Aurora Australis Marine Science Cruise AU9404 - Oceanographic Field Measurements and Analysis

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ABSTRACT

Oceanographic measurements were conducted along WOCE Southern Ocean meridional section SR3 between Tasmania and Antarctica, and along the part of WOCE Southern Ocean zonal section S4 lying between approximately 110 and 162°E, from December 1994 to February 1995. An array of 4 current meter moorings at approximately 51°S in the vicinity of the SR3 line was successfully recovered. A total of 107 CTD vertical profile stations were taken, most to near bottom. Over 2380 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, chlorofluorocarbons, helium, tritium, dissolved inorganic carbon, alkalinity, carbon isotopes, dissolved organic carbon, dimethyl sulphide/dimethyl sulphoniopropionate, iodate/iodide, oxygen 18, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

1 INTRODUCTION

Marine science cruise AU9404, the third oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the Australian Antarctic Division vessel RSV Aurora Australis from December 1994 to February 1995. The major constituent of the cruise was the collection of oceanographic data relevant to the Australian Southern Ocean WOCE Hydrographic Program, along WOCE sections S4 (traversed west to east) and SR3 (traversed south to north) (Figure 1). The primary scientific objectives of this program are summarised in Rosenberg et al. (1995a). Section SR3 was occupied three times previously, in the spring of 1991 (Rintoul and Bullister, submitted), in the autumn of 1993 (Rosenberg et al., 1995a), and in the summer of 1993/94 (Rosenberg et al., 1995b). Zonal section S4 represents a circumnavigation of the globe in the Southern Ocean, with the various parts to be completed by different WOCE participants. The part of S4 completed on this cruise (Figure 1) was a first time occupation. At the western end of the S4 transect, seven of the stations were occupied by the Woods Hole Oceanographic Institute ship R.V. Knorr (M. McCartney, pers. comm.) several days prior to occupation by the Aurora Australis. These stations are intended to provide cross-calibrations for the tracer samples and CTD measurements collected by both vessels.

An array of four full depth current meter moorings, in the vicinity of the SR3 line at the latitude of the Subantarctic Front, was successfully recovered. The moorings had been deployed in the autumn of 1993 by the Aurora Australis, and at the time of writing, have since been redeployed in the same region by the SCRIPPS ship R.V. Melville as part of a larger mooring array (principal investigators Luther, D., Chave, A., Richman, J., Filloux, J., Rintoul, S. and Church, J.). Additional CTD measurements were made at the four mooring locations.

This report describes the collection of oceanographic data from the SR3 and S4 transects, and summarises the chemical analysis and data processing methods employed. Brief comparisons are also made with existing historical data. All information required for use of the data set is presented in tabular and graphical form.

2 CRUISE ITINERARY

The cruise commenced with recovery of one of the current meter moorings at ~50° 25'S (Table 4). Increasing winds prevented further recoveries, so it was decided to continue south leaving retrieval of the remaining moorings for the return leg to Hobart. En route to the Australian Antarctic base Casey, a deep water test CTD cast was conducted, and three CTD stations were occupied along the S4 transect. An upward looking sonar mooring (Bush, 1994) (Table 5) was recovered in the vicinity of Casey; an unsuccessful attempt was made to recover an additional upward looking sonar mooring. Following approximately a week of cargo operations at Casey, the S4 transect proper commenced at ~110°E. Due to time constraints, the originally planned station spacing of 30 nautical miles was increased to 45 nautical miles for most of the S4 transect. Included in the section were stations coinciding with the 7 stations occupied by the Knorr (stations 11, 12, 13, 14, 15, 16 and 17 in Table 2 correspond respectively with Knorr stations 85, 87, 88, 89, 90, 91 and 92). Also included were stations coinciding with locations sampled on the meridional sections SR3 and P11 (see Rosenberg et al., 1995a, for description of the P11 transect). Favourable sea ice and weather conditions permitted conclusion of S4 in 560 m of water just off Young Island in the Balleny Island group (Figure 1).

On the return west to the start of the SR3 section, a shallow test cast was conducted to test the Niskin bottles for CFC blank levels. The SR3 section commenced with 4 CTD stations at various locations on the shelf in the d'Urville Sea, beginning near Commonwealth Bay. Further north, between 61.3°S and 55.5°S, the station spacing was again increased from 30 to 45 nautical miles, due to further time constraints. Following recovery of the remaining 3 current meter moorings (Table 4) around the Subantarctic Front and additional CTD casts at these sites, the SR3 section was completed. A final CTD cast was conducted to test a suspect instrument before returning to Hobart.

Table 1: Summary of cruise itinerary.

Expedition Designation
Cruise AU9404 (cruise acronym WOCET), encompassing WOCE sections S4 and SR3

Chief Scientist Steve Rintoul, CSIRO

Ship RSV Aurora Australis

Ports of Call

Casey

Cruise Dates
December 13 1994 to February 2 1995

3.1 CTD casts and water samples

In the course of the cruise, 107 CTD casts were completed along the S4 and SR3 sections (Figure 1) (Table 2), plus additional locations, with most casts reaching to within 15 m of the sea floor (Table 2). Over 2380 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), chlorofluorocarbons, helium, tritium, dissolved inorganic carbon, alkalinity, carbon isotopes (¹⁴C and ¹³C), dissolved organic carbon, dimethyl sulphide/dimethyl sulphoniopropionate, iodate/iodide, ¹⁸O, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Table 3 provides a summary of samples drawn at each station. Principal investigators for the various water sampling programmes are listed in Table 6a. For all stations, the different samples were drawn in a fixed sequence, as discussed in section 4.1.3. The methods for drawing samples are discussed in section 4.1.4.

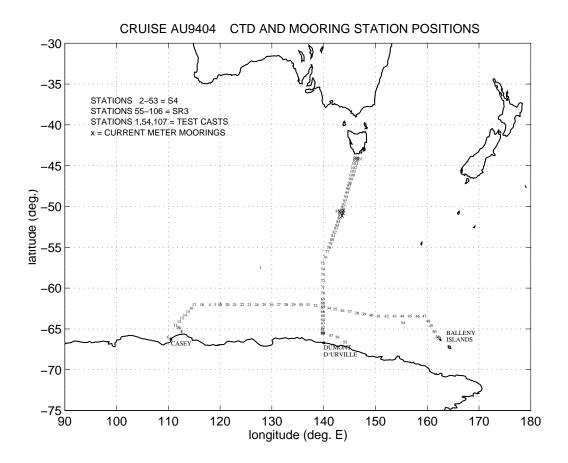


Figure 1: CTD station positions for RSV Aurora Australis cruise AU9404 along WOCE transects S4 and SR3, and current meter mooring locations.

Table 2 (following 3 pages): Summary of station information for RSV Aurora Australis cruise AU9404. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, TEST is a test cast. Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 1 to 18; CTD unit 5 (serial no. 1193) was used for stations 19 to 106; CTD unit 6 (serial no. 2568) was used for station 107.

| station | | ST | ART | | maxP | | BOT | TOM | | | | ENI | | |
|---------|---------------|-------------|--------------|---------|----------|------|-----------|--------------|----------|-----------|------|-----------|-------------|---------|
| number | time date | latitude | longitude de | epth(m) | (dbar) | time | latitude | longitude de | epth(m) | altimeter | time | latitude | longitude d | epth(m) |
| | | | 9 | 1 7 | (2.2.2.) | | | <u> </u> | -1 - (/ | | | | J | -1 () |
| 1 TEST | 0023 20-DEC-9 | 4 57:30.528 | 3 127:47.81E | 4690 | 4308 | 0311 | 57:32.11S | 127:49.47E | _ | _ | 0355 | 57:32.32S | 127:50.31E | 4700 |
| 2 S4 | 1531 21-DEC-9 | | | | 4186 | | | 120:01.68E | 4170 | - | | | 120:01.76E | 4170 |
| 3 S4 | 2147 21-DEC-9 | | | | 4266 | | | 119:02.14E | | - | 0115 | 62:01.00S | 119:04.59E | 4215 |
| 4 S4 | 0556 22-DEC-9 | 4 61:59.97 | S 118:00.14E | 4260 | 4304 | 0752 | 62:00.308 | 118:01.60E | 4260 | - | 0949 | 62:00.81S | 118:03.48E | 4260 |
| 5 S4 | 1206 2-JAN-9 | 5 66:15.84 | S 110:22.41E | 203 | 182 | 1215 | 66:15.79S | 110:22.35E | - | 20.0 | 1223 | 66:15.73S | 110:22.42E | 199 |
| 6 S4 | 1439 2-JAN-9 | 5 65:59.05 | S 109:54.21E | 255 | 192 | 1516 | 65:59.26S | 109:54.96E | 183 | 9.7 | 1544 | 65:59.51S | 109:55.07E | 158 |
| 7 S4 | 1412 3-JAN-9 | 5 65:23.42 | S 112:33.55E | 482 | 644 | 1457 | 65:23.10S | 112:33.20E | 656 | 17.4 | 1548 | 65:22.73S | 112:32.86E | 737 |
| 8 S4 | 1750 3-JAN-9 | 5 65:18.37 | S 112:32.75E | 1170 | 1120 | 1835 | 65:18.52S | 112:32.25E | 1157 | 13.7 | 1939 | 65:17.89S | 112:32.04E | 1164 |
| 9 S4 | 2354 3-JAN-9 | 5 64:57.93 | S 112:10.14E | 2310 | 2284 | 0115 | 64:57.66S | 112:09.60E | 2315 | 13.1 | 0224 | 64:57.44S | 112:09.31E | 2321 |
| 10 S4 | 0416 4-JAN-9 | | | 2250 | 2274 | | | 111:55.05E | 2300 | 9.5 | | | 111:54.89E | 2300 |
| 11 S4 | 1002 4-JAN-9 | | | 2900 | 2866 | 1127 | 64:30.87S | 111:25.77E | 2860 | 13.5 | | | 111:27.38E | 2860 |
| 12 S4 | 1606 4-JAN-9 | | | 2360 | 2304 | | | 112:05.92E | 2315 | 11.0 | 1829 | 64:06.20S | 112:06.66E | 2290 |
| 13 S4 | 2057 4-JAN-9 | 5 63:41.02 | S 112:36.06E | 3358 | 3364 | 2226 | 63:40.80S | 112:36.48E | 3360 | 12.2 | 0001 | 63:40.28S | 112:35.89E | 3365 |
| 14 S4 | 0308 5-JAN-9 | 5 63:16.51 | S 113:12.28E | 3590 | 3596 | 0441 | 63:16.50S | 113:13.00E | - | 13.5 | 0628 | 63:16.69S | 113:13.49E | - |
| 15 S4 | 1112 5-JAN-9 | 5 62:50.95 | S 113:48.94E | 3450 | 3494 | 1220 | 62:50.82S | 113:49.10E | - | - | 1348 | 62:50.58S | 113:49.06E | - |
| 16 S4 | 1713 5-JAN-9 | 5 62:25.17 | S 114:26.07E | 4080 | 4118 | | | 114:25.68E | | 12.9 | 2026 | 62:25.95S | 114:25.45E | 4080 |
| 17 S4 | 2304 5-JAN-9 | | | 4250 | 4286 | 0033 | 62:00.03S | 115:01.00E | 4255 | 12.6 | 0214 | 62:00.09S | 115:02.40E | 4245 |
| 18 S4 | 0607 6-JAN-9 | 5 62:00.17 | S 116:29.70E | 4250 | 4290 | 0744 | 61:59.698 | 116:30.46E | 4250 | 14.0 | 0936 | 61:59.70S | 116:31.81E | 4250 |
| 19 S4 | | | | 4180 | 4220 | 1914 | 62:00.32S | 120:01.36E | 4175 | 12.9 | 2049 | 62:00.48S | 120:02.95E | 4182 |
| 20 S4 | 0001 7-JAN-9 | 5 62:00.02 | S 121:24.93E | 4153 | 4174 | 0139 | 61:59.80S | 121:26.89E | 4150 | 13.2 | 0331 | 61:59.70S | 121:28.11E | 4140 |
| 21 S4 | 0711 7-JAN-9 | | | 4250 | 4290 | | | 122:50.44E | | 5.5 | 1031 | 62:00.54S | 122:51.60E | 4250 |
| 22 S4 | 1356 7-JAN-9 | 5 61:59.91 | S 124:14.98E | 4267 | 4306 | 1520 | 62:00.11S | 124:15.38E | 4265 | 7.1 | 1704 | 62:00.66S | 124:15.49E | 4265 |
| 23 S4 | 2027 7-JAN-9 | 5 61:59.92 | S 125:39.57E | 4338 | 4378 | 2211 | 62:00.22S | 125:39.58E | 4337 | 18.1 | 2349 | 62:00.34S | 125:39.54E | 4335 |
| 24 S4 | 0328 8-JAN-9 | | | 4360 | 4410 | | | 127:05.46E | 4365 | 17.0 | | | 127:05.55E | 4360 |
| 25 S4 | 1033 8-JAN-9 | 5 62:00.04 | S 128:29.96E | 4400 | 4448 | 1221 | 62:00.73S | 128:31.57E | 4400 | 12.3 | 1406 | 62:01.23S | 128:32.95E | 4400 |
| 26 S4 | 1709 8-JAN-9 | | | 4490 | 4540 | | | 129:56.74E | 4495 | 15.6 | 2041 | 62:00.70S | 129:58.36E | 4499 |
| 27 S4 | 0008 9-JAN-9 | 5 62:00.07 | S 131:19.79E | 4530 | 4586 | 0150 | 62:00.57S | 131:20.04E | 4540 | 15.0 | 0329 | 62:01.08S | 131:20.45E | 4540 |
| 28 S4 | 0704 9-JAN-9 | | | 4460 | 4514 | 0858 | 61:59.92S | 132:45.64E | 4460 | 17.6 | 1054 | 62:00.09S | 132:46.83E | 4460 |
| 29 S4 | 1454 9-JAN-9 | 5 62:01.23 | S 134:10.49E | 4370 | 4414 | 1634 | 62:01.41S | 134:11.11E | 4370 | 12.4 | 1826 | 62:01.30S | 134:11.22E | 4370 |
| 30 S4 | 2205 9-JAN-9 | 5 62:00.19 | S 135:35.04E | 4335 | 4376 | 2359 | 62:00.35S | 135:35.07E | 4330 | 11.9 | 0151 | 61:59.81S | 135:35.31E | - |
| 31 S4 | 0611 10-JAN-9 | 5 61:59.99 | S 137:00.09E | 3900 | 3964 | 0800 | 61:59.94S | 137:01.31E | 3850 | 13.7 | 0949 | 61:59.34S | 137:01.14E | 3900 |
| 32 S4 | 1311 10-JAN-9 | 5 62:10.08 | S 138:24.63E | 3990 | 4036 | | | 138:27.19E | | 14.7 | 1650 | 62:09.01S | 138:29.60E | 4031 |
| 33 S4 | 2009 10-JAN-9 | 5 62:21.05 | S 139:51.96E | 3950 | 3994 | 2155 | 62:21.54S | 139:53.39E | 3970 | 13.2 | 2343 | 62:22.09S | 139:53.47E | 3960 |
| 34 S4 | 0357 11-JAN-9 | 5 62:28.75 | S 141:01.77E | 4180 | 4230 | 0638 | 62:28.15S | 141:03.29E | 4205 | 13.4 | 0820 | 62:27.38S | 141:04.32E | 4210 |
| 35 S4 | 1130 11-JAN-9 | 5 62:35.86 | S 142:11.92E | 4140 | 4170 | 1335 | 62:35.868 | 142:12.37E | 4140 | 14.9 | 1515 | 62:35.68S | 142:12.58E | 4140 |
| 36 S4 | 1925 11-JAN-9 | 5 62:45.08 | S 143:36.91E | 4110 | 4154 | 2118 | 62:45.83S | 143:36.16E | 4125 | 14.5 | 2300 | 62:46.56S | 143:36.82E | 4125 |

| station | START | maxP | BOTTOM | END |
|---------|---|--------|--|----------------------------------|
| number | time date latitude longitude depth(m) | (dbar) | time latitude longitude depth(m) altimeter | time latitude longitude depth(m) |
| | into date iditade iongitude depin(in) | (424.) | inite idinade iongrade depth(in) diminete. | inno iamado iongitudo dopin(in) |
| 37 S4 | 0215 12-JAN-95 62:53.96\$ 145:01.65E 4030 | 4058 | 0411 62:54.22\$ 145:03.26E 4030 13.1 | 0602 62:54.13S 145:04.60E 4030 |
| 38 S4 | 0910 12-JAN-95 63:03.00S 146:26.98E 3955 | 3982 | 1047 63:03.12S 146:27.96E 3955 14.6 | 1238 63:03.43S 146:29.37E 3955 |
| 39 S4 | 1541 12-JAN-95 63:11.17S 147:50.05E 3915 | 3940 | 1728 63:10.65S 147:50.90E 3920 16.0 | 1858 63:10.33\$ 147:51.15E 3920 |
| 40 S4 | 2227 12-JAN-95 63:18.27S 149:11.87E 3810 | 3820 | 0006 63:18.64S 149:12.55E 3780 12.6 | 0150 63:18.82S 149:12.47E 3800 |
| 41 S4 | 0502 13-JAN-95 63:25.89\$ 150:38.93E 3765 | 3780 | 0634 63:25.89S 150:39.78E 3755 10.1 | 0805 63:25.59\$ 150:39.75E 3755 |
| 42 S4 | 1116 13-JAN-95 63:26.03S 152:10.57E 3680 | 3694 | 1250 63:25.64S 152:10.83E 3680 16.5 | 1439 63:25.24\$ 152:10.98E 3680 |
| 43 S4 | 1749 13-JAN-95 63:26.11S 153:41.67E 3125 | 3122 | 1902 63:26.19S 153:41.41E 3110 13.3 | 2019 63:26.25S 153:40.98E 3115 |
| 44 S4 | 2323 13-JAN-95 63:26.10S 155:10.47E 2960 | 3108 | 0052 63:26.10S 155:10.90E 3116 13.6 | 0212 63:25.77S 155:11.32E 3135 |
| 45 S4 | 0525 14-JAN-95 63:26.01S 156:39.18E 3230 | 3226 | 0656 63:25.85S 156:39.08E 3230 17.4 | 0812 63:25.75S 156:39.11E 3230 |
| 46 S4 | 1147 14-JAN-95 63:26.03S 158:10.12E 2550 | 2638 | 1308 63:26.03S 158:09.91E - 19.0 | 1418 63:25.62S 158:09.43E - |
| 47 S4 | 1917 14-JAN-95 63:25.74S 159:26.55E 2710 | 1020 | 1956 63:25.64S 159:26.43E 2710 - | 2010 63:25.49S 159:26.69E 2700 |
| 48 S4 | 0149 15-JAN-95 64:00.62\$ 160:10.96E 2880 | 2844 | 0302 64:00.89S 160:10.71E 2870 20.7 | 0418 64:01.29S 160:11.02E 2870 |
| 49 S4 | 0949 15-JAN-95 64:37.34\$ 160:43.55E 3050 | 3088 | 1113 64:37.32S 160:44.28E 3070 14.8 | 1241 64:36.91S 160:45.12E 3130 |
| 50 S4 | 2005 15-JAN-95 65:17.95S 161:24.01E 3100 | 3096 | 2120 65:18.04S 161:23.80E 3100 13.8 | 2246 65:18.20S 161:23.80E 3100 |
| 51 S4 | 0527 16-JAN-95 65:56.27S 162:03.08E 2970 | 2964 | 0648 65:56.02S 162:03.34E 2970 17.1 | 0803 65:55.52S 162:03.49E 2970 |
| 52 S4 | 1042 16-JAN-95 66:06.84S 162:14.65E 1510 | 1552 | 1150 66:06.67S 162:14.18E 1510 14.6 | 1259 66:06.41S 162:13.83E 1560 |
| 53 S4 | 1443 16-JAN-95 66:09.13S 162:15.49E 567 | 550 | 1505 66:09.10S 162:15.34E 568 11.0 | 1533 66:09.03S 162:15.18E 572 |
| 54 TEST | 0301 18-JAN-95 64:13.75S 155:19.95E 3210 | 1038 | 0345 64:13.93S 155:19.70E 3210 - | 0417 64:14.00S 155:19.65E 3210 |
| 55 SR3 | 0525 19-JAN-95 66:35.97S 144:09.76E 850 | 812 | 0556 66:36.28S 144:09.63E 850 17.1 | 0640 66:36.84S 144:09.33E 850 |
| 56 SR3 | 1412 19-JAN-95 66:00.55\$ 142:39.77E 455 | 436 | 1441 66:00.51S 142:39.20E 458 14.1 | 1505 66:00.64S 142:39.06E 460 |
| 57 SR3 | 1910 19-JAN-95 65:50.53S 141:25.71E 332 | 308 | 1920 65:50.58S 141:25.58E 329 14.6 | 1950 65:50.44S 141:24.97E 335 |
| 58 SR3 | 2312 19-JAN-95 65:34.98\$ 139:51.24E 595 | 526 | 2338 65:35.12S 139:50.37E 528 11.5 | 0013 65:35.43S 139:49.25E 436 |
| 59 SR3 | 0137 20-JAN-95 65:32.24S 139:51.19E 1300 | 1242 | 0234 65:32.49S 139:51.11E 1300 17.4 | 0337 65:32.58\$ 139:50.69E 1260 |
| 60 SR3 | 0444 20-JAN-95 65:25.93S 139:50.77E 1875 | 1988 | 0550 65:26.26S 139:50.68E 1950 19.2 | 0654 65:26.48S 139:51.07E - |
| 61 SR3 | 0905 20-JAN-95 65:04.98\$ 139:50.83E 2795 | 2750 | 1020 65:04.75\$ 139:51.64E 2680 17.5 | 1131 65:04.35\$ 139:52.41E 2590 |
| 62 SR3 | 1304 20-JAN-95 64:49.03\$ 139:50.94E 2600 | 2570 | 1417 64:49.40\$ 139:49.38E 2585 12.0 | 1538 64:50.10S 139:47.95E 2530 |
| 63 SR3 | 1819 20-JAN-95 64:16.92S 139:52.08E 3470 | 3472 | 1930 64:17.16S 139:51.31E 3465 11.8 | 2047 64:17.20S 139:51.36E 3465 |
| 64 SR3 | 2301 20-JAN-95 63:51.92S 139:50.81E 3743 | 3758 | 0042 63:51.57\$ 139:52.15E 3748 13.9 | 0242 63:51.27S 139:54.55E 3748 |
| 65 SR3 | 0528 21-JAN-95 63:21.19S 139:50.91E 3820 | 3832 | 0653 63:21.70\$ 139:50.47E 3810 13.0 | 0828 63:22.16S 139:51.22E 3810 |
| 66 SR3 | 1051 21-JAN-95 62:51.09S 139:50.70E 3220 | 3224 | 1216 62:50.85S 139:51.08E 3230 17.0 | 1348 62:50.61S 139:51.54E 3250 |
| 67 SR3 | 1659 21-JAN-95 62:20.78\$ 139:50.44E 3970 | 3988 | 1821 62:20.45S 139:49.66E 3960 15.4 | 1946 62:20.20S 139:49.60E 3960 |
| 68 SR3 | 2215 21-JAN-95 61:50.98\$ 139:51.26E 4300 | 4338 | 0001 61:51.09S 139:51.16E 4301 15.1 | 0145 61:51.32S 139:51.11E 4300 |
| 69 SR3 | 0426 22-JAN-95 61:21.06S 139:51.48E 4340 | 4390 | 0608 61:21.89S 139:53.30E 4340 14.9 | 0744 61:22.57S 139:54.52E 4345 |
| 70 SR3 | 1124 22-JAN-95 60:35.99\$ 139:50.67E 4440 | 4472 | 1258 60:36.15S 139:49.93E 4435 14.1 | 1449 60:35.91S 139:48.93E 4430 |
| 71 SR3 | 1815 22-JAN-95 59:50.90S 139:50.94E 4485 | 4532 | 2006 59:50.88\$ 139:51.78E 4480 11.0 | 2139 59:51.12S 139:52.93E 4480 |
| 72 SR3 | 0121 23-JAN-95 59:05.96S 139:51.25E 3950 | 3954 | 0308 59:05.67S 139:51.61E 3905 12.9 | 0440 59:05.94S 139:51.86E 3925 |

