28	3. Module (#4)	Mi 17.09.08	Do 08.11.12	208,12 W	[Gantt bar]																											
29	4. Module (#2)	Mi 15.04.09	Do 05.09.13	221,13 W	[Gantt bar]																											
30	5. Module (#3)	Do 05.11.09	Fr 30.08.13	191,99 W	[Gantt bar]																											
31	Final adjustment of modules	Do 10.02.11	Do 10.03.11	4 W	[Gantt bar]																											
32	Module connections (parallel work)	Mi 30.05.12	Mi 12.12.12	27,7 W	[Gantt bar]																											
33	1-2 connection of modules #5-#1	Mi 30.05.12	Mi 21.11.12	24,8 W	[Gantt bar]																											
34	1-3 connection of modules #5-#4	Mi 30.05.12	Di 23.10.12	20,7 W	[Gantt bar]																											
35	4-2 connection of modules #1-#2	Mi 30.05.12	Sa 10.11.12	23,3 W	[Gantt bar]																											
36	4-5 connection of modules #2-#3	Mi 30.05.12	Fr 26.10.12	21,3 W	[Gantt bar]																											
37	5-3 connection of modules #4-#3	Mi 30.05.12	Mi 07.11.12	22,7 W	[Gantt bar]																											
38	Contingency module connection 5 W (from risk analysis)	Mi 07.11.12	Mi 12.12.12	5 W	[Gantt bar]																											
39	MST 25: All modules connected	Mi 12.12.12	Mi 12.12.12	0 W	[Milestone diamond]																											
40	Completion of torus	Di 21.12.10	Mo 19.05.14	171,1 W	[Gantt bar]																											
41	Completion OV (ports and domes in support openings)	Mo 18.02.13	Mi 03.07.13	18,4 W	[Gantt bar]																											
42	MST 27: Completion of cryostat	Mi 03.07.13	Mi 03.07.13	0 W	[Milestone diamond]																											
43	Installation current leads	Mi 03.07.13	Mo 19.08.13	6,7 W	[Gantt bar]																											
44	Completion of Periphery (cables (25W), piping, vacuum...)	Mi 03.07.13	Mi 29.01.14	29 W	[Gantt bar]																											
45	KIP 4. Part	Fr 30.08.13	Mi 20.11.13	11,41 W	[Gantt bar]																											
46	Contingency 15 W (from risk analysis)	Mi 29.01.14	Mo 19.05.14	15 W	[Gantt bar]																											
47	MST 26: Start of assembly ECRH	Mo 28.01.13	Mo 28.01.13	0 W	[Milestone diamond]																											
48	Module #5: Installation of ECRH	Mo 28.01.13	Sa 25.01.14	34 W	[Gantt bar]																											
49	Module #1: Installation of ECRH	Mo 28.01.13	Fr 24.01.14	34 W	[Gantt bar]																											
50	Installation ICRH in torus hall	Di 21.12.10	Di 10.05.11	19 W	[Gantt bar]																											
51	Assembly ICRH	Mo 19.08.13	Mo 13.01.14	20 W	[Gantt bar]																											
52	Completion of NBI boxes in assembly hall	Di 21.12.10	Fr 18.03.11	12 W	[Gantt bar]																											
53	Assembly NBI 1. Part	Mo 27.06.11	Sa 07.07.12	52 W	[Gantt bar]																											
54	Assembly NBI 2. Part	Mi 30.01.13	Mi 29.01.14	33,31 W	[Gantt bar]																											
55	MST 29: Start Commissioning	Mo 19.05.14	Mo 19.05.14	0 W	[Milestone diamond]																											



- **1st operation phase with 10s @ 8MW and 50s @ 1MW**
- **inertially cooled divertor and only partial cooling of in-vessel comp's**
- **shut-down (15 months) for completion and hardening**
- **2nd operation phase to approach 30min @ 10MW**
- **3rd operation phase with 10MW ECRH, 20MW NBI and 10MW ICRH**

- **„Fully“ optimized magnetic field configuration with simultaneously ...**
 - low equilibrium currents
 - good magnetohydrodynamic equilibria
 - good magnetohydrodynamic stability
 - good neoclassical confinement
 - good fast-particle confinement
- **First superconducting stellarator with modular magnetic field coils**
 - steady-state island divertor for full power load
 - steady-state 10MW 140GHz ECRH with quasi-optical wave guide
 - steady-state diagnostic and CoDaC system

A promising new high-temperature plasma device



Токмак (1951 Sacharov und Tamm) тороидальная камера в магнитных катушках „toroidal chamber in magnet coils“