| station | START | | maxP | ВО | TTOM | | | | ENI |) | |
|---------|------------------------------|------------------|--------|---------------|--------------|---------|-----------|------|-----------|--------------|---------|
| number | time date latitude lon | ngitude depth(m) | (dbar) | time latitude | longitude de | epth(m) | altimeter | time | latitude | longitude de | epth(m) |
| | | . , , | , | | <u> </u> | | | | | <u> </u> | , , , |
| 73 SR3 | 0818 23-JAN-95 58:21.11S 139 |):51.22E 4000 | 4082 | 0944 58:21.07 | S 139:51.71E | 4020 | 12.1 | 1103 | 58:20.91S | 139:52.44E | 4000 |
| 74 SR3 | 1734 23-JAN-95 57:38.75S 139 |):51.77E 4250 | 4134 | 1921 57:38.83 | S 139:52.72E | - | 16.4 | 2055 | 57:38.99S | 139:53.62E | - |
| 75 SR3 | 0400 24-JAN-95 56:55.80S 139 | :49.74E 4100 | 4066 | 0551 56:56.10 | S 139:49.69E | - | - | 0726 | 56:56.07S | 139:50.39E | - |
| 76 SR3 | 1258 24-JAN-95 56:12.73S 140 |):17.60E 3620 | 3658 | 1433 56:12.03 | S 140:17.54E | - | 15.1 | 1609 | 56:11.60S | 140:17.12E | - |
| 77 SR3 | 1935 24-JAN-95 55:30.06S 140 | :44.00E 3915 | 4186 | 2116 55:30.07 | S 140:44.29E | - | 19.9 | 2243 | 55:30.03S | 140:44.65E | - |
| 78 SR3 | 0154 25-JAN-95 55:00.82S 141 | :00.81E 3300 | 3164 | 0323 55:00.48 | S 141:00.91E | 3200 | 16.1 | 0442 | 55:00.58S | 141:00.81E | 3200 |
| 79 SR3 | 0712 25-JAN-95 54:32.38S 141 | :19.09E 2850 | 2784 | 0842 54:31.26 | S 141:19.08E | 2825 | 17.4 | 0947 | 54:30.95S | 141:18.25E | 2910 |
| 80 SR3 | 1224 25-JAN-95 54:03.87S 141 | :35.86E 2600 | 2732 | 1351 54:03.33 | S 141:36.00E | 2720 | 17.5 | 1511 | 54:02.98S | 141:35.93E | 2720 |
| 81 SR3 | 1753 25-JAN-95 53:35.18S 141 | :52.10E 2590 | 2542 | 1912 53:34.95 | S 141:53.05E | 2490 | 15.9 | 2016 | 53:35.00S | 141:53.20E | 2515 |
| 82 SR3 | 2305 25-JAN-95 53:07.90S 142 | 2:08.18E 3125 | 3142 | 0015 53:07.52 | S 142:08.51E | 3150 | 16.1 | 0130 | 53:07.48S | 142:08.64E | 3150 |
| 83 SR3 | 0402 26-JAN-95 52:40.06S 142 | 2:23.46E 3400 | 3396 | 0525 52:40.31 | S 142:24.37E | 3400 | 10.1 | 0649 | 52:40.48S | 142:24.41E | 3390 |
| 84 SR3 | 0906 26-JAN-95 52:15.97S 142 | 2:38.13E 3500 | 3532 | 1008 52:15.82 | S 142:38.72E | 3500 | 13.6 | 1118 | 52:16.00S | 142:40.31E | 3520 |
| 85 SR3 | 1336 26-JAN-95 51:51.13S 142 | 2:50.05E 3620 | 3650 | 1517 51:51.45 | S 142:51.75E | 3610 | 14.1 | 1650 | 51:51.78S | 142:52.86E | 3615 |
| 86 SR3 | 0950 27-JAN-95 51:26.06S 143 | 3:02.99E 3730 | 3782 | 1113 51:25.95 | S 143:03.69E | 3750 | 13.0 | 1237 | 51:26.29S | 143:03.88E | 3710 |
| 87 SR3 | 1752 27-JAN-95 50:33.31S 142 | 2:41.33E 3830 | 3844 | 1938 50:33.09 | S 142:43.09E | 3800 | 14.8 | | | 142:44.91E | - |
| 88 SR3 | 0635 28-JAN-95 51:01.97S 143 | 3:13.93E 3800 | 3892 | 0814 51:02.60 | S 143:13.85E | - | 11.3 | 0927 | 51:02.71S | 143:13.74E | - |
| 89 SR3 | 1121 28-JAN-95 50:43.05S 143 | 3:24.06E 3650 | 3726 | 1250 50:43.21 | S 143:24.39E | 3650 | 13.2 | 1424 | 50:43.53S | 143:24.69E | 3665 |
| 90 SR3 | 1647 28-JAN-95 50:24.88S 143 | | 3604 | 1822 50:25.23 | | 3608 | 15.5 | | | 143:33.82E | - |
| 91 SR3 | 2151 28-JAN-95 50:05.08S 143 | | 4038 | 2350 50:04.80 | | - | 16.7 | | | 143:45.64E | - |
| 92 SR3 | 0318 29-JAN-95 49:44.03S 143 | | 3502 | 0450 49:43.11 | | 3400 | 19.9 | | | 143:54.66E | 3510 |
| 93 SR3 | 1155 29-JAN-95 49:16.03S 144 | | 4346 | 1345 49:15.50 | | - | 16.5 | | | 144:09.02E | - |
| 94 SR3 | 1818 29-JAN-95 48:47.02S 144 | | 4218 | 2015 48:46.58 | | | 15.8 | | | 144:19.40E | 4140 |
| 95 SR3 | 0153 30-JAN-95 48:18.66S 144 | | 4070 | 0337 48:18.45 | | | 4.4 | | | 144:33.03E | 4095 |
| 96 SR3 | 0745 30-JAN-95 47:48.04S 144 | | 3932 | 0931 47:47.88 | | 3850 | 9.9 | | | 144:45.82E | 3850 |
| 97 SR3 | 1238 30-JAN-95 47:27.94S 144 | | 4354 | 1432 47:27.23 | | - | 14.6 | | | 144:53.94E | - |
| 98 SR3 | 1852 30-JAN-95 47:09.06S 145 | | 4012 | 2039 47:09.04 | | - | 16.4 | - | | 145:02.97E | - |
| 99 SR3 | 0041 31-JAN-95 46:38.89S 145 | | 3374 | 0215 46:38.16 | | | 14.7 | | | 145:14.88E | 3350 |
| 100 SR3 | 0545 31-JAN-95 46:09.92S 145 | | 2778 | 0658 46:09.22 | | | 17.3 | | | 145:27.54E | 2770 |
| 101 SR3 | 1019 31-JAN-95 45:41.77S 145 | | 1962 | 1130 45:41.64 | | 1875 | 19.5 | | | 145:40.21E | 1820 |
| 102 SR3 | 1438 31-JAN-95 45:13.01S 145 | | 2892 | 1601 45:13.40 | | - | 13.8 | _ | | | 2800 |
| 103 SR3 | 1948 31-JAN-95 44:42.98S 146 | | 3220 | 2119 44:42.58 | | | 15.1 | | | 146:01.16E | |
| 104 SR3 | 0043 1-FEB-95 44:22.95S 146 | | 2344 | 0157 44:22.98 | | | 14.1 | | | 146:11.02E | 2345 |
| 105 SR3 | 0431 1-FEB-95 44:06.89S 146 | | 1012 | 0522 44:07.16 | | | 17.2 | | | 146:13.26E | 1070 |
| 106 SR3 | 0707 1-FEB-95 44:00.00\$ 146 | | 228 | 0723 43:59.86 | | 255 | 10.1 | | | 146:19.06E | 255 |
| 107TEST | 1047 1-FEB-95 44:11.83S 146 | S:54.77E 1200 | 1142 | 1136 44:11.71 | S 146:55.01E | 1180 | 60.0 | 1226 | 44:12.08S | 146:55.15E | 1233 |

Table 3: Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), chlorofluorocarbons (CFC), helium/tritium (He/Tr), dissolved inorganic carbon (dic), alkalinity (alk), carbon isotopes (Ctope), dissolved organic carbon (doc), dimethyl sulphide/dimethyl sulphoniopropionate (dms), iodate/iodide (i), ¹⁸O, primary productivity (pp), "Seacat" casts (cat), and the following biological samples: pigments (pig), lugols iodine fixed plankton counts (lug), Coulter counter for particle sizing (cc), bacteria counts (bac), samples to determine presence of viruses inside algae (vir), flow cytometry (fc), video recording (vid), samples for culturing (cul), and transmission electron microscopy (te). Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle); and some biology samples taken from a surface bucket only. Also note that at stations 33, 50, 58, 67, 81 and 94, primary productivity samples were additionally filtered to measure d.o.c. content.

Table 3: (continued)

Table 3: (continued)

| | | | | | | | | | | | | | | | | bio | olog | ју | | | | |
|---------|-----|----|-------|-----|-------|---------|-------|------|------|------|-----------------|----|-----|-----|-----|-----|------|----|---|---|---|---|
| station | sal | do | nut (| CFC | He/Tr | dic/all | Ctope | e do | c dn | ns i | ¹⁸ O | pp | cat | pig | lug | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | |
| 98 SR3 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 99 SR3 | 1 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| 100 SR3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 101 SR3 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 102 SR3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 103 SR3 | 1 | 1 | 1 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 104 SR3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 105 SR3 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 106 SR3 | 1 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 107 TES | Γ1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

<u>Table 4:</u> Current meter moorings recovered along SR3 transect (positions given are at times of deployment). Recovery times are for last mooring component.

| site name | recovery time (UTC) | bottom depth (m) | latitude | longitude | current meter depths (m) | nearest CTD station no. |
|--------------|------------------------|---------------------|-------------------------|--------------------------|------------------------------------|-------------------------|
| SO2 | 03:52, 28/01/95 | 3770 | 50 ^o 33.19'S | 142 ⁰ 42.49'E | 300 600 1000 2000 3200 | 87 SR3 |
| SO3 | 00:42, 27/01/95 | 3800 | 51 ⁰ 01.54'S | 143 ⁰ 14.35'E | 300 600 1000 2000 3200 | 88 SR3 |
| SO4 | 05:57, 27/01/95 | 3580 | 50 ^o 42.73'S | 143 ⁰ 24.15'E | 300 600 1000 2000 3200 | 89 SR3 |
| SO5 | ~09:30, 15/12/9 | 4 3500 | 50 ^o 24.95'S | 143 ⁰ 31.97'E | 1000 2000 3200 | 90 SR3 |

<u>Table 5:</u> Upward looking sonar (ULS) mooring recovered (including current meter [CM]) (positions given are at times of deployment). Recovery time is for last mooring component.

| site name | recovery time (UTC) | bottom depth (m) | latitude | longitude | | rument ths (m) | CTD station no. |
|--------------|------------------------|---------------------|--------------------------|-------------------------|-----|-----------------------|-----------------|
| SOFAR | 01:15, 24/12/94 | 3260 | 63 ⁰ 17.746'S | 107 ⁰ 49.429 | 9'E | 150 (ULS) 200 (CM) | - |

3.2 Moorings recovered

An array of four current meter moorings was recovered (Table 4) along the SR3 transect line. A single upward looking sonar mooring was recovered near Casey; an unsuccessful attempt was made to locate a second upward looking sonar mooring (Table 5).

3.3 XBT/XCTD deployments

A total of 43 XBT and 26 XCTD deployments were made along the SR3 transect. The data were processed further by CSIRO Division of Oceanography (R. Bailey, pers. comm.). Results are not reported here.

3.4 Principal investigators

The principal investigators for the CTD and water sample measurements are listed in Table 6a. Cruise participants are listed in Table 6b.

<u>Table 6a:</u> Principal investigators (*=cruise participant) for water sampling programmes.

| measurement | name | affiliation |
|---|----------------------------------|--|
| CTD, salinity, O ₂ , nutrients chlorofluorocarbons | *Steve Rintoul John Bullister | CSIRO NOAA, U.S.A. |
| helium, tritium, ¹⁸ O | Peter Schlosser | Lamont-Doherty Earth Observatory, U.S.A. |
| D.I.C., alkalinity, carbon isotopes D.O.C. | Tom Trull | CSIRO Antarctic CRC |
| D.M.S. | Graham Jones | James Cook University |
| iodate/iodide | Ed Butler | CSIRO |
| primary productivity | John Parslow | CSIRO |
| biological sampling | *Simon Wright | Antarctic Division |

Table 6b: Scientific personnel (cruise participants).

| | - | | | |
|--|-------------|--|--------|--|
| name | | measurement | | affiliation |
| Ian Knott Simon Marsland Phil Morgan Steve Rintoul Mark Rosenberg Tim Vizer Andrew Woolf | | CTD, electronics CTD CTD CTD, moorings CTD, moorings CTD CTD | | Antarctic CRC Antarctic CRC CSIRO CSIRO Antarctic CRC Antarctic CRC Antarctic CRC |
| Steve Bell Ruth Eriksen Adam Leggett | | salinity, oxygen, nutrier salinity, oxygen, nutrier oxygen | | Antarctic CRC Antarctic CRC Melbourne University |
| Craig Neill David Wisegarver | | CFC CFC | | NOAA NOAA |
| Dee Breger | | helium, tritium, ¹⁸ O | | Lamont-Doherty Earth Observatory |
| Brendan Coutts Roger Dargaville Bronte Tilbrook | | D.I.C., alkalinity, C isoto D.I.C., alkalinity, C isoto D.I.C., alkalinity, C isoto | opes | Antarctic CRC Melbourne University CSIRO |
| Susannah Hunter | | D.O.C. | | Antarctic CRC |
| Mark Curran Megan McDonald | | D.M.S. D.M.S. | | James Cook University James Cook University |
| Anna Brandao | | iodate/iodide | | Antarctic CRC |
| Pru Bonham | | primary productivity | | CSIRO |
| Fiona Scott Peter Pendoley Simon Wright | deputy voya | biological sampling biological sampling age leader, biological san | npling | Antarctic Division Antarctic Division Antarctic Division |
| David James Tim Reid | | ornithology ornithology | | Australasian Ornithologists Union Australasian Ornithologists Union |
| Rob Easther Vera Hansper David Little Tim Osborne Andrew Tabor Mark Underwood | | voyage leader computing doctor computing gear officer, moorings electronics | | Antarctic Division |
| Adam Connolly | | reporter | | The Mercury |

4 FIELD DATA COLLECTION METHODS

4.1 CTD and hydrology measurements

In this section, CTD, hydrology, and ADCP data collection and processing methods are discussed. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 6.

4.1.1 CTD Instrumentation

The CTD instrumentation is described in Rosenberg et al. (1995b). Briefly, General Oceanics Mark IIIC (i.e. WOCE upgraded) CTD units were used. A 24 position rosette package, including a General Oceanics model 1015 pylon, and 10 litre General Oceanics Niskin bottles, was deployed for all casts. Deep sea reversing thermometers (Gohla-Precision) were mounted at rosette positions 2, 12 and 24. A Sea-Tech fluorometer and Li-Cor photosynthetically active radiation sensor were also attached to the package for some casts (Table 22).

4.1.2 CTD instrument and data calibration

Complete calibration information for the CTD pressure, platinum temperature and pressure temperature sensors are presented in Appendix 1. Pre cruise pressure and platinum temperature calibrations were available for all three CTD units, performed at the CSIRO Division of Oceanography Calibration Facility, with the exception of CTD unit 6, where manufacturer supplied platinum temperature calibration coefficients were used for the single test cast where this instrument was used. Pre cruise manufacturer supplied calibrations of the pressure temperature sensors were used for the cruise data. Note that readings from this sensor are applied in a correction formula for pressure data. The complete CTD conductivity and dissolved oxygen calibrations, derived respectively from the in situ Niskin bottle salinity and dissolved oxygen samples, are presented in a later section.

Manufacturer supplied calibrations were applied to the fluorescence and p.a.r. data (Appendix 1). These calibrations are not expected to be correct - correct scaling of fluorescence and p.a.r. data awaits linkage with primary productivity and Seacat (section 3.2) data.

The CTD and hydrology data processing and calibration techniques are described in detail in Appendix 2 of Rosenberg et al. (1995b) (referred to as "CTD methodology" for the remainder of the report). Note however the following updates to the methodology:

- (i) the 10 seconds of CTD data prior to each bottle firing are averaged to form the CTD upcast for use in calibration (5 seconds was used previously);
- (ii) the minimum number of data points required in a 2 dbar bin to form an average was set to 6 (i.e. jmin=6; for previous cruises, jmin=10);
- (iii) in the conductivity calibration for some stations, an additional term was applied to remove the pressure dependent conductivity residual;
- (iv) CTD raw data obtained from the CTD logging PC's no longer contain end of record characters after every 128 bytes.

4.1.3 CTD and hydrology data collection techniques

Data collection techniques are described in Rosenberg et al. (1995b). A fixed sequence was followed for the drawing of water samples on deck, as follows:

first sample: CFC

D.O.C

dissolved oxygen DMS/DMSP helium

D.I.C. alkalinity

carbon isotopes primary productivity

salinity nutrients iodate/iodide

¹⁸O

tritium

last sample: biology

(see Table 3 for a summary of which samples were drawn at each station).

4.1.4 Water sampling methods

The methods used for drawing the various water samples from the Niskin bottles are described here.

Chlorofluorocarbons: 100 ml samples are taken using precision ground glass syringes, following a series of rinses; care is taken to ensure bubble free samples.

Dissolved organic carbon: Sample jar volume = 250 ml (jars baked for 12 hours at 550°C) During d.o.c. sampling, polyethylene gloves were worn by the sampler. The gloves were changed every second sample.

- * rinse spiggot copiously with sample water
- * rinse sample jar twice
- * fill jar with ~200 ml and screw cap on tightly

After sampling, the jars are stored in the dark in a freezer at -18°C.

Dissolved oxygen: sample bottle volume = 150 ml

Bottles are washed and left partially filled with fresh water before use. Tight fitting silicon tubing is attached to the Niskin spiggot for sample drawing. Pickling reagent 1 is 3 M MnCl₂ (1.0 ml used); reagent 2 is 8 N NaOH/4 M NaI (1.0 ml used); reagent 3 is 10 N H₂SO₄ (1.0 ml used).

- * start water flow through tube for several seconds, making sure no bubbles remain in tube
- * pinch off flow in tube, and insert into bottom of sample bottle
- * let flow commence slowly into bottle, gradually increasing by releasing tubing, at all times ensuring no bubbles enter the sample and that turbulence is kept to a minimum
- * fill bottle, overflow by at least one full volume
- * pinch off tube and slowly remove so that bottle remains full to the brim, then rinse glass stopper
- * immediately pickle with reagents 1 then 2, inserting reagent dispenser at least 1 cm below water surface
- * insert glass stopper, ensuring no bubbles are trapped in sample
- * thoroughly shake sample (at least 30 vigorous inversions)
- * store samples in the dark until analysis
- * acidify samples with reagent 3 immediately prior to analysis

DMS and DMSP: Sample containers are quickly rinsed, then filled. For shallow samples only, a 750 ml amber glass bottle is used. For full profile sampling, samples for filtering are collected in 250 ml polyethylene screwcap jars; unfiltered samples are collected in 140 ml amber glass bottles.

Helium: Plastic tubing is attached to both ends of a 2 foot length of copper tubing, with one of the

the intake tube; the copper and plastic tube are struck to ensure no bubbles are trapped during filling. The plastic hoses are clamped, and the assembly removed to a hydraulic press where the copper tube is cut and crimped at either end, and in the middle.

Dissolved inorganic carbon: sample bottle volume = 250 ml

Tight fitting silicon tubing is attached to the Niskin spiggot for sample drawing. Samples are poisoned with 100 μl of a saturated solution of HgCl₂.

- * drain remaining old sample from the bottle
- * start water flow through tube for several seconds, making sure no bubbles remain in tube
- * insert tube into bottom of inverted sample bottle, allowing water to flush bottle for several seconds
- * pinch off flow in tube, and invert sample bottle to upright position, keeping tube in bottom of bottle
- * let flow commence slowly into bottle, gradually increasing, at all times ensuring no bubbles enter the sample
- * fill bottle, overflow by one full volume, and rinse cap
- * shake a small amount of water from top, so that water level is between threads and bottle shoulder
- * insert tip of poison dispenser just into sample, and poison
- * screw on cap, and invert bottle several times to allow poison to disperse through sample

Alkalinity: These are sampled and poisoned in the same fashion as dissolved inorganic carbon, except that 500 ml bottles are used.

Carbon Isotopes: These are sampled and poisoned in the same fashion as dissolved inorganic carbon, except that 500 ml glass stoppered vacuum flasks are used, and vacuum grease is placed around the stopper before inserting.

Primary productivity: Sampled from casts taken during daylight hours; samples were drawn for analysis of primary productivity and suspended particle size (taken from the shallowest four Niskin bottles). At most primary productivity sites, a Seabird "Seacat" CTD was deployed to obtain vertical profiles of photosynthetically active radiation (p.a.r.) and fluorescence from the top part of the water column. For primary productivity samples, 500 ml blacked out plastic jars are quickly rinsed then gently filled with ~400 ml of water through a length of tubing attached to the Niskin spiggot. Samples for particle size analysis are collected in 250 ml plastic bottles (with a single quick rinse prior to filling).

Salinity: sample bottle volume = 300 ml

- * drain remaining old sample from the bottle (bottles are always stored approximately 1/3 full with water between stations)
- * rinse bottle and cap 3 times with 100 ml of sample (shaking thoroughly each time); on each rinse, contents of sample bottle are poured over the Niskin bottle spiggot
- * fill bottle with sample, to bottle shoulder, and screw cap on firmly

At all filling stages, care is taken not to let the Niskin bottle spiggot touch the sample bottle.

Nutrients: sample tube volume = 12 ml

Two nutrient sample tubes are filled simultaneously at each Niskin bottle.

- * rinse tubes and caps 3 times
- * fill tubes
- * shake out water from tubes so that water level is at or below marking line 2 cm below top of tubes (10 ml mark), and screw on caps firmly

After sampling, one set of tubes are refrigerated for analysis within 12 hours; the duplicate set of tubes are placed in a freezer until required.

lodate: same as for nutrients

lodide: same as for nutrients, except 100 ml plastic bottle used.

¹⁸O: Sample bottle volume = 20 ml

Sample bottles given 3 quick rinses, then filled.

Tritium: 1 litre argon-filled bottles are filled to the top, minus headspace.

Biological sampling: Several different analyses were performed on the biological water samples, as listed in Table 3. Biological samples were usually drawn from the shallowest four or five Niskin bottles, with additional samples collected from a surface bucket.

4.1.5 Hydrology analytical methods

The analytical techniques and data processing routines employed in the Hydrographic Laboratory onboard the ship are discussed in Appendix 3 of Rosenberg et al. (1995b). Note the following changes to the methodology:

- (i) 150 ml sample bottles were used (300 ml bottles had been used previously), and 1.0 ml of reagents 1, 2 and 3 were used (2.0 ml used previously); the corresponding calculation value for the total amount of oxygen added with the reagents = 0.017 ml (0.034 ml previously);
- (ii) exact oxygen sample bottle volumes were individually measured, and applied for each individual bottle in the calculation of dissolved oxygen concentration.

4.2 Underway measurements

Throughout the cruise, the ship's data logging system continuously recorded bottom depth, ship's position and motion, surface water properties and meteorological information. All measurements were quality controlled during the cruise, to remove bad data (Ryan, 1995).

After quality controlling of the automatically logged GPS data set, gaps (due to missing data and data flagged as bad) are automatically filled by dead-reckoned positions (using the ship's speed and heading). Positions used for CTD stations are derived from this final GPS data set. Bottom depth is measured by a Simrad EA200 12 kHz echo sounder. A sound speed of 1498 ms⁻¹ is used for all depth calculations, and the ship's draught of 7.3 m has been accounted for in final depth values (i.e. depths are values from the surface).

Seawater is pumped on board via an inlet at 7 m below the surface. A portion of this water is diverted to the thermosalinograph (Aplied Microsystems Ltd, model STD-12), and to the fluorometer (Turner Design, peak sensitivity for chlorophyll-a). Sea surface temperatures are measured by a sensor next to the seawater inlet at 7 m depth.

The underway measurements for the cruise are contained in column formatted ascii files. The two file types are as follows (see Appendix 4 in Rosenberg et al., 1995b, for a complete description):

- (i) 10 second digitised underway measurement data, including time, latitude, longitude, depth and sea surface temperature;
- (ii) 15 minute averaged data, including time, latitude and longitude, air pressure, wind speed and direction, air temperature, humidity, quantum radiation, ship speed and heading, roll and pitch, sea surface salinity and temperature, average fluorescence, and seawater flow.

4.3 ADCP

A vessel mounted acoustic Doppler current profiler (ADCP) was installed in the hull during dry-docking of the ship in mid 1994. The unit is a high power 150 kHz narrow band ADCP produced by RD Instruments. The four transducer heads are mounted in a concave Janus configuration, with the beams 30 degrees off vertical, and with the transducers aligned at 45° to fore and aft. The transducers are mounted in a seachest ~7 m below the water surface, behind a 81 mm thick low density polyethylene window, with the window flush to the ship's hull. The inside of the seachest is lined with acoustic tiles (polyurethane with barytes and air microsphere fillers), and filled with

ADCP data were logged on a Sparc 5 Sun workstation. Logging parameters are listed in Table 7. An array of sounders is mounted on the ship for use in hydroacoustic biology surveys (T. Pauly, pers. comm.). When these sounders are in operation, firing of the ADCP is synchronised with the sounder trigger pulses, to avoid interference between the two systems. When this synchronisation is active, the ADCP ping rate is lowered by ~35%. When the ADCP system bottom tracking is active, the ping rate is decreased by ~50 %. Gyrocompass heading data were logged on the Sun through a synchro to digital converter, at a one second sampling frequency. GPS data collected by a Lowrance receiver were also logged by the Sun; the Lowrance unit received GPS positions every 2 seconds, and GPS velocities every 2 seconds, with positions and velocities received on alternate seconds. ADCP data processing is discussed in more detail in Dunn (a and b, unpublished reports).

<u>Table 7:</u> ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 50 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averageing: bins 3 to 6 (13/12/94-13/01/95 i.e. files 1-86)

bins 3 to 10 (13/01/95-21/01/95 i.e. files 87-107) bins 3 to 13 (21/01/95-01/02/95 i.e. files 108-136)

ensemble averageing duration: 3 min.

5 MAJOR PROBLEMS ENCOUNTERED

5.1 Logistics

The only significant logistic problem was shortage of time, due in part to delayed cargo operations at Casey. For part of the transects, as mentioned above, station spacing was increased to 45 nautical miles, to ensure completion of the oceanographic work in the available time.

5.2 CTD sensors

Various problems occurred with the CTD sensors over the course of the cruise. For CTD 1103 (used for the first 18 stations), the conductivity output became increasingly noisy after station 10, resulting in random salinity noise with an amplitude up to ~0.01 psu. The CTD was finally changed to CTD 1193 following station 18. After the cruise, the noise problem in CTD 1103 was traced to loosely mounted cards inside the housing.

Conductivity noise was minimal for CTD 1193, however the conductivity cell response showed a strong pressure dependence. In addition, the same conductivity cell displayed significant hysteresis between the down and upcasts. These problems are discussed in more detail in section 6. Following station 56, the conductivity cell on CTD 1193 was changed for a spare. The spare cell functioned well, except for a transient error when first entering the water - the cell appeared to need soaking near the surface for up to 2 minutes, before a stable conductivity reading was reached.

Prior to station 95, moisture was discovered entering the CTD 1193 housing, causing corrosion of the fast temperature sensor connector. The fault was traced to pits in the o-ring seats of the metal mounting plate on which the conductivity and fast temperature sensors are mounted. As a temporary fix, the connectors were sprayed with a water displacing agent, and the space behind the sensors in

more of these substances caused slight contamination of the conductivity cell, resulting in a small amount of signal noise over the next few stations.

For both CTD 1103 and 1193, the oxygen sensor oil reservoir housing could not be screwed tightly onto the mounting connector threads. As a result, any impact, such as caused by the instrument breaking through the water surface on deployment, caused the housing to move sufficiently for the silicon oil to drain past the o-ring, and resulting in loss of data (see section 6). This occurred several times early in the cruise. Following station 28, 2 adjacent o-rings (instead of the usual 1) were installed in the oxygen oil reservoir housing, solving the oil drainage problem.

Following station 76, a crack was discovered in the housing window for the photosynthetically active radiation sensor. The sensor was not used for the remainder of the cruise.

The altimeter did not function for the first 4 stations, thus these CTD casts were only taken to within ~100 to 200 m of the bottom. Following station 4, the problem was traced to a burnt out chip in CTD 1103. The altimeter performed well for the remainder of the cruise, allowing close CTD approaches to the bottom (Table 2).

5.3 Other equipment

The first few days of bathymetry data were lost due to problems with the 12 kHz echo sounder transducer. Good bathymetry data was obtained starting from 19/12/94 UTC.

Routing of the aft CTD winch wire resulted in serious kinking of the wire on several occasions - the wire required retermination each time. Following station 33, operations were changed to the forward CTD winch wire, and no more serious problems occurred for the remainder of the cruise.

One of the upward looking sonar moorings (Table 5) could not be located with the acoustic release surface transducer. No attempt was made to send the release command, owing to the significant sea ice coverage. At the time of writing, further recovery attempts indicated the mooring was no longer present at the deployment site.

6 RESULTS

This section details information relevant to the creation and the quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 14 and 15, and section 6.1.2; hydrology data - Tables 18 and 19.
```

Historical data comparisons are made in section 7. Data file formats are described in Appendix 4 of Rosenberg et al. (1995b).

6.1 CTD measurements

6.1.1 Creation of CTD 2 dbar-averaged and upcast burst data

Conductivity

Four different conductivity cells were used during the cruise, as follows:

```
conductivity cell 1, stations 1-18 (using CTD 1103); conductivity cell 2, stations 19-56 (using CTD 1193);
```

conductivity cell 4, station 107 (using CTD 2568).

With the exception of cell 4, all the conductivity cells displayed large transient errors when entering the water. In addition, cell 3 displayed significant hysteresis between downcast and upcast conductivity data. As a result, for stations 1 to 106, upcast CTD data was used for all the 2 dbaraveraged pressure, temperature and conductivity data. Note that station 107 data were not used.

The response of conductivity cells 1 and 2 showed a pressure dependence, much stronger in the case of cell 2. For both these cells (i.e. stations 1 to 56), the pressure dependent conductivity residual was removed by the following steps:

- (a) CTD conductivity was initially calibrated to derive conductivity residuals (c_{btl} c_{cal}), where c_{btl} and c_{cal} are as defined in the CTD methodology, noting that c_{cal} is the conductivity value after the initial calibration only i.e. prior to any pressure dependent correction.
- (b) Next, for each station grouping (Table 11), a linear pressure dependent fit was found for the conductivity residuals i.e. for station grouping i, fit parameters α_i (Table 11) and β_i were found from

$$(c_{btl} - c_{cal})_n = \alpha_i p_n + \beta_i$$
 (eqn 1)

where the residuals $(c_{btl} - c_{cal})_n$ and corresponding pressures p_n (i.e. pressures where Niskin bottles fired) are all the values accepted for conductivity calibration in the station grouping.

(c) Lastly, the conductivity calibration was repeated, this time fitting $(c_{ctd} + \alpha_i p)$ to the bottle values c_{btl} in order to remove the linear pressure dependence for each station grouping i (for uncalibrated conductivity c_{ctd} as defined in the CTD methodology; and note that the offsets β_i were not applied).

Dissolved oxygen

For stations 19 to 106, downcast oxygen temperature and oxygen current data were merged with the upcast pressure, temperature and conductivity data (upcast dissolved oxygen data is in general not reliable). With this data set, calibration of the dissolved oxygen data then followed the usual methodology. No CTD oxygen data was obtained for stations 1 to 18, due to a hardware fault in CTD 1103.

A small additional error in CTD dissolved oxygen data is expected to occur from the merging of downcast oxygen data with upcast pressure, temperature and conductivity data - where horizontal gradients occur, there will be some mismatch of downcast and upcast data as the ship drifts during a CTD cast. At most, this error is not expected to exceed ~3%.

Summary

stations 1-18: all CTD data from upcast; weak pressure dependent conductivity residual removed; no CTD dissolved oxygen data;

stations 19-56: CTD data from upcast, except for dissolved oxygen data (downcast); strong pressure dependent conductivity residual removed.

stations 57-106: CTD data from upcast, except for dissolved oxygen data (downcast).

Further information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- Surface pressure offsets calculated for each station are listed in Table 10.
- * Missing 2 dbar data averages are listed in the files avmiss.out and avoxmiss.out (the latter for CTD

- * CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 11 and 12.
- * CTD raw data scans flagged for special treatment are listed in Table 13.
- * Suspect 2 dbar averages are listed in Tables 14 and 15. The file avinterp.out lists 2 dbar averages which are linear interpolations of the surrounding 2 dbar averages.
- * CTD dissolved oxygen calibration coefficients are listed in Table 16. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 17.
- Stations containing fluorescence and photosynthetically active radiation data are listed in Table 22.
- * The different protected and unprotected thermometers used for the stations are listed in Table 23.

6.1.2 CTD data quality

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 2 to 5. For temperature, salinity and dissolved oxygen, the respective residuals (T_{therm} - T_{cal}), (s_{btl} - s_{cal}) and (o_{btl} - o_{cal}) are plotted. For conductivity, the ratio c_{btl}/c_{cal} is plotted. Note that for stations where a correction was made for the pressure dependent conductivity error, c_{cal} here refers to the final calibrated value after the correction. T_{therm} and T_{cal} are respectively the protected thermometer and calibrated upcast CTD burst temperature values; s_{btl} , s_{cal} , o_{btl} , o_{cal} , c_{btl} and c_{cal} , and the mean and standard deviation values in Figures 2 to 5, are as defined in the CTD methodology.

CTD data quality cautions for the various parameters are discussed below. Table 8 contains a summary of these cautions.

Pressure

The titanium strain gauge pressure sensors used in the Mark IIIC CTD's display a higher noise level than the older stainless steel strain gauge models, with a typical rms of ~±0.2 dbar (Millard et al., 1993). Noise in the pressure signal for CTD 1193 (used for stations 19 to 106) was found to be higher than this, with spikes of up to 1 dbar amplitude occurring. In the creation of CTD raw data files monotonically increasing with pressure (see CTD methodology), pressure spikes with a width exceeding 3 data points are retained as real values. Thus as a result of the high noise levels for CTD 1193, a large number of 2 dbar bins were missing, as not enough data points were present in these bins to form a bin average. The number of missing bins was reduced by setting to 6 the minimum number of data points required in a 2 dbar bin to form an average (i.e. jmin=6; for previous cruises, jmin=10). Note that jmin=6 was used for the entire cruise. For remaining missing bins, values were linearly interpolated between surrounding bins, except where the local temperature gradient exceeded 0.005°C between the surrounding bins i.e. temperature gradient > 0.00125 degrees/dbar.

For stations 48, 54 and 72, surface pressure offset values fell on small pressure spikes, thus the final surface pressure offsets were estimated from a manual inspection of the pressure data. A manual estimate was also required for station 55. The surface pressure offset values for stations 66 and 76 were estimated from the surrounding stations (Table 10). Any resulting additional error in the CTD pressure data is judged to be small (no more than 0.2 dbar).

For stations 7, 11, 16, 28, 65 and 66, flooding of the dissolved oxygen sensor with seawater resulted in bad pressure temperature data (as discussed in Rosenberg et al., 1995b). To allow accurate calculation of pressure in dbar, the following pressure temperature data were used in pressure calculations for these stations:

| station with bad pressure temperature | used pressure temperature data from this station for upcast |
|---------------------------------------|--|
| 7 | 8 |
| 11 | 10 |
| 16 | 17 |
| 28 | 27 |
| 65 | 64 |
| 66 | 67 for p≥2000 dbar |
| 66 | 66 for n<2000 dhar |

Note that the pressure temperature profiles chosen above provide the closest match to the assumed pressure temperature profiles for stations 7, 11, 16, 28, 65 and 66, and any errors are judged to be small (<0.3 dbar).

Salinity

The conductivity ratios for all bottle samples are plotted in Figure 3, while the salinity residuals are plotted in Figure 4. The final standard deviation values for the salinity residuals (Figure 4) indicate the CTD salinity data over the whole cruise is accurate to within ±0.002 psu.

No conductivity residual correction was made for stations 1 and 54: all bottles were fired at the same depth for these stations (test casts), so that any pressure dependent conductivity residual (section 6.1.1) could not be quantified. Note that as a result, the salinities for these stations can only be considered as accurate to ~0.01 psu.

Bottle salinity data was lost for station 24, due to malfunction of the salinometer. The station was grouped with surrounding stations for conductivity calibration (Table 11).

No conductivity residual correction (section 6.1.1) was made for stations 3 to 10 and 52 to 53, as no pressure dependent conductivity residual was found for these stations.

Temperature

The temperature residuals are shown in Figure 2, along with the mean offset and standard deviation of the residuals. The thermometer value used in each case is the mean of the two protected thermometer readings (protected thermometers used are listed in Table 23). Note that in the figures, the "dubious" and "rejected" categories refer to corresponding bottle samples and upcast CTD bursts in the conductivity calibration, rather than to CTD/thermometer temperature values.

For CTD 1193 (stations 19 to 106), there was a problem with the laboratory calibration of the platinum temperature sensor. With the original pre-cruise calibration coefficients, an offset of 0.007°C was found between CTD and reversing thermometer temperature values. As a consequence, an additional offset value of -0.007°C (Appendix 1) was applied to all CTD temperature values for stations 19 to 106.

Table 8: Summary of cautions to CTD data quality.

| 7 | pressure | station 8 pressure temperature profile used for pressure calculation |
|-----------|---------------------|--|
| 11 | pressure | station 10 pressure temperature profile used for pressure calculation |
| 16 | pressure | station 17 pressure temperature profile used for pressure calculation |
| 24 | salinity | CTD conductivity calibrated with bottles from surrounding stations |
| 28 | pressure | station 27 pressure temperature profile used for pressure calculation |
| 47 | salinity, oxygen | most bottles tripped on the fly - may introduce small inaccuracy into the conductivity and dissolved oxygen calibrations |
| 54 | salinity | test cast - all bottles fired at same depth; salinity accuracy reduced |
| 65 | pressure | station 64 pressure temperature profile used for pressure calculation |
| 66 | pressure | surface pressure offset estimated from surrounding stations |
| 66 | pressure | station 67 pressure temperature profile used for pressure calculation for p≥2000 dbar |
| 76 | pressure | surface pressure offset estimated from surrounding stations |
| 107 | all parameters | data not used for this station (test cast only) |
| 2-4,11-51 | ,55-56 salinity | additional correction applied for pressure dependent conductivity residual |
| 19 to 106 | temperature | additional calibration offset value based on comparison with reversing thermometer data |
| 1 to 107 | fluorescence/p.a.r. | fluorescence and p.a.r. sensors (where active) are uncalibrated |
| 1 to 18 | oxygen | no CTD dissolved oxygen data due to faulty hardware |
| 28,65,66 | oxygen | no CTD dissolved oxygen data due to oil drainage from sensor housing |

Dissolved Oxygen

After the cruise, the CTD dissolved oxygen data for CTD 1103 (stations 1 to 18) was found to be unusable. The fault was traced to incorrect wiring in the factory-provided oxygen sensor mounting.

The dissolved oxygen residuals are plotted in Figure 5. The final standard deviation values are within 1% of full scale values (where full scale is approximately equal to 250 μmol/l for pressure > 750 dbar, and 350 μ mol/I for pressure < 750 dbar).

In general, good calibrations of the CTD dissolved oxygen data were obtained using the in situ bottle data, however some atypical values were found for the calibration coefficients (Tables 16 and 17) (see the CTD methodology for full details of calibration formulae). For most stations, the best calibration was achieved using large values of the order 10.0 for the coefficient K₁ (i.e. oxygen current slope), and large negative values of the order -1.5 for the coefficient K_3 (i.e. oxygen current bias). This, however, is not considered relevant to actual data quality.

In addition, the following unusual coefficient values were found (for typical values, see Millard and Yang, 1993, and Millard, 1991):

stations 56 and 58: $K_5 > 1$ (usually expect $0 < K_5 < 1$);

 $K_6 < 0$ (usually expect a positive value); stations 58 and 105:

Despite some atypical calibration coefficient values, all dissolved oxygen calibrations are considered valid.

Oil drainage from the oxygen sensor mounting resulted in unusable dissolved oxygen data for stations 28, 65 and 66.

No oxygen bottle samples were collected for station 54. No attempt was made to calibrate the dissolved oxygen data for this station.

Fluorescence and P.A.R. Data

As discussed in section 4 above, fluorescence and p.a.r. are effectively uncalibrated. These data should not be used quantitatively other than for linkage with primary productivity data.

6.2 Hydrology data

6.2.1 Hydrology data quality

Quality control information relevant to the hydrology data is tabulated, as follows:

- * Questionable dissolved oxygen and nutrient Niskin bottle sample values are listed in Tables 18 and 19 respectively. Note that questionable values are included in the hydrology data file, whereas bad values have been removed.
- * Laboratory temperatures at the times of nutrient analyses are listed in Table 20.
- * Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 21.

For station 47, the cast was abandoned at ~1000 on the downcast, due to ice floes around the CTD wire. During retrieval, bottles at rosette positions 1 to 18 were tripped on the fly. For station 48, 8 bottles did not trip, due to malfunction of the rosette pylon.

Nutrients

For the phosphate analyses, it was found that the autoanalyser peak height of a sample which was run immediately after a series of wash solution vials (low nutrient sea water) was suppressed by, on average, 2%, as discussed in section 6.2.1 of Rosenberg et al. (1995b). For stations 1 to 34, samples thus affected (typically from rosette positions 12 and 24) were treated as bad data. Following station 34, additional "dummy" samples drawn from the Niskin bottles were inserted in autoanalyser runs immediately following wash solution vials to artificially mask the suppression effect on subsequent samples.

Surface phosphate values for many of the remaining stations still remain artificially suppressed - in Figure 9 the low phosphate values, in the vicinity of the nitrate+nitrite concentration of ~25 umol/l, are all near surface samples. Moreover, these samples all occur in regions where the steepest vertical gradients in nutrient concentrations are found. As a result of the steep vertical gradients, near surface phosphate concentrations are much lower than for the remainder of the water column, and any suppression of the phosphate autoanalyser peaks for the near surface samples will become amplified when data are viewed as ratios (Figure 9). These questionable near surface phosphate samples are listed in Table 19.

For surface silicate samples at stations 71 to 104, the autoanalyser silicate peaks were spiked, causing problems in the automatic peak integration performed by the software DAPA (see Appendix 3 in Rosenberg et al., 1995b). The replicate surface sample (one of the dummy samples for the phosphate analysis) did not show the same response, so the replicate was used for measuring the peak height.

The following notes also apply to the nutrient data:

* For station 107, no nutrient samples were collected.

* For the station 62, all nutrient concentrations were derived from manual measurements of autoanalyser peak heights, using the strip chart recordings.

6.2.2 Hydrology sample replicates

The accuracy and precision of bottle data are considered relative to the full scale deflection of measurement for nutrients

phosphate: 3.0 µmol/l nitrate+nitrite: 35.0 µmol/l silicate: 140 µmol/l

and relative to the maximum data value for dissolved oxygen

dissolved oxygen: \sim 350 μ mol/l for pressure < 750 dbar \sim 250 μ mol/l for pressure > 750 dbar.

In general, no organised sample replication was carried out, thus the replicate data set discussed here is small. Most replicate data were obtained opportunistically, from multiple fired Niskin bottles taken during bottle test casts, or from depths sampled in both casts of shallow/deep cast pairs. Two types of replicate data were obtained from the hydrology data set, as follows.

Replicate samples drawn from the same Niskin bottle

A series of repeat nutrient samples were drawn from 2 different Niskin bottles at station 32. At each of the Niskins, the absolute value of the differences about the mean value were formed (Figure 6a). Precision values for phosphate, nitrate+nitrite and silicate are respectively 0.16%, 0.22% and 0.35% of the full scale deflection (Table 9a).

Table 9a: Precision data for replicates drawn from same Niskin bottle.

| parameter | standard deviation | % of full scale | number of | number of |
|-----------------|--------------------|-----------------|-----------|---------------|
| | of differences | deflection | samples | sample groups |
| phosphate | 0.0047 μmol/l | 0.16 | 22 | 2 |
| nitrate+nitrite | 0.0765 μmol/l | 0.22 | 24 | 2 |
| silicate | 0.4906 μmol/l | 0.35 | 24 | 2 |

Replicate samples drawn from different Niskin bottles tripped at same depth

At several stations, multiple Niskin bottles were fired at a single depth. For each set of Niskin bottles tripped at a single depth, a mean value m_x was calculated for the sample set and the differences $x-m_x$ formed, where x is the phosphate, nitrate+nitrite, silicate, salinity or dissolved oxygen bottle value; the standard deviation of all $x-m_x$ values for the replicate data was calculated. Absolute values of the differences $x-m_x$ are shown in Figure 6b, and the results are summarised in Table 9b. It is assumed that these precision values would be further reduced if sample groups were drawn from the same Niskin bottle.

<u>Table 9b:</u> Precision data for replicates drawn from Niskin bottles tripped at the same depth.

parameter standard deviation % of full scale number of number of

| phosphate | 0.0061 μmol/l | 0.20 | 59 | 24 |
|------------------|---------------|------|----|----|
| nitrate+nitrite | 0.1473 μmol/l | 0.42 | 66 | 27 |
| silicate | 0.6266 μmol/l | 0.45 | 67 | 27 |
| salinity | 0.0007 psu | - | 67 | 27 |
| dissolved oxygen | 0.1446 μmol/l | 0.06 | 66 | 27 |

7 HISTORICAL DATA COMPARISONS

In this section, a brief comparison is made between the au9404 cruise data, and data from the previous cruise au9407 (Rosenberg et al., 1995b).

7.1 Dissolved oxygen

Vertical profiles of CTD dissolved oxygen concentrations for cruises au9404 and au9407 are compared in Figure 7. Note that dissolved oxygen concentrations of bottle samples for both cruises were measured using the WHOI automated method (see Appendix 3, Rosenberg et al., 1995b). Concentration values for the two cruises are in general consistent.

7.2 Salinity

The meridional variation of the salinity maximum for the two cruises i.e. for Lower Circumpolar Deep Water (as defined by Gordon, 1967) is compared in Figure 8. For the comparison, CTD 2 dbar data were used i.e. CTD salinity, temperature and pressure values at the nearest 2 dbar bin to the salinity maximum for each station. Note that in the figure, property differences are only formed between station pairs (i.e. corresponding au9404 and au9407 stations) which are separated by less than 1.5 nautical miles of latitude.

There appears to be a mean offset of ~0.003 psu between the two cruises (Figure 8), smaller than the large salinity offset of ~0.007 psu found between cruises au9309 and au9407 (Appendix 6 in Rosenberg et al., 1995b). Note that there is no consistent biasing of the temperature or pressure data (Figure 8), suggesting that the difference is due to salinity alone, the same result as found for the comparison between earlier cruises. In summary, the following approximate mean salinity differences are evident for the successive occupations of the SR3 transect:

cruise comparison mean salinity difference

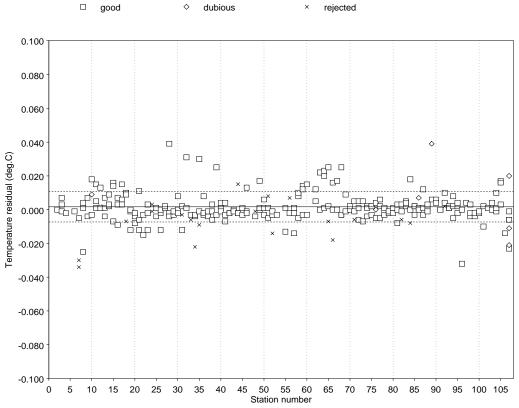
au9309-au9101 < 0.002 psu au9309-au9407 0.007 psu au9404-au9407 0.003 psu

As discussed in Rosenberg et al. 1995b, the most likely source of any systematic salinity error is the salinometers (YeoKal Mk IV) used for the analysis of salinity samples from the Niskin bottles. However, the exact cause of the error remains inconclusive. At the time of writing, two more recent occupations of SR3 stations await processing, while a further transect of SR3 is planned using more accurate salinometers (Guildline Autosals). These later data sets may clarify any instrument errors.

7.3 Nutrients

Phosphate and nitrate+nitrite concentrations are in general consistent for the au9404 and au9407 data, revealed by comparison of the nitrate+nitrite to phosphate ratio (Figure 9). Note that for au9404, the depressed phosphate values at the approximate nitrate+nitrite level of 25 µmol/l are all near

There is a small non-linearity in the nitrate+nitrite to phosphate ratio for both cruises, with low nutrient values lying below the best fit linear relationship (Figure 9). A similar trend is evident in data from cruise au9309 (Figure A6.4 in Rosenberg et al., 1995b), and data along the P11 transect from cruise au9391 (Figure A6.10 in Rosenberg et al., 1995a) (although there is more scatter in the au9391 data). For cruise au9404, these low values correspond with near surface samples north of the Subantarctic Front (Figure 10) i.e. north of ~50°S. Note that at both the Subantarctic and Subtropical Fronts (at ~50°S and ~45.5°S respectively from inspection of surface temperatures in Figure 10), there is a sharp horizontal gradient in surface nutrient values, with concentrations decreasing to the north across the fronts. A corresponding northward decrease in the nitrate+nitrite to phosphate ratio is also evident (Figure 10), accounting for the non-linearity in the ratio at low nutrient concentrations (Figure 9). This effect, also observed in the earlier cruises, appears to be a real feature.



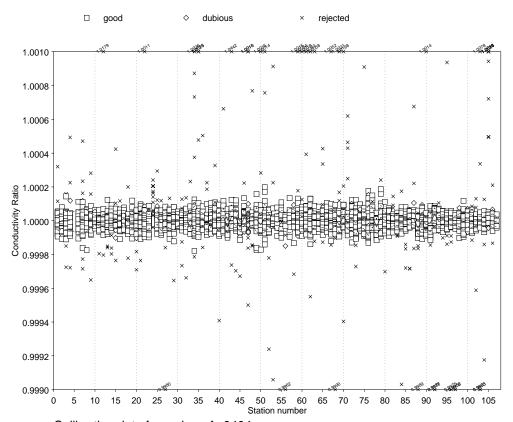
Calibration data for cruise: Au9404

Calibration file: histcal.lis

Mean offset Temperature = 0.00166312c (s.d. = 0.0090 °c)

Number of samples used = 243 out of 265

<u>Figure 2:</u> Temperature residual (T_{therm} - T_{cal}) versus station number for cruise au9404. The solid line is the mean of all the residuals; the broken lines are \pm the standard deviation of all the residuals (as defined in the CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.

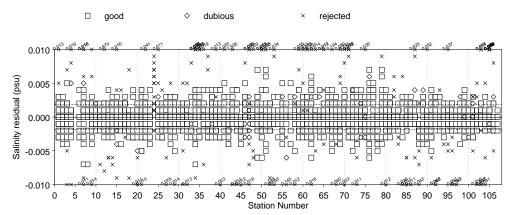


Calibration data for cruise: Au9404

Calibration file : histcal.lis Conductivity s.d. = 0.00005

Number of bottles used = 2129 out of 2379 Mean ratio for all bottles = 1.00000

<u>Figure 3:</u> Conductivity ratio c_{btl}/c_{cal} versus station number for cruise au9404. The solid line follows the mean of the residuals for each station; the broken lines are \pm the standard deviation of the residuals for each station (as defined in the CTD methodology).



Calibration data for cruise : Au9404

Calibration file: histcal.lis

Mean offset salinity = 0.0000psu (s.d. = 0.0018 psu)

Number of bottles used = 2129 out of 2379

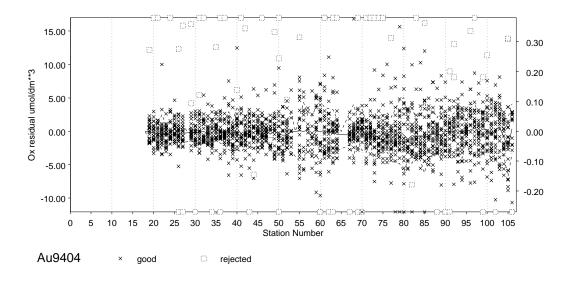
<u>Figure 4:</u> Salinity residual (s_{btl} - s_{cal}) versus station number for cruise au9404. The solid line is the mean of all the residuals; the broken lines are \pm the standard deviation of all the residuals (as defined in the CTD methodology).

Mean of Residual = -0.257umol/dm**3

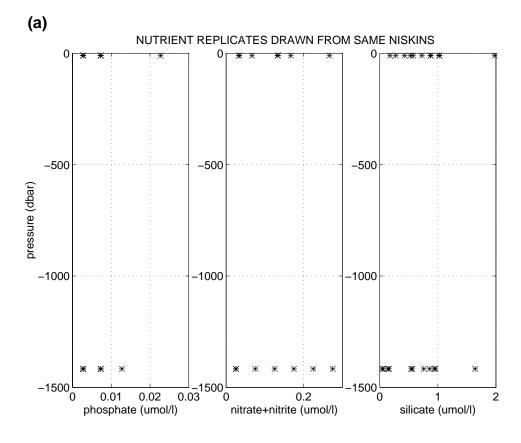
S.D. of residual = $2.881 \text{umol/dm}^{**}3$ (Equiv to 0.065 ml/l)

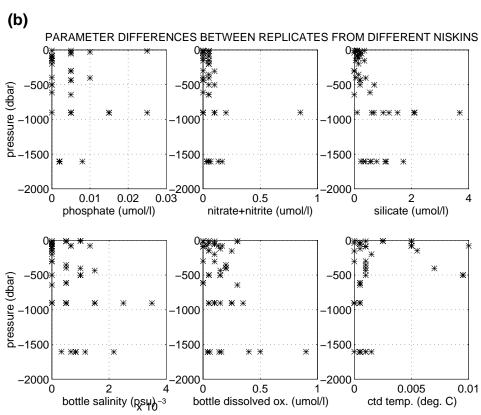
Used 1849 bottles out of total 1947

S.D. deep (>750m) 2.107umol/dm**3 (equiv to 0.047ml/l)



<u>Figure 5:</u> Dissolved oxygen residual (o_{btl} - o_{cal}) versus station number for cruise au9404. The solid line follows the mean residual for each station; the broken lines are \pm the standard deviation of the residuals for each station (as defined in the CTD methodology).





<u>Figure 6:</u> Absolute value of parameter differences for replicate samples, for replicates drawn from (a) the same Niskin bottle, and (b) different Niskins tripped at the same depth. Note that differences are between parameter values and depth mean.

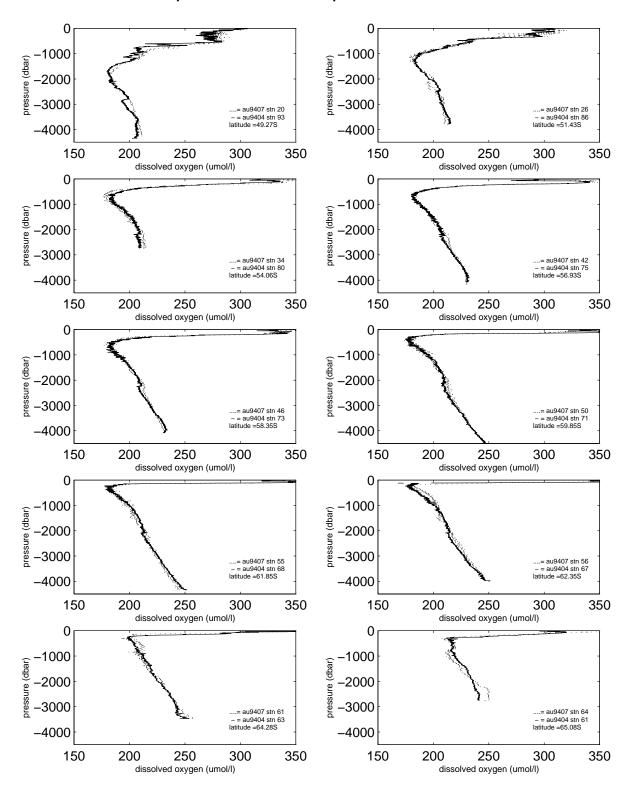


Figure 7: CTD dissolved oxygen vertical profile data for comparison of au9404 and au9407 data.

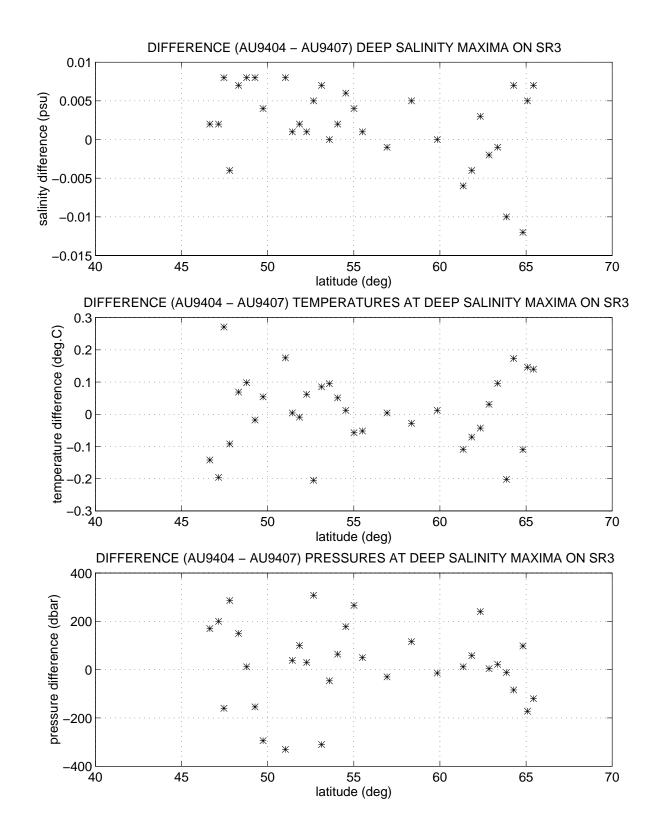


Figure 8: Variation with latitude south along the SR3 transect of properties at the deep salinity

cruise au9404 and cruise au9407 i.e. au9404 value minus au9407 value. Note that differences are formed only between stations from the two cruises which are separated by no more than 1.5 nautical miles of latitude.

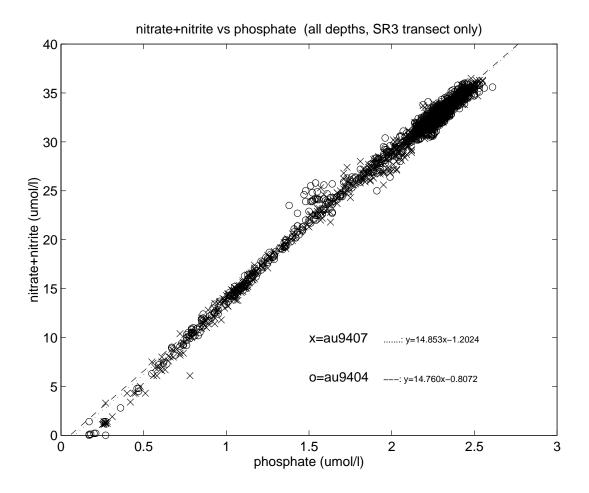
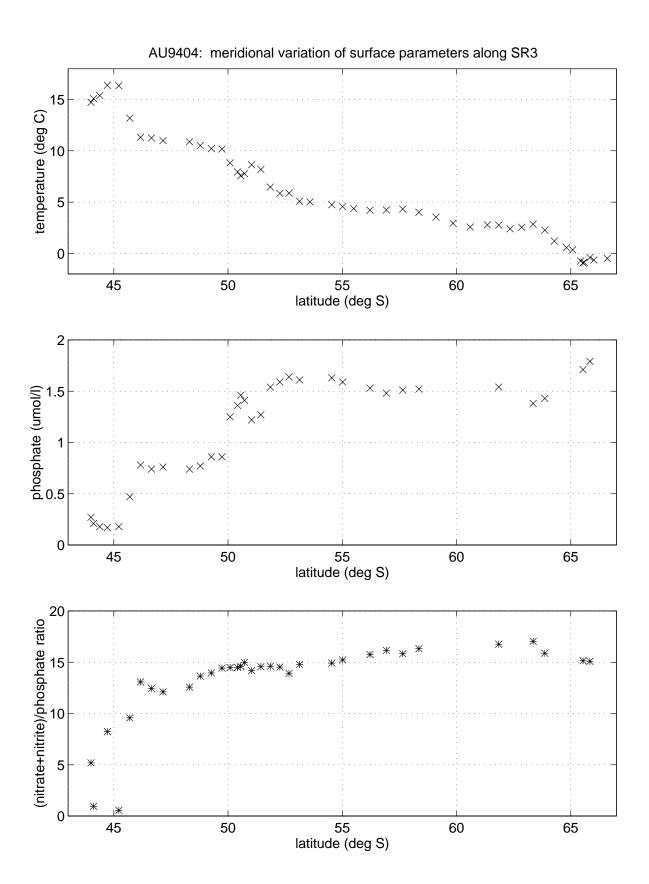


Figure 9: Bulk plot of nitrate+nitrite versus phosphate for all au9404 and au9407 data along the SR3 transect, together with linear best fit lines.



<u>Figure 10:</u> Meridional variation along the SR3 transect of CTD temperature, phosphate concentration, and nitrate+nitrite to phosphate ratio, all at the near surface Niskin bottle.

<u>Table 10:</u> Surface pressure offsets (as defined in the CTD methodology). ** indicates that value is estimated from surrounding stations, or else determined from manual inspection of pressure data.

| station number | surface p offset (dbar) | | surface p offset (dbar) | | surface p offset (dbar) | station : | surface p offset (dbar) |
|---|---|---|--|--|--|---|---|
| number | • | | | | • | | |
| 15 S4 16 S4 17 S4 18 S4 19 S4 20 S4 21 S4 22 S4 23 S4 24 S4 25 S4 26 S4 27 S4 | -3.24 -3.86 -3.73 -2.96 -0.40 -0.29 -1.08 -0.63 -0.82 -0.32 -0.42 -0.72 -0.93 | 42 S4 43 S4 44 S4 45 S4 46 S4 47 S4 48 S4 49 S4 50 S4 51 S4 52 S4 53 S4 54 TEST | -0.84 -1.13 -1.03 -1.61 -0.60 -0.59 -1.00** -1.08 -0.92 -0.66 -1.22 -1.58 | 69 SR3 70 SR3 71 SR3 72 SR3 73 SR3 74 SR3 75 SR3 76 SR3 77 SR3 78 SR3 79 SR3 80 SR3 81 SR3 | -1.28 -1.36 -1.04 -0.90** -0.87 -1.07 -1.09 -1.66** -1.32 -1.67 -2.37 -1.94 | 96 SR3 97 SR3 98 SR3 99 SR3 100 SR3 101 SR3 102 SR3 103 SR3 104 SR3 105 SR3 106 SR3 | -1.74 -1.86 -1.94 -1.46 -2.24 -1.49 -1.77 -1.55 -1.34 -1.52 -1.73 |

<u>Table 11:</u> CTD conductivity calibration coefficients. F_1 , F_2 and F_3 are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping; σ is the standard deviation of the conductivity residual for the n samples in the station grouping (eqn A2.19 in the CTD methodology); α is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals (eqn 1).

| station grouping | F ₁ | F ₂ | F_3 | n | σ | α |
|---|---|---|---|--|--|---|
| 001 to 002 S4 | -0.55151931E-01 | 0.98768159E-03 | -0.25816422E-06 | 43 | 0.001388 0 | 0 (stn 1) .7039725E-06 (stn 2) |
| 003 to 004 S4 005 to 006 S4 007 to 008 S4 009 to 010 S4 011 to 012 S4 013 to 014 S4 015 to 018 S4 021 to 022 S4 023 to 027 S4 028 to 029 S4 030 to 031 S4 032 to 033 S4 034 to 035 S4 036 to 038 S4 039 to 040 S4 041 to 043 S4 044 to 046 S4 047 to 048 S4 049 to 051 S4 052 to 053 S4 | -0.55896676E-01 -1.3093410 -0.54926719E-01 -0.84408096E-01 -0.79525457E-01 -0.47581367E-01 -0.90261955E-01 0.35624898E-01 0.35077650E-01 0.21164570E-02 0.10941363E-01 0.88594631E-02 0.19440563E-01 -0.60553073 0.36708276E-01 0.82647512E-01 0.19447580E-01 0.30237096E-01 0.59998387E-01 0.40529276E-01 0.72904220E-01 -0.16437023E-01 | 0.98729002E-03 0.10322266E-02 0.98668229E-03 0.98892340E-03 0.98788105E-03 0.98726571E-03 0.95488768E-03 0.955489180E-03 0.95544232E-03 0.95649136E-03 0.96028342E-03 0.95577090E-03 0.95577090E-03 0.955736474E-03 0.95680538E-03 0.96962316E-03 0.95536507E-03 0.94224468E-03 | -0.10392899E-07 0 0.31628388E-07 -0.11378698E-06 -0.17868175E-07 0.20690218E-07 0.52286883E-07 0.12901507E-06 -0.11562160E-06 -0.70763325E-08 0.89732482E-07 0.50457051E-07 -0.84564608E-07 -0.18690584E-06 0.21875702E-07 0.77198775E-07 -0.79680507E-08 -0.27308193E-08 -0.28862853E-06 0.20374809E-07 0.25347666E-06 0.18430266E-06 | 33 43 45 43 87 44 46 85 46 43 40 66 45 68 66 31 67 30 | 0.001772 0.001976 0.001072 0.000863 0.001268 0.001376 0.001699 0.001277 0.001467 0.000846 0.001096 0.002047 0.001375 0.001361 0.001541 0.001468 0.001060 0.001983 0.001039 | 0 0 1.4608959E-06 0.8503317E-06 1.1245280E-06 -3.9074269E-06 -3.1360125E-06 -3.8628606E-06 -4.1948918E-06 -4.2553530E-06 -3.7799151E-06 -0.5076831E-06 -3.1761190E-06 -2.9058778E-06 -2.3631424E-06 -1.8128443E-06 -0.9916311E-06 -1.0150511E-06 |
| 00 1 10 000 0110 | 0.101070202 01 | 0.0 10 102772 00 | 0.101002002 00 | 10 | 1.105 | 52417E-05(stn55) 57907E-05(stn56) |
| 057 to 058 SR3 059 to 060 SR3 061 to 062 SR3 063 to 065 SR3 066 to 067 SR3 068 to 071 SR3 072 to 074 SR3 075 to 076 SR3 077 to 079 SR3 080 to 081 SR3 082 to 083 SR3 084 to 085 SR3 086 to 092 SR3 093 to 095 SR3 096 to 097 SR3 098 to 099 SR3 100 to 101 SR3 | 0.83091393E-01 0.38970365E-01 0.10962147E-01 0.53262814E-02 -0.67340513E-02 0.26176288E-01 -0.33286342E-01 -0.24514632E-01 -0.38553928E-01 -0.64523829E-02 -0.31874236E-01 -0.22073834E-01 -0.68709889E-02 0.13907181E-02 0.37615123E-02 0.20749048E-01 0.65954377E-02 0.57362283E-03 | 0.97579514E-03 0.95136388E-03 0.96004529E-03 0.96057593E-03 0.95711703E-03 0.95501467E-03 0.95585560E-03 0.95585560E-03 0.95852101E-03 0.95459300E-03 0.95688724E-03 0.95680064E-03 0.95744099E-03 0.95472218E-03 0.95472218E-03 | -0.36657863E-06 0.77236642E-07 -0.52779303E-07 -0.57406289E-07 0.32602246E-08 0.16981713E-07 -0.39304776E-07 0.26753495E-07 0.79812009E-08 -0.14973816E-07 -0.53150506E-07 0.38284407E-07 0.42797804E-08 0.14985374E-09 -0.84529938E-08 -0.32570719E-06 0.59023049E-08 -0.41938467E-07 | 19 41 43 62 43 81 65 45 64 44 43 150 65 40 48 43 57 | 0.001715 0.001387 0.001912 0.001059 0.001515 0.001365 0.001755 0.002289 0.001975 0.001366 0.000775 0.001037 0.001549 0.001092 0.000884 0.001562 0.001298 0.000914 | |

<u>Table 12:</u> Station-dependent-corrected conductivity slope term ($F_2 + F_3$. N), for station number N, and F_2 and F_3 the conductivity slope and station-dependent correction calibration terms respectively.

| station number | (F ₂ + F ₃ . N) | station number | (F ₂ + F ₃ . N) | station number | (F ₂ + F ₃ . N) |
|-------------------|---------------------------------------|-------------------|---------------------------------------|-------------------|---------------------------------------|
| | | | | | _ |
| | 0.98742342E-03 | 37 S4 | 0.95658030E-03 | 73 SR3 | 0.95827468E-03 |
| 2 S4 | 0.98716526E-03 | 38 S4 | 0.95660218E-03 | 74 SR3 | 0.95823538E-03 |
| 3 S4 | 0.98725884E-03 | 39 S4 | 0.95504184E-03 | 75 SR3 | 0.95786211E-03 |
| 4 S4 | 0.98724844E-03 | 40 S4 | 0.95511904E-03 | 76 SR3 | 0.95788886E-03 |
| 5 S4 | 0.10322266E-02 | 41 S4 | 0.95703805E-03 | 77 SR3 | 0.95842332E-03 |
| 6 S4 | 0.10322266E-02 | 42 S4 | 0.95703008E-03 | 78 SR3 | 0.95843131E-03 |
| 7 S4 | 0.98690369E-03 | 43 S4 | 0.95702211E-03 | 79 SR3 | 0.95843929E-03 |
| 8 S4 | 0.98693532E-03 | 44 S4 | 0.95668522E-03 | 80 SR3 | 0.95732310E-03 |
| 9 S4 | 0.98789931E-03 | 45 S4 | 0.95668249E-03 | 81 SR3 | 0.95730813E-03 |
| 10 S4 | 0.98778553E-03 | 46 S4 | 0.95667976E-03 | 82 SR3 | 0.95817735E-03 |
| 11 S4 | 0.98768450E-03 | 47 S4 | 0.95605761E-03 | 83 SR3 | 0.95812420E-03 |
| 12 S4 | 0.98766663E-03 | 48 S4 | 0.95576899E-03 | 84 SR3 | 0.95780889E-03 |
| 13 S4 | 0.98670749E-03 | 49 S4 | 0.95636344E-03 | 85 SR3 | 0.95784717E-03 |
| 14 S4 | 0.98672818E-03 | 50 S4 | 0.95638381E-03 | 86 SR3 | 0.95725530E-03 |
| 15 S4 | 0.98805001E-03 | 51 S4 | 0.95640419E-03 | 87 SR3 | 0.95725958E-03 |
| 16 S4 | 0.98810230E-03 | 52 S4 | 0.95542546E-03 | 88 SR3 | 0.95726386E-03 |
| 17 S4 | 0.98815459E-03 | 53 S4 | 0.95567894E-03 | 89 SR3 | 0.95726814E-03 |
| 18 S4 | 0.98820687E-03 | | 0.95835512E-03 | 90 SR3 | 0.95727242E-03 |
| 19 S4 | 0.95733896E-03 | 55 SR3 | 0.95853942E-03 | 91 SR3 | 0.95727670E-03 |
| 20 S4 | 0.95746798E-03 | 56 SR3 | 0.95872372E-03 | 92 SR3 | 0.95728098E-03 |
| 21 S4 | 0.95741133E-03 | 57 SR3 | 0.95490015E-03 | 93 SR3 | 0.95681457E-03 |
| 22 S4 | 0.95729571E-03 | 58 SR3 | 0.95453358E-03 | 94 SR3 | 0.95681472E-03 |
| 23 S4 | 0.95832904E-03 | 59 SR3 | 0.95592085E-03 | 95 SR3 | 0.95681487E-03 |
| 24 S4 | 0.95832197E-03 | 60 SR3 | 0.95599808E-03 | 96 SR3 | 0.95662950E-03 |
| 25 S4 | 0.95831489E-03 | 61 SR3 | 0.95682575E-03 | 97 SR3 | 0.95662105E-03 |
| 26 S4 | 0.95830781E-03 | 62 SR3 | 0.95677297E-03 | 98 SR3 | 0.95534341E-03 |
| 27 S4 | 0.95830074E-03 | 63 SR3 | 0.95695933E-03 | 99 SR3 | 0.95501771E-03 |
| 28 S4 | 0.95795483E-03 | 64 SR3 | 0.95690192E-03 | 100 SR3 | 0.95531241E-03 |
| 29 S4 | 0.95804456E-03 | 65 SR3 | 0.95684452E-03 | 101 SR3 | 0.95531831E-03 |
| 30 S4 | 0.95800507E-03 | 66 SR3 | 0.95733220E-03 | 102 SR3 | 0.95529443E-03 |
| 31 S4 | 0.95805553E-03 | 67 SR3 | 0.95733546E-03 | 103 SR3 | 0.95525249E-03 |
| 32 S4 | 0.95757736E-03 | 68 SR3 | 0.95616942E-03 | 104 SR3 | 0.95521055E-03 |
| 33 S4 | 0.95749279E-03 | 69 SR3 | 0.95618640E-03 | 105 SR3 | 0.95543257E-03 |
| 34 S4 | 0.97676403E-03 | 70 SR3 | 0.95620339E-03 | 106 SR3 | 0.95534163E-03 |
| 35 S4 | 0.97657712E-03 | 71 SR3 | 0.95622037E-03 | | |
| 36 S4 | 0.95655843E-03 | 72 SR3 | 0.95831399E-03 | | |

<u>Table 13:</u> CTD raw data scans, mostly in the vicinity of artificial density inversions, flagged for special treatment. Note that the pressure listed is approximate only; possible actions taken are either to ignore the raw data scans for all further calculations, or to apply a linear interpolation over the region of the bad data scans. Causes of bad data, listed in the last column, are detailed in the CTD methodology. For the raw scan number ranges, the lowest and highest scans numbers are not included in the ignore or interpolate actions.

| station | approximate | | action | reason |
|---------|--------------|------------------------------|-------------|------------------------|
| number | pressure (db | ar) numbers | taken | |
| 1 | 69 | 312710-312712 | ignore | fouling of cond. cell |
| 2 | 103 | 267360-267656; 267704-268141 | ignore | wake effect |
| 2 | 28; 24 | 274342-274439; 274610-274752 | ignore | wake effect |
| 3 | 110 | 294797-294846 | ignore | wake effect |
| 4 | 189 | 326120-326134 | ignore | fouling of cond. cell |
| 4 | 101 | 331813-332033 | ignore | wake effect |
| 17 | 102 | 269059-269211; 269417-269509 | ignore | wake effect |
| 18 | 53 | 300375-300727 | ignore | wake effect |
| 20 | 3704-3718 | 163056-163405 | ignore | fouling of cond. cell |
| 32 | 600 | 287236-287282 | ignore | fouling of cond. cell |
| 34 | 110-112 | 378784-378843 | ignore | fouling of cond. cell |
| 35 | 28; 26 | 330110-330137; 330166-330192 | ignore | fouling of cond. cell |
| 36 | 131-137 | 305201-305336 | ignore | fouling of cond. cell |
| 41 | 56-77 | 262645-262993 | ignore | fouling of cond. cell |
| 45 | 64-67 | 237753-237801 | interpolate | wake effect |
| 47 | 11 | 76038-76197 | interpolate | wake effect |
| 60 | 256-258 | 16896-170036 | interpolate | wake effect |
| 60 | 320 | 166669-166671 | ignore | suspect pressure value |
| 61 | 259 | 195087-195110 | ignore | wake effect |
| 65 | 56-72 | 254997-255277 | ignore | fouling of cond. cell |
| 71 | 213-216 | 285966-286010 | ignore | fouling of cond. cell |
| 94 | 1012-1039 | 271068-271531 | ignore | fouling of cond. cell |
| 95 | 828-834 | 257553-257678 | ignore | fouling of cond. cell |
| 103 | 236 | 227094-227097 | ignore | fouling of cond. cell |
| 105 | 150; 12 | 110099-110538; 121628-121631 | ignore | fouling of cond. cell |

<u>Table 14:</u> Suspect 2 dbar averages. Note: for suspect salinity values, the following are also suspect: sigma-T, specific volume anomaly, and geopotential anomaly.

| station | suspect 2 db | oar values (dbar) | reason |
|------------------|--------------|-------------------|--|
| number | bad | questionable | |
| Suspect salinity | values | | |
| 1 | 60,62 | 58,64,116,118 | salinity spike in steep local gradient |
| 2 | 24 | 20,22 | salinity spike in steep local gradient |
| 3 | 34,36 | 98 | salinity spike in steep local gradient |
| 4 | - | 100,110 | salinity spike in steep local gradient |
| 10 | - | 404 | salinity spike in steep local gradient |
| 11 | - | 120,122,124 | salinity spike in steep local gradient |
| 15 | 38 | 36,40,42,52,54 | salinity spike in steep local gradient |
| 16 | 38 | - | salinity spike in steep local gradient |
| 17 | 58 | 56,60 | salinity spike in steep local gradient |
| 18 | 54,96,1 | 08 52,56 | salinity spike in steep local gradient |
| 25 | - | 48 | salinity spike in steep local gradient |
| 29 | - | 46 | salinity spike in steep local gradient |
| 35 | - | 34 | salinity spike in steep local gradient |
| 55 | - | 802-812 | possible fouling of conductivity cell |
| 60 | - | 322 | salinity spike in steep local gradient |
| 67 | - | 54 | salinity spike in steep local gradient |
| 68 | 42 | - | salinity spike in steep local gradient |
| 71 | 64 | - | salinity spike in steep local gradient |
| 72 | - | 64 | salinity spike in steep local gradient |
| 73 | - | 52 | salinity spike in steep local gradient |
| 74 | - | 60 | salinity spike in steep local gradient |
| 76 | - | 72 | salinity spike in steep local gradient |
| 78 | - | 78 | salinity spike in steep local gradient |
| Suspect dissolve | ed oxygen va | lues | |
| 64 | 3230-3258 | 3 - | |
| 74 | 1358 | - | |
| 74 | 3664 | - | |
| 74 | 3760 | - | |
| 91 | 462-474 | - | |

<u>Table 15a:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

| stn | suspect | 2dbar values(| dbar) | stn | n suspect 2dbar values(dbar) | | | |
|-----|---------|---------------|----------------|-----|------------------------------|--------------|----------------|--|
| no. | bad | questionable | comment | no. | bad | questionable | comment | |
| | | | | | | | | |
| 13 | - | 2 | temperature ok | 71 | - | 2 | temperature ok | |
| 14 | - | 2 | temperature ok | 72 | - | 2 | temperature ok | |
| 16 | - | 2 | temperature ok | 73 | - | 2 | temperature ok | |
| 18 | - | 2 | temperature ok | 74 | - | 2 | temperature ok | |
| 63 | - | 2 | temperature ok | | | | • | |

<u>Table 15b:</u> Suspect 2 dbar-averaged dissolved oxygen data from near the surface.

| stn | • | , , | | • | t 2dbar values(dbar | r) stn | suspect | ` , |
|-----|-----|--------------|-----|-----|---------------------|--------|---------|--------------|
| no. | bad | questionable | no. | bad | questionable | no. | bad | questionable |
| | | | | | | | | |
| 19 | - | 2-24 | 52 | - | 2 | 75 | - | 2-6 |
| 20 | - | 2-14 | 53 | - | 2 | 84 | - | 2-10 |

| 25 | - | 2-10 | 67 | - | 2-14 | 85 | - | 2-10 |
|----|---|------|----|---|------|----|---|------|
| 37 | - | 2-60 | 69 | - | 2-12 | 95 | - | 2-10 |
| 38 | - | 2-12 | 70 | - | 2-12 | | | |

<u>Table 16:</u> CTD dissolved oxygen calibration coefficients. K_1 , K_2 , K_3 , K_4 , K_5 and K_6 are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 σ (for σ defined as in eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

| station number | . Κ ₁ | K ₂ K ₃ | $K_{\!\scriptscriptstyle 4}$ | K ₅ | K_6 | dox n |
|----------------------|------------------|-------------------------------|------------------------------|----------------|------------|-----------|
| 19 | 10.84 | 6.0000 -1.520 | -0.0997 | 0.5714 | 0.0001243 | 0.0836 22 |
| 20 | 11.15 | 7.0000 -1.498 | -0.1347 | 0.6687 | 0.0001243 | 0.0977 22 |
| 21 | 9.50 | 8.0000 -1.490 | -0.1347 | 0.2524 | 0.0001101 | 0.0977 22 |
| 22 | 9.79 | 6.5000 -1.318 | -0.0774 | 0.5944 | 0.0001077 | 0.1631 24 |
| 23 | 9.85 | 8.0000 -1.318 | | 0.5259 | 0.0001191 | 0.0993 24 |
| 23 24 | 11.31 | 6.0000 -1.527 | -0.0634 -0.1429 | 0.5259 | 0.0001102 | 0.1042 22 |
| 2 4 25 | 10.08 | 5.0000 -1.428 | | 0.3847 | 0.0001013 | 0.0943 23 |
| | 10.06 | | -0.0586 0.1175 | 0.1932 | 0.0001219 | |
| 26 | | 6.0000 -1.331 | -0.1175 | | | 0.1114 22 |
| 27 | 10.82 | 5.0000 -1.484 | -0.1072 | 0.3868 | 0.0001021 | 0.0833 20 |
| 28 | - | | - 0.0594 | 0.0540 | 0.0001225 | 0.0024.22 |
| 29 | 10.00 | 5.0000 -1.421 | -0.0584 | 0.0549 | 0.0001235 | 0.0821 22 |
| 30 | 13.27 | 6.3000 -1.765 | -0.1997 | 0.6450 | 0.0000960 | 0.0952 23 |
| 31 | 10.20 | 5.5000 -1.323 | -0.1257 | 0.6496 | 0.0001120 | 0.1202 22 |
| 32 | 11.22 | 6.1000 -1.513 | -0.1274 | 0.6352 | 0.0001118 | 0.1145 23 |
| 33 | 9.90 | 6.5000 -1.343 | -0.0834 | 0.4733 | 0.0001193 | 0.1101 23 |
| 34 | 11.42 | 5.0000 -1.606 | -0.1106 | 0.4598 | 0.0001185 | 0.1193 23 |
| 35 | 9.55 | 5.0000 -1.274 | -0.0870 | 0.3656 | 0.0001115 | 0.0900 23 |
| 36 | 10.62 | 5.7000 -1.462 | | 0.5355 | 0.0001164 | 0.1128 22 |
| 37 | 10.99 | 5.4000 -1.366 | -0.1729 | 0.6951 | 0.0000956 | 0.1161 22 |
| 38 | 9.83 | 8.5000 -1.300 | -0.0998 | 0.4719 | 0.0001090 | 0.1785 24 |
| 39 | 11.85 | 5.5000 -1.693 | -0.0893 | 0.9384 | 0.0001481 | 0.1395 24 |
| 40 | 9.52 | 5.0000 -1.222 | | 0.4554 | 0.0000956 | 0.1988 23 |
| 41 | 10.35 | 5.0000 -1.321 | -0.1407 | 0.5947 | 0.0000991 | 0.1704 22 |
| 42 | 10.19 | 5.0000 -1.365 | -0.1027 | 0.6043 | 0.0001209 | 0.1027 23 |
| 43 | 10.46 | 5.0000 -1.415 | -0.0988 | 0.7758 | 0.0001334 | 0.1264 23 |
| 44 | 9.98 | 5.0000 -1.276 | -0.1154 | 0.7166 | 0.0001112 | 0.1620 23 |
| 45 | 8.59 | 5.0000 -1.092 | | 0.8185 | 0.0001261 | 0.1211 23 |
| 46 | 9.40 | 7.6000 -1.077 | -0.1526 | 0.7112 | 0.0000860 | 0.0937 23 |
| 47 | 4.56 | 8.0000 -0.129 | -0.1478 | 0.5075 | 0.0000238 | 0.1100 24 |
| 48 | 9.82 | 8.0000 -1.220 | -0.1357 | 0.6939 | 0.0001045 | 0.1126 15 |
| 49 | 8.69 | 5.0000 -0.823 | -0.2138 | 0.7031 | 0.0000645 | 0.1851 23 |
| 50 | 10.13 | 5.0000 -1.288 | -0.1417 | 0.7160 | 0.0001096 | 0.1802 21 |
| 51 | 9.92 | 5.7000 -1.265 | -0.1289 | 0.6950 | 0.0001095 | 0.1700 23 |
| 52 | 9.38 | 5.0000 -0.620 | -0.3413 | 0.7189 | 0.0000302 | 0.1431 23 |
| 53 | 9.81 | 5.0000 -1.182 | -0.1388 | 0.6609 | 0.0000698 | 0.1821 11 |
| 54 | - | | - | - | - | |
| 55 | 6.97 | 5.0000 -0.663 | -0.0339 | 0.7479 | 0.0002265 | 0.2867 23 |
| 56 | 10.77 | 5.0000 -0.784 | -0.1082 | 1.7653 | 0.0002543 | 0.2701 11 |
| 57 | 7.77 | 5.0000 -0.893 | -0.0376 | 0.9939 | 0.0002700 | 0.1365 9 |
| 58 | 18.99 | 5.0000 -1.887 | -0.3220 | 1.0860 | -0.0000862 | 0.2016 12 |
| 59 | 7.80 | 6.5000 -0.828 | -0.1463 | 0.5008 | 0.0000699 | 0.2340 23 |
| 60 | 10.74 | 5.0000 -1.405 | | 0.6837 | 0.0000890 | 0.2835 22 |
| 61 | 8.56 | 5.4000 -0.752 | | 0.7231 | 0.0000545 | 0.2215 22 |
| 62 | 6.83 | 5.0000 -0.702 | | 0.3474 | 0.0000582 | 0.2236 23 |
| 63 | 9.99 | 5.0000 -1.155 | | 0.7218 | 0.0000761 | 0.2073 22 |
| | | | | | | |

| 65 66 | - | | - | - | - | |
|-------------|-------------------|---------------|---------|-------------|------------|-----------|
| 67 | 9.88 | 8.1000 -1.358 | -0.0693 | - 0.5847 | 0.0001246 | 0.0932 22 |
| | e 16: (cor | | -0.0033 | 0.3047 | 0.0001240 | 0.0932 22 |
| <u>1401</u> | <u>c 10.</u> (coi | itiliaca) | | | | |
| 68 | 10.37 | 5.0000 -1.398 | -0.0993 | 0.6389 | 0.0001149 | 0.2438 24 |
| 69 | 10.21 | 5.0000 -1.507 | | 0.5929 | 0.0001541 | 0.0993 22 |
| 70 | 10.13 | 5.0000 -1.482 | -0.0384 | 0.6813 | 0.0001547 | 0.1931 23 |
| 71 | 10.94 | 5.0000 -1.563 | -0.0789 | 0.6839 | 0.0001389 | 0.1362 23 |
| 72 | 10.30 | 7.0000 -1.405 | -0.0978 | 0.5148 | 0.0001129 | 0.1102 22 |
| 73 | 11.69 | 5.0000 -1.712 | -0.0789 | 0.6026 | 0.0001338 | 0.2344 22 |
| 74 | 11.15 | 5.0000 -1.618 | -0.0774 | 0.7047 | 0.0001443 | 0.1594 23 |
| 75 | 11.19 | 5.0000 -1.548 | -0.1200 | 0.4974 | 0.0001064 | 0.1792 22 |
| 76 | 9.81 | 5.0000 -1.417 | -0.0364 | 0.4576 | 0.0001436 | 0.1843 23 |
| 77 | 11.49 | 5.0000 -1.668 | -0.0842 | 0.6645 | 0.0001397 | 0.1952 21 |
| 78 | 15.42 | 5.0000 -2.300 | -0.1429 | 0.8493 | 0.0001510 | 0.2491 24 |
| 79 | 10.63 | 5.0000 -1.523 | -0.0686 | 0.7043 | 0.0001431 | 0.2986 24 |
| 80 | 15.38 | 4.8000 -2.256 | -0.1733 | 0.8770 | 0.0001353 | 0.3505 23 |
| 81 | 12.66 | 5.0000 -1.843 | -0.1084 | 0.8944 | 0.0001435 | 0.1945 23 |
| 82 | 12.32 | 5.0000 -1.784 | -0.1071 | 0.8816 | 0.0001374 | 0.2613 23 |
| 83 | 11.65 | 5.0000 -1.704 | -0.0841 | 0.7762 | 0.0001453 | 0.1655 22 |
| 84 | 12.00 | 5.0000 -1.788 | | 0.6134 | 0.0001404 | 0.2362 24 |
| 85 | 13.74 | 4.6000 -2.095 | -0.0979 | 0.5523 | 0.0001431 | 0.3313 23 |
| 86 | 12.92 | 5.0000 -1.943 | -0.1079 | 0.9207 | 0.0001597 | 0.1862 23 |
| 87 | 11.10 | 5.0000 -1.617 | -0.0748 | 0.7939 | 0.0001402 | 0.2204 23 |
| 88 | 12.15 | 5.0000 -1.813 | -0.0984 | 0.9811 | 0.0001700 | 0.1533 22 |
| 89 | 13.48 | 5.0000 -2.058 | -0.1033 | 0.7539 | 0.0001634 | 0.2285 24 |
| 90 | 12.95 | 5.0000 -1.975 | -0.0904 | 0.6741 | 0.0001597 | 0.1744 23 |
| 91 | 12.49 | 5.0000 -1.903 | | 0.6989 | 0.0001619 | 0.1489 22 |
| 92 | 11.68 | 5.0000 -1.778 | | 0.8059 | 0.0001793 | 0.1691 21 |
| 93 | 11.85 | 5.0000 -1.822 | | 0.7029 | 0.0001812 | 0.1999 24 |
| 94 | 11.56 | 5.0000 -1.716 | | 0.9086 | 0.0001596 | 0.2278 24 |
| 95 | 11.31 | 5.0000 -1.685 | | 0.8041 | 0.0001618 | 0.1031 24 |
| 96 | 13.48 | 5.0000 -2.135 | | 0.5469 | 0.0001834 | 0.2361 22 |
| 97 | 11.53 | 5.0000 -1.745 | | 0.6549 | 0.0001629 | 0.2228 21 |
| 98 | 11.11 | 5.0000 -1.627 | | 0.8678 | 0.0001512 | 0.1764 24 |
| 99 | 11.13 | 5.0000 -1.686 | | 0.8706 | 0.0001874 | 0.1619 22 |
| 100 | 11.73 | 5.0000 -1.816 | | 0.6922 | 0.0001936 | 0.2216 23 |
| 101 | 10.99 | 5.0000 -1.610 | | 0.6581 | 0.0001085 | 0.2108 24 |
| 102 | 11.61 | 5.0000 -1.805 | | 0.7840 | 0.0002055 | 0.2297 23 |
| 103 | 11.13 | 5.0000 -1.730 | | 0.7031 | 0.0002107 | 0.2480 23 |
| 104 | 10.63 | 5.0000 -1.549 | | 0.9403 | 0.0001587 | 0.1744 24 |
| 105 | 10.31 | 5.0000 -1.342 | | 0.7824 | -0.0000437 | 0.2751 22 |
| 106 | 7.45 | 9.8000 -0.946 | -0.0346 | 0.8315 | 0.0000151 | 0.2323 15 |

<u>Table 17:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

| station numbe | - | K_2 | K_3 | K ₄ | K ₅ | K ₆ | coef varie | ficients d |
|----------------------|--------------------|------------------|------------------|--------------------------|----------------|----------------------------|----------------|---|
| 19 | 11.9000 | 6.0000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | K ₃ K ₄ K ₅ K ₆ |
| 20 | 11.5000 | 7.0000 | -1.400 | -0.360E-01 -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 21 22 | 10.1000 | 8.0000 | -1.100 | | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 23 | 10.5500 10.7500 | 6.5000 8.0000 | -1.100 -1.100 | -0.360E-01 -0.360E-01 | 0.850 0.750 | 0.15000E-03 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 23 24 | 11.5000 | 6.0000 | -1.100 | -0.660E-01 | 0.750 | 0.15000E-03 | K₁ K₁ | $K_3 K_4 K_5 K_6$ |
| 2 4 25 | 11.3000 | 5.0000 | -1.020 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6 K_3 K_4 K_5 K_6$ |
| 26 | 10.5800 | 6.0000 | -1.020 | -0.500E-01 | 0.750 | 0.15000E-03 | K_1 | |
| 20 27 | 11.2300 | 5.0000 | -1.300 | -0.550E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6 K_3 K_4 K_5 K_6$ |
| 28 | - | - | -1.500 | -0.550L-01 - | - | 0.13000L-03 | 111 | - |
| 29 | 11.1000 | 5.0000 | -1.050 | -0.380E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 30 | 13.1500 | 6.3000 | -1.700 | -0.400E-01 | 0.750 | 0.15000E-03 | K₁ K₁ | $K_3 K_4 K_5 K_6$ |
| 31 | 10.4000 | 5.5000 | -1.200 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 32 | 11.5000 | 6.1000 | -1.400 | -0.400E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 33 | 10.6700 | 6.5000 | -1.100 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 34 | 12.1000 | 5.0000 | -1.410 | -0.500E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 35 | 10.0000 | 5.0000 | -1.100 | -0.400E-01 | 0.750 | 0.15000E-03 | K₁ K₁ | $K_3 K_4 K_5 K_6$ |
| 36 | 11.0000 | 5.7000 | -1.300 | -0.370E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 37 | 10.9000 | 5.4000 | -1.300 | -0.500E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 38 | 10.0000 | 8.5000 | -1.250 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 39 | 12.9000 | 5.5000 | -1.300 | -0.360E-01 | 0.850 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 40 | 9.4000 | 5.0000 | -1.230 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 41 | 10.5500 | 5.0000 | -1.100 | -0.700E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 42 | 11.0000 | 5.0000 | -1.100 | -0.400E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 43 | 11.0000 | 5.0000 | -1.150 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ . | $K_3 K_4 K_5 K_6$ |
| 44 | 10.3500 | 5.0000 | -1.100 | -0.360E-01 | 0.800 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 45 | 8.5000 | 5.0000 | -1.100 | -0.360E-01 | 0.800 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 46 | 9.9000 | 7.6000 | -1.000 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 47 | 4.8500 | 8.0000 | -0.040 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 48 | 10.4000 | 8.0000 | -1.100 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 49 | 8.8500 | 5.0000 | -0.850 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 50 | 10.3500 | 5.0000 | -1.110 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 51 | 10.5000 | 5.7000 | -1.100 | -0.370E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 52 | 10.8000 | 5.0000 | -0.650 | -0.600E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 53 | 9.6000 | 5.0000 | -0.470 | -0.700E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 54 | - | - | - | - | - | - | | - |
| 55 | 7.1000 | 5.0000 | -0.650 | -0.360E-01 | 0.740 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 56 | 10.2000 | 5.0000 | -0.650 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 57 | 7.8500 | 5.0000 | -0.870 | -0.360E-01 | 0.800 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 58 | 7.6500 | 5.0000 | -0.570 | -0.360E-01 | 0.670 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 59 | 8.4000 | 6.5000 | -0.800 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 60 | 10.8000 | 5.0000 | -1.120 | -0.360E-01 | 0.710 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 61 | 9.0000 | 5.4000 | -0.680 | -1.000E-01 | 0.740 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 62 | 7.1500 | 5.0000 | -0.650 | -0.600E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 63 | 10.4000 | 5.0000 | -1.020 | -0.500E-01 | 0.740 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 64 | 11.4000 | 6.0000 | -1.400 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 65 | - | - | - | - | - | - | | - |
| 66 | - | - | - | - | - | - | | - |

| 68 | 10.7000 | 5.0000 | -1.100 | -0.400E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
|---------|-------------|--------|--------|------------|-------|-------------|----------------|-------------------|
| 69 | 10.1500 | 5.0000 | -1.520 | -0.300E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| Table 1 | 7: (continu | ıed) | | | | | | |
| | | | | | | | | |
| 70 | 10.4500 | 5.0000 | -1.450 | -0.350E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 71 | 12.5000 | 5.0000 | -1.100 | -0.400E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 72 | 10.7000 | 7.0000 | -1.200 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 73 | 12.9500 | 5.0000 | -1.230 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 74 | 12.6800 | 5.0000 | -1.000 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 75 | 11.3000 | 5.0000 | -1.200 | -0.600E-01 | 0.700 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 76 | 10.1500 | 5.0000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 77 | 12.4000 | 5.0000 | -1.150 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 78 | 14.0000 | 5.0000 | -1.600 | -0.400E-01 | 0.690 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 79 | 10.4000 | 5.0000 | -1.500 | -0.500E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 80 | 13.5000 | 4.8000 | -1.400 | -0.500E-01 | 0.650 | 0.10000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 81 | 12.5500 | 5.0000 | -1.200 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 82 | 12.0500 | 5.0000 | -1.100 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 83 | 12.5000 | 5.0000 | -1.120 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 84 | 12.7000 | 5.0000 | -1.120 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 85 | 12.5000 | 4.6000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 86 | 13.3000 | 5.0000 | -1.610 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 87 | 11.8000 | 5.0000 | -1.210 | -0.360E-01 | 0.750 | 0.15000E-03 | K_1 | $K_3 K_4 K_5 K_6$ |
| 88 | 13.0000 | 5.0000 | -1.510 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 89 | 13.5000 | 5.0000 | -1.570 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 90 | 13.3000 | 5.0000 | -1.520 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 91 | 13.9000 | 5.0000 | -1.650 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 92 | 13.2000 | 5.0000 | -1.410 | -0.360E-01 | 0.700 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 93 | 14.1000 | 5.0000 | -1.600 | -0.360E-01 | 0.600 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 94 | 12.7000 | 5.0000 | -1.310 | -0.450E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 95 | 12.3000 | 5.0000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |
| 96 | 15.4000 | 5.0000 | -1.820 | -0.400E-01 | 0.690 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 97 | 13.4500 | 5.0000 | -1.420 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 98 | 12.0000 | 5.0000 | -1.200 | -0.400E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 99 | 12.9000 | 5.0000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 100 | 14.4000 | 5.0000 | -1.640 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 101 | 12.5000 | 5.0000 | -1.300 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 102 | 12.9000 | 5.0000 | -1.200 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 103 | 14.3000 | 5.0000 | -1.370 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 104 | 11.8000 | 5.0000 | -1.200 | -0.360E-01 | 0.750 | 0.15000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 105 | 11.3000 | 5.0000 | -1.150 | -0.370E-01 | 0.800 | 0.20000E-03 | K₁ | $K_3 K_4 K_5 K_6$ |
| 106 | 7.2000 | 9.8000 | -1.020 | -0.200E-01 | 0.740 | 0.20000E-03 | K ₁ | $K_3 K_4 K_5 K_6$ |

<u>Table 18:</u> Questionable dissolved oxygen Niskin bottle sample values (not deleted from hydrology data file).

| stn no. | rosette position | stn no. | rosette position |
|---------|------------------|---------|------------------|
| 1 | 2,24 | 44 | 1 |
| 12 | 1 | 48 | 1 |
| 15 | 14 | 64 | 13,14 |
| 16 | 14 | 77 | 2 |
| 17 | 14 | 80 | 9 |
| 32 | 1 | 101 | 5 |

Table 19: Questionable nutrient sample values (not deleted from hydrology data file).

| PHOSPHATE | | NITRA ⁻ | ГЕ | SILICATE | | |
|-----------|-------------------|--------------------|-----------|----------|----------|--|
| station | rosette | station | rosette | station | rosette | |
| number | position | number | position | number | position | |
| | | 2 | 2 | | | |
| 4 | 17 | 4 | 4 | | | |
| 7 | 21,22,23 | • | • | | | |
| 14 | 13 | 14 | 13 | 14 | 13 | |
| 17 | 23 | | | | | |
| 19 | 23 | | | | | |
| 21 | 23 | 21 | 19 | | | |
| 24 | 22 | | | | | |
| 25 | 23 | | | | | |
| 27 | 22 | | | | | |
| 28 | whole stn | | | | | |
| 30 | 23 | | | | | |
| 32 | 23 | | | | | |
| 34 | 23 | | | | | |
| 35 | 24 | | | | | |
| 36 | 24 | | | 27 | 0 | |
| 37 40 | 24 24 | | | 37 | 2 | |
| 40 | 24 | 42 | 11,12 | | | |
| | | 45 | 1 to 13 | | | |
| 50 | 24 | 40 | 1 10 10 | | | |
| 51 | 23 | | | | | |
| 52 | whole stn | 52 | whole stn | | | |
| 55 | 22 | | | | | |
| 56 | 22 | | | | | |
| | | 60 | whole stn | | | |
| 64 | 24 | | | | | |
| 65 | 24 | | | | | |
| 67 | 23 | | | | | |
| 68 | 23,24 | | | | | |
| 69 | 23 | | | | | |
| 71 | 23 | | | 71 | 11 | |
| 72 73 | 23 | | | 72 | 19 | |
| 73 74 | 23,24 | | | | | |
| 74 75 | 23,24 22,23,24 | | | | | |
| 76 | 23,24 | | | | | |
| 10 | 20,27 | | | | | |

83 22

103 22 to 24

<u>Table 20:</u> Laboratory temperatures T₁ at the times of nutrient analyses. Note that a mean value of 21.5°C was used for conversion to gravimetric units for WOCE format data (Appendix 2).

| stn | T_{L} | stn | T_l | stn | T_1 | stn | T_1 | stn | T_{l} | stn | T ₁ |
|-----|---------|-----|-------|-----|-------|-----|-------|-----|---------|-----|----------------|
| no. | (°C) | no. | (°C) | no. | (°C) | no. | | | (°C) | no. | (°C) |
| 1 | 22 | | 21.7 | | 21 | | 22 | | 21.5 | 101 | 21.5 |
| 2 | 22 | 22 | 22 | 42 | 21 | | 21 | | 21.5 | 102 | 21.5 |
| 3 | 22 | 23 | 21.5 | 43 | 21.5 | 63 | 21.5 | 83 | 22 | 103 | 21 |
| 4 | 23 | 24 | 22 | 44 | 21 | 64 | 21 | 84 | 22 | 104 | 21.5 |
| 5 | - | 25 | 20.5 | 45 | 22 | 65 | 22 | 85 | 22 | 105 | 21.5 |
| 6 | 21 | 26 | 21 | 46 | 21 | 66 | 22 | 86 | 22 | 106 | 21.5 |
| 7 | 22 | 27 | 21 | 47 | 21 | 67 | 22 | 87 | 23 | | |
| 8 | 20.5 | 28 | 21 | 48 | 21 | 68 | 21.5 | 88 | 22.5 | | |
| 9 | 21 | 29 | 21 | 49 | 21 | 69 | 22 | 89 | 22.5 | | |
| 10 | 22.5 | 30 | 21 | 50 | 20.5 | 70 | 22 | 90 | 23.5 | | |
| 11 | 21.5 | 31 | 21.5 | 51 | 21.5 | 71 | 22 | 91 | 22.5 | | |
| 12 | 21.5 | 32 | 21 | 52 | 22 | 72 | 21.5 | 92 | 21.5 | | |
| 13 | 21.5 | 33 | 20.5 | 53 | 21 | 73 | 21.5 | 93 | 22 | | |
| 14 | 22 | 34 | 22 | 54 | 19.5 | 74 | 22 | 94 | 22 | | |
| 15 | 22 | 35 | 21 | 55 | 20 | 75 | 22 | 95 | 21 | | |
| 16 | 21.5 | 36 | 21 | 56 | 19.5 | 76 | 21.5 | 96 | 21.5 | | |
| 17 | 21 | 37 | 21.5 | 57 | 21 | 77 | 21.5 | 97 | 21.5 | | |
| 18 | 22.5 | 38 | 21.5 | 58 | 21 | 78 | 21.5 | 98 | 21.5 | | |
| 19 | 21 | 39 | 21 | 59 | 21 | 79 | 22 | 99 | 22 | | |
| 20 | 22 | 40 | 21 | 60 | 22 | 80 | 21.5 | 100 | 22 | | |

<u>Table 21:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

| | n rosette er position | station number | rosette position | station number | rosette position |
|----|--------------------------|-------------------|------------------|-------------------|---------------------|
| | | | | | |
| 19 | 22 | 46 | 22 | 77 | 19 |
| 20 | 22 | 48 | 1 | 82 | 20 |
| 21 | 22 | 49 | 23 | 83 | 19 |
| 24 | 21 | 50 | 1,22,23 | 85 | 19 |
| 26 | 21,22 | 52 | 23 | 88 | 18 |
| 27 | 21,22 | 55 | 22 | 90 | 18 |
| 29 | 12,22 | 60 | 22,24 | 91 | 18,22 |
| 30 | 22 | 61 | 20,24 | 92 | 13,23 |
| 31 | 12,23 | 62 | 24 | 96 | 10 |
| 32 | 23 | 63 | 21,24 | 97 | 11 |
| 34 | 23 | 64 | 22 | 99 | 14,18 |
| 35 | 22 | 67 | 24 | 100 | 14 |
| 36 | 21,23 | 69 | 21,24 | 102 | 22 |
| 37 | 23 | 70 | 24 | 105 | 7,8 |
| 40 | 3 | 71 | 21 | 106 | 17,18 |
| 41 | 22 | 72 | 20,23 | | |
| 42 | 21 | 73 | 20 | | |

<u>Table 22:</u> Stations containing fluorescence (fl) and photosynthetically active radiation (par) 2 dbar-averaged data.

| stations with fl data | stations with par data | | | |
|-----------------------|-------------------------------|--|--|--|
| 5 to 12 | 2 to 4 5 to 12 13 to 76 | | | |

<u>Table 23:</u> Protected and unprotected reversing thermometers used for cruise AU9404 (serial numbers are listed).

| protected | thermometers | | |
|-----------|-------------------------------|-----------------------|-------------------------------|
| station | rosette position 24 | rosette position 12 | rosette position 2 |
| numbers | thermometers | thermometers | thermometers |
| 2 | - | 12094,11973 (pos. 13) | - |
| 3 to 8 | 12095,12096 | 12119,12120 | 12094,11973 |
| 9 to 63 | 12095,12096 | 12119,12120 | 12094,11637 |
| 64 to 102 | 12095,12096 | 12119,12120 | 12094,11973 |
| 103 to 10 | 6 11637,11638 | 12094,11973 | 12119,12120 |
| 107 1 | 1638 (pos. 23); 11637 (pos. 2 | | 94 (pos. 12); 12096 (pos. 8); |
| | 12119 (pos. 5); 12120 (pos. | 2) | |

unprotected thermometers

| station | rosette position 12 | rosette position 2 |
|-----------|---------------------|--------------------|
| numbers | thermometers | thermometers |
| 2 | 11992 (pos. 13) | - |
| 3 to 35 | 11993 | 11992 |
| 36 to 107 | 11992 | 11993 |
| | | |

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APPENDIX 1 CTD Instrument Calibrations

<u>Table A1.1:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9404. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

| | CTD serial 110 coefficient | 3 (unit no. 7) value of coefficient | | CTD serial 119 coefficient | 93 (unit no. 5) value of coefficient | | | |
|------------------|---|---|---|---|--|--|--|--|
| | re calibration coe Calibration Fact pcal0 pcal1 | | | re calibration cod Calibration Fac pcal0 pcal1 | efficients ility - 13/09/1994 -9.273027 1.008386e-01 | | | |
| | pcal2 pcal3 | 6.393209e-9 0.0 | | pcal2 pcal3 | 0.0 0.0 | | | |
| | m temperature c Calibration Faci | alibration coefficients ility - 23/09/1994 | CSIRO | Calibration Fac | ralibration coefficients ility - 23/09/1994 (with rom cruise thermometer data) | | | |
| | Tcal0 | 0.70500e-02 | | Tcal0 | -0.62088e-02 - 0.007 | | | |
| | Tcal1 | 0.50000e-03 | | Tcal1 | 0.49880e-03 | | | |
| | Tcal2 | 0.35049e-11 | | Tcal2 | 0.27541e-11 | | | |
| • | re temperature c al Oceanics - July | alibration coefficients | pressure temperature calibration coefficients General Oceanics - July 1993 | | | | | |
| Conord | Tpcal0 | 1.062859e+02 | Goriora | Tpcal0 | 2.238391e+02 | | | |
| | Tpcal1 | -2.117688e-03 | | Tpcal1 | -1.155218e-02 | | | |
| | Tpcal2 | 2.597323e-09 | | Tpcal2 | 2.418139e-07 | | | |
| | Tpcal3 | 0.000000 | | Tpcal3 | -2.007116e-12 | | | |
| coeffic press | coefficients for temperature correction to coefficients for temperature correction to | | | | | | | |
| • | ure al Oceanics - July | v 1002 | Genera | are al Oceanics - Jul | v 1003 | | | |
| Genera | ai Oceanics - July | y 1333 | Genera | ii Oceanics - Jui | у тэээ | | | |
| | T_{o} | 21.50 | | T_0 | 22.00 | | | |
| | S_1 | -5.9127e-07 | | S ₁ | -2.3599e-06 | | | |
| | _ | | | _ | | | | |

preliminary polynomial coefficients applied to fluorescence (fl) and photosynthetically active radiation (par) raw digitiser counts (supplied by manufacturer)

-1.6700e-01

| f0 | -2.699918e+01 |
|------|---------------|
| f1 | 8.239746e-04 |
| f2 | -2.071294e-22 |
| | |
| par0 | -4.499860 |
| par1 | 1.373290e-04 |

-3.2430e-01

 S_2

APPENDIX 2: WOCE Data Format Addendum

A2.1 INTRODUCTION

This Appendix is relevant only to data submitted to the WHP Office. For WOCE format data, file format descriptions as detailed earlier in this report should be ignored. Data files submitted to the WHP Office are in the standard WOCE format as specified in Joyce et al. (1991).

A2.2 CTD 2 DBAR-AVERAGED DATA FILES

- * CTD 2 dbar-averaged file format is as per Table 3.12 of Joyce et al. (1991), except that measurements are centered on even pressure bins (with first value at 2 dbar).
- * CTD temperature and salinity are reported to the third decimal place only.
- * Files are named as in the CTD methodology, except that for WOCE format data the suffix ".all" is replaced with ".ctd".
- * The quality flags for CTD data are defined in Table A2.1. Data quality information is detailed in earlier sections of this report.

A2.3 HYDROLOGY DATA FILES

- * Hydrology data file format is as per Table 3.7 of Joyce et al. (1991), with quality flags defined in Tables A2.2 and A2.3.
- * Files are named as in the CTD methodology, except that for WOCE format data the suffix ".bot" is replaced by ".sea".
- * The total value of nitrate+nitrite only is listed.
- * Silicate and nitrate+nitrite are reported to the first decimal place only.
- * CTD temperature (including theta), CTD salinity and bottle salinity are all reported to the third decimal place only.
- * CTD temperature (including theta), CTD pressure and CTD salinity are all derived from upcast CTD burst data; CTD dissolved oxygen is derived from downcast 2 dbar-averaged data.
- * Raw CTD pressure values are not reported.
- * SAMPNO is equal to the rosette position of the Niskin bottle.

A2.4 CONVERSION OF UNITS FOR DISSOLVED OXYGEN AND NUTRIENTS

A2.4.1 Dissolved oxygen

Niskin bottle data

For the WOCE format files, all Niskin bottle dissolved oxygen concentration values have been converted from volumetric units μ mol/I to gravimetric units μ mol/kg, as follows. Concentration C_k in μ mol/kg is given by

$$C_k = 1000 C_1 / \rho(\theta, s, 0)$$
 (eqn A2.1)

where C_1 is the concentration in μ mol/I, 1000 is a conversion factor, and $\rho(\theta,s,0)$ is the potential density at zero pressure and at the potential temperature θ , where potential temperature is given by

for the *in situ* temperature T, salinity s and pressure p values at which the Niskin bottle was fired. Note that T, s and p are upcast CTD burst data averages.

CTD data

In the WOCE format files, CTD dissolved oxygen data are converted to μ mol/kg by the same method as above, except that T, s and p in eqns A2.1 and A2.2 are CTD 2 dbar-averaged data.

A2.4.2 Nutrients

For the WOCE format files, all Niskin bottle nutrient concentration values have been converted from volumetric units μ mol/I to gravimetric units μ mol/kg using

$$C_k = 1000 C_1 / \rho(T_1, s, 0)$$
 (eqn A2.3)

where 1000 is a conversion factor, and $\rho(T_I,s,0)$ is the water density in the hydrology laboratory at the laboratory temperature T_I and at zero pressure. Note that T_I =21.5°C was used for all stations. Upcast CTD burst data averages are used for s.

<u>Table A2.1:</u> Definition of quality flags for CTD data (after Table 3.11 in Joyce et al., 1991). These flags apply both to CTD data in the 2 dbar-averaged *.ctd files, and to upcast CTD burst data in the *.sea files.

| flag | definition |
|------|-----------------------------------|
| 1 | not calibrated with water samples |
| 2 | acceptable measurement |
| 3 | questionable measurement |
| 4 | bad measurement |
| 5 | measurement not reported |
| 6 | interpolated value |
| 7,8 | these flags are not used |
| 9 | parameter not sampled |
| | |

<u>Table A2.2:</u> Definition of quality flags for Niskin bottles (i.e. parameter BTLNBR in *.sea files) (after Table 3.8 in Joyce et al., 1991).

| flag | definition |
|------|--|
| 1 | this flag is not used |
| 2 | no problems noted |
| 3 | bottle leaking, as noted when rosette package returned on deck |
| 4 | bottle did not trip correctly |
| 5 | bottle leaking, as noted from data analysis |
| 6 | bottle not fired at correct depth, due to misfiring of rosette pylon |
| 7,8 | these flags are not used |
| 9 | samples not drawn from this bottle |

<u>Table A2.3:</u> Definition of quality flags for water samples in *.sea files (after Table 3.9 in Joyce et al., 1991).

| flag | definition |
|------|--------------------------------------|
| 1 | this flag is not used |
| 2 | acceptable measurement |
| 3 | questionable measurement |
| 4 | bad measurement |
| 5 | measurement not reported |
| 7 | manual autoanalyser peak measurement |
| 6,8 | these flags are not used |
| 9 | parameter not sampled |

A2.5 STATION INFORMATION FILES

- * File format is as per section 2.2.2 of Joyce et al. (1991), and files are named as in the CTD methodology, except that for WOCE format data the suffix ".sta" is replaced by ".sum".
- * All depths are calculated using a uniform speed of sound through the water column of 1498 ms⁻¹. Reported depths are as measured from the water surface. Missing depths are due to interference of the ship's bow thrusters with the echo sounder signal.
- * An altimeter attached to the base of the rosette frame (approximately at the same vertical position as the CTD sensors) measures the elevation (or height above the bottom) in metres. The elevation value at each station is recorded manually from the CTD data stream display at the bottom of each CTD downcast. Motion of the ship due to waves can cause an error in these manually recorded values of up to ± 3 m.
- * Lineout (i.e. meter wheel readings of the CTD winch) were unavailable.

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CFC-11 and CFC-12 Measurements on AU9404 (WOCE SR3 and S4)

(Following discussion provided by John Bullister, 27 April 1997)

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CFC Sampling Procedures and Data Processing

CFC water samples were usually the first samples collected from the 10 liter bottles. Care was taken to co-ordinate the sampling of CFCs with other gas samples to minimize the time between the inital opening of each bottle and the completion of sample drawing. In most cases, all dissolved gas samples were collected within several minutes of the initial opening of each bottle. CFC samples were collected in 100 ml precision glass syringes and held immersed in a water bath until processing. For air sampling, a ~100 meter length of 3/8" OD Dekaron tubing was run from the CFC lab van to the bow of the ship. Air was sucked through this line into the CFC van using an Air Cadet pump. The air was compressed in the pump, and the downstream pressure held at about 1.5 atm using a back pressure regulator. A tee allowed a flow (~100 cc/min) of the compressed air to be directed to the gas sample valves, while the bulk of the air (>7 liter/minute) was vented through the back pressure regulator.

Concentrations of CFC-11 and CFC-12 in air samples, seawater and gas standards on the cruise were measured by shipboard electron capture gas chromatography, using techniques similiar to those described by Bullister and Weiss (1988). The CFC analytical system functioned well during this expedition.

Analytical blanks for the water stripping process were determined and subtracted from the measured water sample concentrations. Both gas and water sample analytical blanks were very low for most of the expedition. In a few cases, for very low concentration water samples and a higher than average water sample analytical blank, subtraction of the water sample CFC analytical blank from the measured CFC water sample concentration yielded negative reported concentration values.

Concentrations of CFC-11 and CFC-12 in air, seawater samples and gas standards are reported relative to the SIO93 calibration scale (Cunnold, et. al., 1994). CFC concentrations in air and standard gas are reported in units of mole fraction CFC in dry gas, and are typically in the parts-per-trillion (ppt) range. Dissolved CFC concentrations are given in units of picomoles of CFC per kg seawater (pmol/kg). CFC concentrations in air and seawater samples were determined by fitting their chromatographic peak areas to multi-point calibration curves, generated by pressurizing sample loops and injecting known volumes of gas from a CFC working standard (PMEL cylinder 33790) into the analytical instrument. The concentrations of CFC-11 and CFC-12 in this working standard were calibrated versus a primary CFC standard (36743) (Bullister, 1984) before the cruise and a secondary standard (32386) before and after the cruise. No measurable drift between the working standards could be detected during this interval. Full range calibration curves were run 11 times during the cruise. Single injections of a fixed volume of standard gas at one atmosphere were run much more frequently (at intervals of 1 to 2 hours) to monitor short term changes in detector sensitivity. We estimate a precision (1 standard deviation) for dissolved CFC measurements on this cruise of about 1%, or 0.005 pmol/kg, whichever is greater (see listing of replicate samples given at the end of this report).

As expected, low (~0.01 pmol/kg) but non-zero CFC concentrations were measured in deep samples along the northern ends of the SR3 section. Deep and bottom CFC concentrations increased significantly southward along the section. It is likely that most of the deep CFC signals observed on SR3, which are strongly correlated with elevated dissolved oxygen and cold temperatures, are due to deep ventilation processes in this high latitude region, and not simply blanks due of the sampling and analytical procedures. The measured levels of CFC in deep water samples on the northern end of SR3 are considerable higher than those found on WOCE sections in the low latitude Pacific and Indian Oceans. For example, typical measured deep water CFC measurements along WOCE section I2 (at about 8S) were ~0.003 pmol/kg for CFC-11 and <0.001 for CFC-12. Since no "zero" concentration CFC water was present anywhere along SR3 or SR4, and an earlier occupation of SR3 in 1991 showed similar low levels of CFCs along the northern end of this section, no corrections for 'sampling blanks' have been applied to the reported CFC signals for SR3 or SR4.

A number of CFC samples (from a total of ~1500) had clearly anomolous CFC-11 and/or CFC-12 concentrations relative to adjacent samples. These appeared to occur more or less randomly, and were not clearly associated with other features in the water column (eg. elevated oxygen concentrations, salinity or temperature features, etc.). This suggests that the high values were due to isolated low-level CFC contamination events. These samples are included in this report and are flagged as either 3 (questionable) or 4 (bad) measurements. 34 analyses of CFC-11 were assigned a flag of 3 and 49 analyses of CFC-12 were assigned a flag of 3. 82 analyses of CFC-11 were assigned a flag of 4 and 70 CFC-12 samples assigned a flag of 4.

In addition to the file of mean CFC concentrations reported for each water sample (keyed to the unique station:sample ID), tables of the following are included in this report:

Table 2a. AU9404 Replicate dissolved CFC-11 analyses

Table 2b. AU9404 Replicate dissolved CFC-12 analyses

Table 3. AU9404 CFC air measurements

Table 4. AU9404 CFC air measurements interpolated to station locations

A value of -9.0 is used for missing values in the listings.

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| Stn 1 | | n CFC-11 | Stn | | CFC-11 | Stn | | CFC-11 |
|----------|-----|----------------|----------|----------|----------|----------|----------|----------------|
| | | (pmol/kg) | | | pmol/kg) | | | pmol/kg) |
| 1 | 2 | 0.059 | 18 | 204 | 0.480 | 35 | 24 | 6.310 |
| 1 | 2 | 0.090 | 18 | 204 | 0.481 | 35 | 24 | 6.268 |
| 4 | 1 | 1.434 | 19 | 24 | 6.419 | 35 | 107 | 0.150 |
| 4 | 1 | 1.444 | 19 | 24 | 6.378 | 35 | 107 | 0.155 |
| 4 | 11 | 0.155 | 21 | 13 | 0.138 | 37 | 1 | 1.546 |
| 4 | 11 | 0.151 | 21 | 13 | 0.135 | 37 | 1 | 1.560 |
| 4 | 13 | 0.326 | 21 | 24 | 6.406 | 37 | 2 | 1.226 |
| 4 | 13 | 0.360 | 21 | 24 | 6.396 | 37 | 2 | 1.261 |
| 4 | 18 | 6.734 | 23 | 1 | 1.631 | 37 | 11 | 0.073 |
| 4 | 18 | 6.843 | 23 | 1 | 1.620 | 37 | 11 | 0.078 |
| 9 | 9 | 0.561 | 23 | 20 | 0.645 | 37 | 16 | 0.195 |
| 9 | 9 | 0.564 | 23 | 20 | 0.617 | 37 | 16 | 0.202 |
| 10 | 1 | 1.523 | 23 | 24 | 6.398 | 37 | 24 | 6.379 |
| 10 | 1 | 1.528 | 23 | 24 | 6.398 | 37 | 24 | 6.371 |
| 10 | 13 | 0.459 | 23 | 204 | 0.425 | 38 | 1 | 1.499 |
| 10 | 13 | 0.459 | 23 | 204 | 0.441 | 38 | 1 | 1.501 |
| 10 | 24 | 6.203 | 25 | 23 | 6.216 | 39 | 1 | 1.784 |
| 10 | 24 | 6.406 | 25 | 23 | 6.200 | 39 | 1 | 1.784 |
| 12 | 11 | 0.329 | 25 | 204 | 0.284 | 39 | 6 | 0.221 |
| 12 | 11 | 0.321 | 25 | 204 | 0.290 | 39 | 6 | 0.222 |
| 14 | 2 | 1.480 | 26 | 11 | 0.094 | 39 | | 0.105 |
| 14 | 2 | 1.520 | 26 | 11 | 0.096 | 39 | | 0.107 |
| 14 | 5 | 0.668 | 26 | 11 | 0.097 | 39 | | 0.334 |
| 14 | 5 | 0.645 | 26 | 11 | 0.084 | 39 | 18 | 0.340 |
| 14 | 6 | 0.548 | 26 | 12 | 0.107 | 39 | 23 | 5.562 |
| 14 | 6 | 0.577 | 26 | 12 | 0.107 | 39 | | 5.529 |
| 14 | 6 | 0.571 | 26 | 12 | 0.119 | 40 | | 0.095 |
| 14 | 9 | 0.397 | 26 | 12 | 0.119 | 40 | | 0.093 |
| 14 | 9 | 0.396 | 26 | 13 | 0.162 | 41 | 1 | 1.390 |
| 14 | 11 | 0.390 | 26 | 13 | 0.162 | 41 | 1 | 1.385 |
| 14 | 11 | 0.279 | 26 | 13 | 0.154 | 41 | 2 | |
| | 13 | | | | | | 2 | 0.886 |
| 14 | 13 | 0.133 | 26 | 15 | 0.195 | 41 | | 0.879 0.092 |
| 14 14 | 21 | 0.135 | 26 26 | 15 15 | 0.220 | 41 41 | 11 11 | |
| | 21 | 0.905 0.926 | 26 26 | | 0.230 | | | 0.084 |
| 14 | | | - | 15 45 | 0.189 | 41 | 14 | 0.104 |
| 14 | 122 | | 26 | 15 | 0.225 | 41 | 14 | 0.103 |
| 14 | 122 | | 31 | 5 | 0.197 | 41 | 16 | 0.176 |
| 18 | 1 | 1.345 | 31 | 5 | 0.190 | 41 | 16 | 0.201 |
| 18 | 1 | 1.295 | 31 | 24 | 6.464 | 41 | 24 | 6.387 |
| 18 | 2 | 0.916 | 31 | 24 | 6.491 | 41 | 24 | 6.397 |
| 18 | 2 | 0.986 | 32 | 11 | 0.123 | 41 | 107 | 0.091 |
| 18 | 6 | 0.207 | 32 | 11 | 0.123 | 41 | | 0.092 |
| 18 | 6 | 0.247 | 32 | 11 | 0.132 | 41 | | 2.998 |
| 18 | 8 | 0.152 | 33 | 1 | 1.661 | 41 | 222 | 3.009 |
| 18 | 8 | 0.159 | 33 | 1 | 1.641 | 42 | | 0.062 |
| 18 | 16 | 0.259 | 33 | 12 | 0.104 | 42 | | 0.061 |
| 18 | 16 | 0.238 | 33 | 12 | 0.110 | 43 | | 0.078 |
| 18 | 20 | 0.880 | 33 | 24 | 6.252 | 43 | | 0.079 |
| 18 | 20 | 0.832 | 33 | 24 | 6.271 | 43 | | 0.224 |
| 18 | 24 | 6.303 | 35 | 1 | 2.329 | 43 | | 0.225 |
| 18 | 24 | 6.518 | 35 | 1 | 2.339 | 43 | | 0.140 |
| 18 | 122 | | 35 | 11 | 0.085 | 43 | | 0.144 |
| 18 | 122 | 4.890 | 35 | 11 | 0.066 | 45 | | 0.631 |
| | | | | | | 45 | 2 | 0.596 |
| | | | | | | | | |

| Stn | Niskin (| | Stn | Niskin C | CFC-11 | Stn | Niskin C | |
|-----|----------|--------|----------|----------|--------|-----|----------|--------|
| | (pm | ol/kg) | | (pm | ol/kg) | | | ol/kg) |
| 45 | 5 | 0.305 | 49 | 107 | 0.354 | 61 | 24 | 6.306 |
| 45 | 5 | 0.308 | 49 | 107 | 0.357 | 61 | 24 | 6.250 |
| 45 | 8 | 0.154 | 50 | 1 | 1.575 | 62 | 1 | 1.815 |
| 45 | 8 | 0.143 | 50 | 1 | 1.577 | 62 | 1 | 1.805 |
| 45 | 11 | 0.150 | 50 | 6 | 0.434 | 63 | 2 | 2.139 |
| 45 | 11 | 0.142 | 50 | 6 | 0.405 | 63 | 2 | 2.135 |
| 45 | 14 | 0.245 | 50 | 11 | 0.090 | 63 | 12 | 0.337 |
| | | | | | | | | |
| 45 | 14 | 0.248 | 50 | 11 | 0.089 | 63 | 12 | 0.334 |
| 45 | 20 | 0.558 | 50 | 16 | 0.216 | 63 | 222 | 4.159 |
| 45 | 20 | 0.583 | 50 | 16 | 0.212 | 63 | 222 | 4.140 |
| 45 | 222 | 3.436 | 50 | 24 | 5.514 | 65 | 1 | 2.221 |
| 45 | 222 | 3.621 | 50 | 24 | 5.571 | 65 | 1 | 2.220 |
| 47 | 1 | 0.179 | 51 | 1 | 1.492 | 65 | 24 | 6.235 |
| 47 | 1 | 0.177 | 51 | 1 | 1.496 | 65 | 24 | 6.264 |
| 47 | 20 | 4.101 | 51 | 5 | 0.434 | 67 | 1 | 1.857 |
| 47 | 20 | 4.084 | 51 | 5 | 0.438 | 67 | 1 | 1.848 |
| 48 | 1 | 0.976 | 51 | 10 | 0.090 | 67 | 17 | 0.242 |
| 48 | 1 | 1.014 | 51 | 10 | 0.089 | 67 | 17 | 0.225 |
| 48 | 2 | 0.901 | 51 | 17 | 0.377 | 67 | 107 | 0.121 |
| 48 | 2 | 0.900 | 51 | 17 | 0.375 | 67 | 107 | 0.123 |
| 48 | 6 | 0.333 | 51 | 24 | 5.237 | 68 | 9 | 0.064 |
| 48 | 6 | 0.335 | 51 | 24 | 5.206 | 68 | 9 | 0.061 |
| | | | | | | | | |
| 48 | 9 | 0.170 | 51 | 103 | 1.036 | 68 | 11 | 0.071 |
| 48 | 9 | 0.168 | 51 | 103 | 1.028 | 68 | 11 | 0.068 |
| 48 | 11 | 0.170 | 54 | 1 | 0.104 | 69 | 1 | 1.501 |
| 48 | 11 | 0.175 | 54 | 1 | 0.102 | 69 | 1 | 1.503 |
| 48 | 11 | 0.173 | 54 | 6 | 0.104 | 69 | 6 | 0.160 |
| 48 | 11 | 0.172 | 54 | 6 | 0.105 | 69 | 6 | 0.151 |
| 48 | 13 | 0.211 | 54 | 11 | 0.105 | 69 | 11 | 0.065 |
| 48 | 13 | 0.210 | 54 | 11 | 0.118 | 69 | 11 | 0.066 |
| 48 | 15 | 4.573 | 54 | 12 | 0.106 | 69 | 17 | 0.312 |
| 48 | 15 | 4.615 | 54 | 12 | 0.108 | 69 | 17 | 0.313 |
| 48 | 204 | 0.564 | 54 | 18 | 0.109 | 69 | 20 | 1.206 |
| 48 | 204 | 0.566 | 54 | 18 | 0.106 | 69 | 20 | 1.221 |
| 49 | 1 | 1.147 | 54 | 23 | 0.110 | 69 | 23 | 6.537 |
| 49 | 1 | 1.150 | 54 | 23 | 0.109 | 69 | 23 | 6.488 |
| 49 | 5 | 0.618 | 54 | 24 | 0.112 | 69 | 103 | 0.593 |
| 49 | 5 | 0.616 | 54 | 24 | 0.108 | 69 | 103 | 0.593 |
| 49 | 9 | 0.211 | 54 | 24 | 0.129 | 71 | 1 | 1.288 |
| | | 0.211 | 54 54 | | | | 1 | |
| 49 | 9 | | | 24 | 0.105 | 71 | | 1.284 |
| 49 | 11 | 0.129 | 55 | 11 | 4.834 | 71 | 11 | 0.051 |
| 49 | 11 | 0.129 | 55 | 11 | 4.862 | 71 | 11 | 0.055 |
| 49 | 13 | 0.201 | 55 | 18 | 4.124 | 71 | 20 | 1.296 |
| 49 | 13 | 0.198 | 55 | 18 | 4.110 | 71 | 20 | 1.289 |
| 49 | 15 | 0.254 | 55 | 24 | 6.432 | 71 | 24 | 6.049 |
| 49 | 15 | 0.250 | 55 | 24 | 6.405 | 71 | 24 | 6.020 |
| 49 | 17 | 0.429 | 60 | 1 | 2.348 | 73 | 1 | 0.269 |
| 49 | 17 | 0.425 | 60 | 1 | 2.384 | 73 | 1 | 0.271 |
| 49 | 21 | 1.756 | 60 | 1 | 2.360 | 73 | 8 | 0.050 |
| 49 | 21 | 1.755 | 61 | 6 | 1.094 | 73 | 8 | 0.050 |
| 49 | 24 | 4.649 | 61 | 6 | 1.099 | 73 | 10 | 0.061 |
| 49 | 24 | 4.692 | 61 | 11 | 0.430 | 73 | 10 | 0.058 |
| 49 | 103 | 1.021 | 61 | 11 | 0.433 | 73 | 11 | 0.071 |
| 49 | 103 | 1.034 | | | - | 73 | 11 | 0.069 |
| | | | | | | | | |

| Stn | | CFC-11 | Stn | | CFC-11 | Stn | | CFC-11 |
|------------------|----------|---------|-----|-----|---------|-----|-----|---------|
| | | nol/kg) | | | mol/kg) | | | mol/kg) |
| 73 | 17 | 0.705 | 85 | 20 | 4.731 | 97 | 1 | 0.005 |
| 73 | 17 | 0.701 | 85 | 20 | 4.735 | 97 | 1 | 0.005 |
| 73 | 23 | 5.624 | 86 | 8 | 0.061 | 97 | 14 | 3.392 |
| 73 | 23 | 5.676 | 86 | 8 | 0.064 | 97 | 14 | 3.393 |
| 73 | 103 | 0.130 | 86 | 11 | 0.209 | 97 | 18 | 3.762 |
| 73 | 103 | 0.128 | 86 | 11 | 0.230 | 97 | 18 | 3.768 |
| 74 | 1 | 0.246 | 86 | 17 | 2.235 | 97 | 204 | 0.008 |
| 74 | 1 | 0.246 | 86 | 17 | 2.221 | 97 | 204 | 0.010 |
| 74 | 12 | 0.123 | 86 | 23 | 4.428 | 98 | 1 | 0.004 |
| 74 | 12 | 0.120 | 86 | 23 | 4.491 | 98 | 1 | 0.006 |
| 74 | 24 | 5.503 | 89 | 6 | 0.026 | 98 | 105 | 0.006 |
| 74 | 24 | 5.531 | 89 | 6 | 0.024 | 98 | 105 | 0.006 |
| 75 | 1 | 0.239 | 89 | 24 | 4.559 | 99 | 10 | 0.691 |
| 75 | 1 | 0.267 | 89 | 24 | 4.549 | 99 | 10 | 0.689 |
| 75 | 5 | 0.081 | 89 | 105 | 0.022 | 99 | 15 | 3.683 |
| 75 | 5 | 0.080 | 89 | 105 | 0.021 | 99 | 15 | 3.662 |
| 75 | 11 | 0.083 | 89 | 204 | 0.027 | 99 | 20 | 3.845 |
| 75 | 11 | 0.084 | 89 | 204 | 0.021 | 99 | 20 | 3.839 |
| 75 | 16 | 0.554 | 91 | 10 | 0.085 | 99 | 105 | 0.037 |
| 75 | 16 | 0.559 | 91 | 10 | 0.083 | 99 | 105 | 0.041 |
| 75 | 23 | 5.604 | 91 | 15 | 0.911 | 101 | 10 | 0.632 |
| 75 | 23 | 5.605 | 91 | 15 | 0.915 | 101 | 10 | 0.625 |
| 76 | 1 | 0.135 | 91 | 105 | 0.011 | 101 | 15 | 3.559 |
| 76 | 1 | 0.133 | 91 | 105 | 0.011 | 101 | 15 | 3.556 |
| 76 76 | 19 | 1.163 | 92 | 204 | 0.030 | 101 | 20 | 3.655 |
| 76 76 | 19 | 1.184 | 92 | 204 | 0.030 | 101 | 20 | 3.667 |
| 76 76 | 24 | | 93 | 6 | 0.029 | 101 | | 0.113 |
| | 24 24 | 5.573 | | 6 | | | | |
| 76 77 | | 5.583 | 93 | | 0.020 | 101 | | 0.118 |
| 77 77 | 1 | 0.137 | 93 | 16 | 2.203 | 103 | | 0.006 |
| 77 77 | 1 | 0.153 | 93 | 16 | 2.181 | 103 | | 0.003 |
| 77 77 | 6 | 0.090 | 93 | 20 | 3.621 | 103 | | 0.009 |
| 77 77 | 6 | 0.077 | 93 | 20 | 3.607 | 103 | | 0.007 |
| 77 77 | 18 | 1.569 | 94 | 6 | 0.026 | 103 | | 0.972 |
| 77 | 18 | 1.556 | 94 | 6 | 0.025 | 103 | | 0.976 |
| 77 | 24 | 5.500 | 95 | 1 | 0.006 | 103 | | 2.974 |
| 77 - 2 | 24 | 5.472 | 95 | 1 | 0.005 | 103 | | 2.981 |
| 79 | 1 | 0.073 | 95 | 1 | 0.006 | 105 | | 2.988 |
| 79 | 1 | 0.068 | 95 | 9 | 0.143 | 105 | 23 | 2.983 |
| 79 | 10 | 0.069 | 95 | 9 | 0.143 | | | |
| 79 | 10 | 0.064 | 95 | 16 | 3.227 | | | |
| 81 | 13 | 0.499 | 95 | 16 | 3.242 | | | |
| 81 | 13 | 0.494 | 95 | 19 | 3.687 | | | |
| 81 | 19 | 4.397 | 95 | 19 | 3.664 | | | |
| 81 | 19 | 4.412 | 95 | 23 | 3.732 | | | |
| 83 | 2 | 0.041 | 95 | 23 | 3.736 | | | |
| 83 | 2 | 0.037 | 95 | 103 | 0.011 | | | |
| 83 | 5 | 0.034 | 95 | | 0.012 | | | |
| 83 | 5 | 0.035 | 95 | | 0.024 | | | |
| 85 | 2 | 0.022 | 95 | 105 | 0.026 | | | |
| 85 | 2 | 0.017 | 96 | | 0.009 | | | |
| 85 | 8 | 0.039 | 96 | 105 | 0.013 | | | |
| 85 | 8 | 0.042 | 96 | 204 | 0.006 | | | |
| 85 | 15 | 1.043 | 96 | 204 | 0.008 | | | |
| 85 | 15 | 1.041 | | | | | | |
| | | | | | | | | |

| Stn | Niskir | n CFC-12 | Stn | Niskin | CFC-12 | Stn | Niski | n CFC-12 |
|-----|--------|----------|-----|--------|---------|-----|-------|-----------|
| | | pmol/kg) | | | mol/kg) | | | (pmol/kg) |
| 1 | 2 ` | 0.037 | 18 | 204 | 0.226 | 29 | 2 | 0.462 |
| 1 | 2 | 0.045 | 18 | 204 | 0.208 | 29 | 2 | 0.449 |
| 4 | 1 | 0.638 | 21 | 1 | 0.840 | 29 | 11 | 0.074 |
| 4 | 1 | 0.647 | 21 | 1 | 0.817 | 29 | 11 | 0.076 |
| 4 | 13 | 0.167 | 21 | 10 | 0.055 | 29 | 24 | 3.066 |
| 4 | 13 | 0.185 | 21 | 10 | 0.058 | 29 | 24 | 3.078 |
| 4 | 18 | 3.199 | 21 | 13 | 0.090 | 31 | 1 | 0.486 |
| 4 | 18 | 3.283 | 21 | 13 | 0.085 | 31 | 1 | 0.483 |
| 9 | 9 | 0.252 | 21 | 24 | 3.285 | 31 | 5 | 0.104 |
| 9 | 9 | 0.266 | 21 | 24 | 3.219 | 31 | 5 | 0.097 |
| 10 | 1 | 0.680 | 23 | 1 | 0.719 | 31 | 14 | 0.068 |
| 10 | 1 | 0.693 | 23 | 1 | 0.753 | 31 | 14 | 0.061 |
| 10 | 24 | 2.856 | 23 | 12 | 0.046 | 31 | 18 | 0.144 |
| 10 | 24 | 2.916 | 23 | 12 | 0.050 | 31 | 18 | 0.141 |
| 12 | 11 | 0.150 | 23 | 12 | 0.054 | 31 | 24 | 3.068 |
| 12 | 11 | 0.165 | 23 | 16 | 0.116 | 31 | 24 | 3.008 |
| 14 | 2 | 0.659 | 23 | 16 | 0.130 | 32 | 11 | 0.077 |
| 14 | 2 | 0.684 | 23 | 16 | 0.120 | 32 | 11 | 0.068 |
| 14 | 5 | 0.288 | 23 | 20 | 0.292 | 32 | 11 | 0.072 |
| 14 | 5 | 0.303 | 23 | 20 | 0.275 | 33 | 1 | 0.764 |
| 14 | 6 | 0.257 | 23 | 24 | 3.308 | 33 | 1 | 0.752 |
| 14 | 6 | 0.242 | 23 | 24 | 3.414 | 33 | 11 | 0.082 |
| 14 | 6 | 0.240 | 23 | 204 | 0.227 | 33 | 11 | 0.051 |
| 14 | 9 | 0.164 | 23 | 204 | 0.197 | 33 | 12 | 0.069 |
| 14 | 9 | 0.166 | 23 | 204 | 0.204 | 33 | 12 | 0.061 |
| 14 | 11 | 0.107 | 25 | 1 | 0.565 | 33 | 18 | 0.147 |
| 14 | 11 | 0.116 | 25 | 1 | 0.580 | 33 | 18 | 0.153 |
| 14 | 21 | 0.410 | 25 | 12 | 0.058 | 33 | 24 | 3.058 |
| 14 | 21 | 0.426 | 25 | 12 | 0.060 | 33 | 24 | 3.061 |
| 14 | 122 | 1.776 | 25 | 23 | 3.166 | 35 | 1 | 1.077 |
| 14 | 122 | 1.772 | 25 | 23 | 3.150 | 35 | 1 | 1.092 |
| 18 | 1 | 0.590 | 25 | 107 | 0.048 | 35 | 11 | 0.040 |
| 18 | 1 | 0.610 | 25 | 107 | 0.053 | 35 | 11 | 0.040 |
| 18 | 2 | 0.391 | 25 | 204 | 0.132 | 35 | 24 | 3.030 |
| 18 | 2 | 0.432 | 25 | 204 | 0.123 | 35 | 24 | 2.954 |
| 18 | 6 | 0.111 | 26 | 11 | 0.043 | 35 | 107 | 0.071 |
| 18 | 6 | 0.110 | 26 | 11 | 0.041 | 35 | 107 | 0.091 |
| 18 | 8 | 0.072 | 26 | 11 | 0.040 | 37 | 1 | 0.696 |
| 18 | 8 | 0.069 | 26 | 11 | 0.031 | 37 | 1 | 0.691 |
| 18 | 10 | 0.049 | 26 | 12 | 0.066 | 37 | 2 | 0.567 |
| 18 | 10 | 0.043 | 26 | 12 | 0.063 | 37 | 2 | 0.553 |
| 18 | 14 | 0.057 | 26 | 12 | 0.060 | 37 | 11 | 0.043 |
| 18 | 14 | 0.061 | 26 | 12 | 0.066 | 37 | 11 | 0.043 |
| 18 | 16 | 0.118 | 26 | 13 | 0.065 | 37 | 16 | 0.100 |
| 18 | 16 | 0.110 | 26 | 13 | 0.058 | 37 | 16 | 0.107 |
| 18 | 18 | 0.156 | 26 | 13 | 0.062 | 37 | 24 | 3.055 |
| 18 | 18 | 0.158 | 26 | 15 | 0.105 | 37 | 24 | 3.017 |
| 18 | 20 | 0.371 | 26 | 15 | 0.093 | 38 | 1 | 0.658 |
| 18 | 20 | 0.379 | 26 | 15 | 0.095 | 38 | 1 | 0.667 |
| 18 | 24 | 3.035 | 26 | 15 | 0.124 | 39 | 1 | 0.820 |
| 18 | 24 | 3.170 | 26 | 15 | 0.105 | 39 | 1 | 0.799 |
| 18 | 122 | 2.350 | 29 | 1 | 1.007 | 39 | 6 | 0.104 |
| 18 | 122 | 2.291 | 29 | 1 | 1.027 | 39 | 6 | 0.113 |
| - | | | - | | | | | - |

| Stn | Niskin | CFC-12 | Stn | Niskir | n CFC-12 | Stn | Niski | in CFC-12 |
|----------|--------|----------|-----|----------|----------|-----|-------|-----------|
| | (r | omol/kg) | | (| pmol/kg) | | | (pmol/kg) |
| 39 | 11 | 0.054 | 48 | 9 | 0.080 | 54 | 1 | 0.051 |
| 39 | 11 | 0.061 | 48 | 9 | 0.086 | 54 | 1 | 0.050 |
| 39 | 18 | 0.164 | 48 | 11 | 0.084 | 54 | 6 | 0.056 |
| 39 | 18 | 0.163 | 48 | 11 | 0.082 | 54 | 6 | 0.053 |
| 39 | 23 | 2.607 | 48 | 11 | 0.082 | 54 | 11 | 0.050 |
| 39 | 23 | 2.630 | 48 | 11 | 0.082 | 54 | 11 | 0.067 |
| 40 | 11 | 0.050 | 48 | 13 | 0.095 | 54 | 12 | 0.059 |
| 40 | 11 | 0.065 | 48 | 13 | 0.102 | 54 | 12 | 0.059 |
| 41 | 1 | 0.614 | 48 | 15 | 2.234 | 54 | 18 | 0.063 |
| 41 | 1 | 0.604 | 48 | 15 | 2.221 | 54 | 18 | 0.062 |
| 41 | 2 | 0.391 | 48 | 204 | 0.264 | 54 | 23 | 0.059 |
| 41 | 2 | 0.392 | 48 | 204 | 0.252 | 54 | 23 | 0.054 |
| 41 | 11 | 0.055 | 49 | 1 | 0.509 | 54 | 24 | 0.062 |
| 41 | 11 | 0.043 | 49 | 1 | 0.506 | 54 | 24 | 0.062 |
| 41 | 14 | 0.060 | 49 | 5 | 0.276 | 54 | 24 | 0.062 |
| 41 | 14 | 0.056 | 49 | 5 | 0.276 | 54 | 24 | 0.062 |
| 41 | 16 | 0.100 | 49 | 9 | 0.094 | 55 | 11 | 2.284 |
| 41 | 16 | 0.088 | 49 | 9 | 0.106 | 55 | 11 | 2.294 |
| 41 | 24 | 3.075 | 49 | 11 | 0.060 | 55 | 18 | 1.943 |
| 41 | 24 | 3.062 | 49 | 11 | 0.057 | 55 | 18 | 1.979 |
| 41 | 107 | 0.050 | 49 | 13 | 0.089 | 55 | 24 | 3.090 |
| 41 | 107 | 0.051 | 49 | 13 | 0.079 | 55 | 24 | 3.129 |
| 41 | 222 | 1.408 | 49 | 15 | 0.116 | 60 | 1 | 1.104 |
| 41 | 222 | 1.413 | 49 | 15 | 0.110 | 60 | 1 | 1.089 |
| 42 | 8 | 0.035 | 49 | 17 | 0.112 | 60 | 1 | 1.003 |
| 42 | 8 | 0.037 | 49 | 17 | 0.201 | 61 | 1 | 0.805 |
| 43 | 1 | 0.270 | 49 | 21 | 0.818 | 61 | 1 | 0.792 |
| 43 | 1 | 0.274 | 49 | 21 | 0.809 | 61 | 6 | 0.792 |
| 43 | 11 | 0.274 | 49 | 24 | | 61 | 6 | |
| | 11 | | | 24 24 | 2.191 | 61 | 11 | 0.490 |
| 43 | | 0.034 | 49 | | 2.206 | | 11 | 0.207 |
| 43 | 17 | 0.109 | 49 | 103 | 0.451 | 61 | | 0.208 |
| 43 | 17 | 0.104 | 49 | 103 | 0.465 | 61 | 24 | 3.113 |
| 43 | 107 | 0.068 | 49 | 107 | 0.161 | 61 | 24 | 3.112 |
| 43 | 107 | 0.067 | 49 | 107 | 0.180 | 62 | 1 | 0.832 |
| 45 | 2 | 0.283 | 50 | 1 | 0.698 | 62 | 1 | 0.832 |
| 45 | 2 | 0.290 | 50 | 1 | 0.728 | 63 | 2 | 1.000 |
| 45 | 5 | 0.150 | 50 | 6 | 0.198 | 63 | 2 | 1.021 |
| 45 45 | 5 | 0.132 | 50 | 6 | 0.190 | 63 | 12 | 0.164 |
| 45 45 | 8 | 0.078 | 50 | 11 | 0.042 | 63 | 12 | 0.173 |
| 45 | 8 | 0.069 | 50 | 11 | 0.039 | 63 | 222 | |
| 45 | 14 | 0.116 | 50 | 16 | 0.100 | 63 | 222 | |
| 45 | 14 | 0.113 | 50 | 16 | 0.109 | 65 | 1 | 1.044 |
| 45 | 20 | 0.253 | 50 | 24 | 2.689 | 65 | 1 | 1.041 |
| 45 | 20 | 0.242 | 50 | 24 | 2.652 | 65 | 24 | 3.014 |
| 45 | 222 | 1.728 | 51 | 1 | 0.660 | 65 | 24 | 3.030 |
| 45 | 222 | 1.694 | 51 | 1 | 0.658 | 67 | 1 | 0.869 |
| 47 | 1 | 0.089 | 51 | 5 | 0.205 | 67 | 1 | 0.871 |
| 47 | 1 | 0.081 | 51 | 5 | 0.207 | 67 | 17 | 0.119 |
| 47 | 20 | 2.099 | 51 | 17 | 0.180 | 67 | 17 | 0.113 |
| 47 | 20 | 2.109 | 51 | 17 | 0.180 | 67 | 107 | |
| 48 | 1 | 0.443 | 51 | 24 | 2.552 | 67 | 107 | |
| 48 | 1 | 0.434 | 51 | 24 | 2.563 | 68 | 9 | 0.036 |
| 48 | 6 | 0.160 | 51 | 103 | 0.465 | 68 | 9 | 0.037 |
| 48 | 6 | 0.174 | 51 | 103 | 0.456 | | | |

| Stn | Niskin | CFC-12 | Stn | Niskin | CFC-12 | Stn | Niskin | CFC-12 |
|----------|---------------------|----------------|----------|----------|----------|----------|--------|----------|
| | (p | mol/kg) | | (p | omol/kg) | | (r | omol/kg) |
| 68 | 11 | 0.032 | 76 | 19 | 0.542 | 91 | 105 | 0.011 |
| 68 | 11 | 0.043 | 76 | 19 | 0.556 | 91 | 105 | 0.013 |
| 69 | 1 | 0.711 | 76 | 24 | 2.701 | 92 | 204 | 0.025 |
| 69 | 1 | 0.693 | 76 | 24 | 2.702 | 92 | 204 | 0.019 |
| 69 | 6 | 0.077 | 77 | 1 | 0.084 | 93 | 2 | 0.015 |
| 69 | 6 | 0.077 | 77 | 1 | 0.082 | 93 | 2 | 0.024 |
| 69 | 11 | 0.034 | 77 | 6 | 0.049 | 93 | 6 | 0.013 |
| 69 | 11 | 0.035 | 77 | 6 | 0.046 | 93 | 6 | 0.015 |
| 69 | 17 | 0.145 | 77 | 18 | 0.734 | 93 | 16 | 1.066 |
| 69 | 17 | 0.145 | 77 | 18 | 0.737 | 93 | 16 | 1.077 |
| 69 | 20 | 0.537 | 77 | 24 | 2.680 | 93 | 20 | 1.884 |
| 69 | 20 | 0.561 | 77 | 24 | 2.675 | 93 | 20 | 1.838 |
| 69 | 23 | 3.136 | 79 | 1 | 0.047 | 94 | 6 | 0.024 |
| 69 | 23 | 3.109 | 79 | 1 | 0.043 | 94 | 6 | 0.017 |
| 69 | 103 | 0.292 | 79 | 10 | 0.040 | 95 | 1 | 0.014 |
| 69 | 103 | 0.276 | 79 | 10 | 0.037 | 95 | 1 | 0.014 |
| 71 | 1 | 0.587 | 81 | 13 | 0.228 | 95 | 1 | 0.013 |
| 71 | 1 | 0.600 | 81 | 13 | 0.228 | 95 | 9 | 0.067 |
| 71 | 5 | 0.095 | 81 | 19 | 2.149 | 95 | 9 | 0.074 |
| 71 | 5 | 0.093 | 81 | 19 | 2.136 | 95 | 16 | 1.625 |
| 71 | 11 | 0.027 | 83 | 2 | 0.025 | 95 | 16 | 1.619 |
| 71 | 11 | 0.034 | 83 | 2 | 0.025 | 95 | 19 | 1.831 |
| 71 | 20 | 0.589 | 83 | 5 | 0.024 | 95 | 19 | 1.823 |
| 71 | 20 | 0.580 | 83 | 5 | 0.024 | 95 95 | 23 | 1.839 |
| 71 | 24 | 2.921 | 83 | 11 | 0.023 | 95 95 | 23 | 1.039 |
| 71 | 24 24 | 2.923 | 83 | 11 | 0.041 | 95 95 | 103 | 0.014 |
| 73 | 2 4 1 | 2.923 0.142 | 83 | 222 | | 95 95 | 103 | 0.014 |
| | 1 | 0.142 | | | 2.767 | 95 95 | | |
| 73 72 | 8 | 0.142 | 83 | 222 | 2.754 | | 105 | 0.018 |
| 73 | | | 85 95 | 2 | 0.018 | 95 | 105 | 0.017 |
| 73 | 8 | 0.040 | 85 95 | 2 | 0.005 | 96 | 105 | 0.013 |
| 73 | 10 | 0.040 | 85 | 15 15 | 0.496 | 96 | 105 | 0.009 |
| 73 | 10 | 0.039 | 85 | 15 | 0.477 | 96 | 204 | 0.007 |
| 73 | 11 | 0.048 | 85 | 20 | 2.238 | 96 | 204 | 0.007 |
| 73 | 11 | 0.048 | 85 | 20 | 2.237 | 97 | 1 | 0.006 |
| 73 | 17 | 0.329 | 86 | 8 | 0.036 | 97 | 1 | 0.010 |
| 73 | 17 | 0.335 | 86 | 8 | 0.033 | 97 | 18 | 1.936 |
| 73 | 23 | 2.734 | 86 | 11 | 0.107 | 97 | 18 | 1.888 |
| 73 | 23 | 2.662 | 86 | 11 | 0.103 | 97 | 204 | 0.007 |
| 73 | 103 | 0.076 | 86 | 17 | 1.070 | 97 | 204 | 0.013 |
| 73 74 | 103 | 0.070 | 86 | 17 | 1.032 | 98 | 1 | 0.009 |
| 74 74 | 1 | 0.132 | 86 | 23 | 2.230 | 98 | 1 | 0.011 |
| 74 74 | 1 | 0.140 | 86 | 23 | 2.215 | 98 | 105 | 0.013 |
| 74 | 12 | 0.068 | 89 | 6 | 0.012 | 98 | 105 | 0.008 |
| 74 75 | 12 | 0.066 | 89 | 6 | 0.003 | 99 | 10 | 0.326 |
| 75 75 | 1 | 0.129 | 89 | 24 | 2.240 | 99 | 10 | 0.304 |
| 75 75 | 1 | 0.135 | 89 | 24 | 2.232 | 99 | 15 | 1.821 |
| 75 75 | 5 | 0.058 | 89 | 105 | 0.006 | 99 | 15 | 1.855 |
| 75 75 | 5 | 0.061 | 89 | 105 | 0.008 | 99 | 20 | 2.027 |
| 75 75 | 16 | 0.264 | 89 | 204 | 0.006 | 99 | 20 | 1.998 |
| 75 75 | 16 | 0.267 | 89 | 204 | 0.003 | 99 | 105 | 0.025 |
| 75 75 | 23 | 2.687 | 91 | 10 | 0.050 | 99 | 105 | 0.024 |
| 75 70 | 23 | 2.698 | 91 | 10 | 0.047 | 101 | 10 | 0.306 |
| 76 70 | 1 | 0.076 | 91 | 15 45 | 0.435 | 101 | 10 | 0.307 |
| 76 | 1 | 0.077 | 91 | 15 | 0.421 | | | |

| Stn | Niskin | CFC-12 | Stn | Niskin | CFC-12 | | |
|-----|--------|---------|-----|-----------|--------|--|--|
| | (pi | mol/kg) | | (pmol/kg) | | | |
| 101 | 15 | 1.787 | 103 | 16 | 0.478 | | |
| 101 | 15 | 1.761 | 103 | 16 | 0.483 | | |
| 101 | 20 | 1.857 | 103 | 21 | 1.542 | | |
| 101 | 20 | 1.887 | 103 | 21 | 1.569 | | |
| 101 | 105 | 0.058 | 105 | 23 | 1.599 | | |
| 101 | 105 | 0.061 | 105 | 23 | 1.615 | | |
| 103 | 1 | 0.011 | | | | | |
| 103 | 1 | 0.008 | | | | | |

Table 3: AU9404 CFC Air Measurements

| Time | | | F11 | F12 | |
|------------------------|--------------|------------------------|--------------------------|----------------|---------------|
| Date | (hhmm) | Latitude | Longitude | PPT I | PPT |
| 19 Dec 94 | 2338 | 57 26.6 S | 127 53.5 E | 257.0 | 515.0 |
| 19 Dec 94 | 2350 | 57 26.6 S | 127 53.5 E | 257.3 | 507.3 |
| 20 Dec 94 | 0015 | 57 26.6 S | 127 53.5 E | 257.0 | 509.7 |
| 20 Dec 94 | 0033 | 57 26.6 S | 127 53.5 E | 257.3 | 511.4 |
| 22 Dec 94 | 0704 | 62 00.3 S | 118 00.4 E | 257.7 | 510.3 |
| 22 Dec 94 | 0716 | 62 00.3 S | 118 00.4 E | 258.0 | 508.3 |
| 22 Dec 94 | 0729 | 62 00.3 S | 118 00.4 E | 257.5 | 511.3 |
| 22 Dec 94 | 0741 | 62 00.3 S | 118 00.4 E | 258.1 | 508.5 |
| 5 Jan 95 | 0335 | 63 16.0 S | 113 13.0 E | 258.4 | 509.5 |
| 5 Jan 95 | 0347 | 63 16.0 S | 113 13.0 E | 259.8 | 507.2 |
| 5 Jan 95 | 0359 | 63 16.0 S | 113 13.0 E | 257.4 | 508.8 |
| 5 Jan 95 | 0412 | 63 16.0 S | 113 13.0 E | 257.7 | 509.2 |
| 12 Jan 95 | 0146 | 62 52.7 S | 144 51.1 E | 258.8 | 511.1 |
| 12 Jan 95 | 0157 | 62 52.7 S | 144 51.1 E | 257.2 | 512.4 |
| 12 Jan 95 | 0213 | 62 52.7 S | 144 51.1 E | 257.9 | 510.7 |
| 12 Jan 95 | 0227 | 62 52.7 S | 144 51.1 E | 256.4 | 511.8 |
| 14 Jan 95 | 0751 | 63 26.0 S | 156 39.0 E | 259.8 | 511.5 |
| 14 Jan 95 | 0803 | 63 26.0 S | 156 39.0 E | 259.2 | 510.3 |
| 20 Jan 95 | 0938 | 65 04.9 S | 139 51.5 E | 261.5 | 508.7 |
| 20 Jan 95 | 0952 | 65 04.9 S | 139 51.5 E | 260.1 | 507.6 |
| 20 Jan 95 | 1008 | 65 04.9 S | 139 51.5 E | 260.1 | 506.7 |
| 20 Jan 95 | 1021 | 65 04.9 S | 139 51.5 E | 260.8 | -9.0 -07.0 |
| 20 Jan 95 | 1035 | 65 04.9 S | 139 51.5 E | 260.5 | 507.2 |
| 22 Jan 95 | 1424 | 60 36.0 S | 139 51.0 E | 259.0 | 507.1 |
| 22 Jan 95 22 Jan 95 | 1435 | 60 36.0 S 60 36.0 S | 139 51.0 E 139 51.0 E | 258.8 | 510.4 |
| 27 Jan 95 | 1449 1107 | 51 35.9 S | 143 03.1 E | 259.3 255.6 | 508.4 -9.0 |
| 27 Jan 95 27 Jan 95 | 1117 | 51 35.9 S | 143 03.1 E | 257.8 | -9.0 501.9 |
| 27 Jan 95 27 Jan 95 | 1130 | 51 35.9 S | 143 03.1 E | 256.2 | 499.6 |
| 27 Jan 95 | 1145 | 51 35.9 S | 143 03.1 E | 258.0 | 497.5 |
| 27 Jan 95 | 1157 | 51 35.9 S | 143 03.1 E | 259.0 | 497.4 |
| 1 Feb 95 | 0353 | 44 07.0 S | 146 13.0 E | 256.9 | 502.0 |
| 1 Feb 95 | 0404 | 44 07.0 S | 146 13.0 E | 257.4 | 500.5 |
| 1 Feb 95 | 0416 | 44 07.0 S | 146 13.0 E | 257.3 | 498.8 |
| 1 Feb 95 | 0417 | 44 07.0 S | 146 13.0 E | 256.2 | 496.9 |
| | | | | | |

```
Stn
                              F11
                                   F12
No.
    Latitude Longitude
                           Date
                                    PPT
                                           PPT
     57 32.1 S 127 49.5 E
                                      257.5 510.2
                           20 Dec 94
 1
 2
     61 59.1 S 120 01.7 E
                           21 Dec 94
                                      257.6
                                            510.2
 3
     62 00.7 S 119 02.1 E
                           21 Dec 94 257.6 510.2
                           22 Dec 94 257.6 510.2
     62 00.3 S 118 01.6 E
     65 59.3 S 109 55.0 E
 6
                           2 Jan 95
                                     258.3 506.6
 7
     65 23.1 S
              112 33.2 E
                           3 Jan 95
                                     258.3
                                            506.6
 8
     65 18.5 S 112 32.2 E
                           3 Jan 95
                                     258.3
                                            506.6
 9
    64 57.7 S 112 09.6 E
                           4 Jan 95
                                     258.3
                                            506.6
              111 55.1 E
                                     258.3
 10
    64 44.9 S
                            4 Jan 95
                                            506.6
     64 30.9 S 111 25.8 E
                                     258.3 506.6
                            4 Jan 95
 11
                                     258.3 506.6
    64 06.1 S 112 05.9 E
                            4 Jan 95
    63 40.8 S 112 36.5 E
                                     258.3
 13
                            4 Jan 95
                                            506.6
 14
    63 16.5 S
               113 13.0 E
                            5 Jan 95
                                     258.3
                                            506.6
 15 62 50.8 S
              113 49.1 E
                                     258.3
                                           506.6
                            5 Jan 95
    62 25.3 S 114 25.7 E
                                     258.3
 16
                            5 Jan 95
                                            506.6
    62 00.0 S
                                     258.0
 17
               115 01.0 E
                            6 Jan 95
                                            510.1
 18
    61 59.7 S
               116 30.5 E
                            6 Jan 95
                                     258.0 510.1
    62 00.3 S
              120 01.4 E
 19
                            6 Jan 95
                                     258.0
                                           510.1
 20 61 59.8 S 121 26.9 E
                            7 Jan 95
                                     258.0 510.1
 21
     62 00.2 S
               122 50.4 E
                            7 Jan 95
                                     258.0 510.1
 22
    62 00.1 S
              124 15.4 E
                            7 Jan 95
                                     258.0 510.1
 23 62 00.2 S
               125 39.6 E
                            7 Jan 95
                                     258.0
                                            510.1
 24
    62 00.4 S
               127 05.5 E
                            8 Jan 95
                                     258.4
                                            509.9
 25
    62 00.7 S
               128 31.6 E
                            8 Jan 95
                                     258.4
                                            509.9
 26 62 00.2 S
              129 56.7 E
                                     258.4 509.9
                            8 Jan 95
    62 00.6 S 131 20.0 E
                                     258.4
 27
                            9 Jan 95
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