# E. Microstructural Changes In NO<sub>x</sub> Trap Materials under Lean and Rich Conditions at High Temperatures

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### Objective

- Facilitate deployment of a nitrogen oxides (NO<sub>x</sub>) trap for lean diesel or gasoline exhaust by
  - investigating materials issues related to deterioration of the performance of NO<sub>x</sub> traps upon aging as a result of thermal and sulfation-desulfation cycles
  - investigating materials that are robust under the lean NO<sub>x</sub> trap operating conditions

#### Approach

- Synthesize new model catalyst systems containing platinum (Pt): Pt/BaO.6Al<sub>2</sub>O<sub>3</sub>, [10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)], and 2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)].
- Treat them under thermal, lean-diesel, and rich-diesel conditions at 500°C for 4 h and monitor changes in microstructure. The next step involves evaluation under lean-rich cycles and aging under laboratory aging cycles.
- Evaluate the performance of the selected systems on a bench-top flow reactor.

#### Accomplishments

- Completed the microstructural evaluation of model catalysts Pt/BaO.6Al<sub>2</sub>O<sub>3</sub>, [10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)] and 2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)]. The latter is a better representative of this class of NO<sub>x</sub> trap systems.
  - Completed and reproduced the study of microstructural changes on aging under diesel lean and rich conditions at 500°C.
  - Completed microstructural changes under thermal aging studies of these samples for comparison.
  - Completed microstructural changes in thermally aged samples after extended exposure to lean and rich conditions.
- Began updating the ex-situ reactor to enhance its capabilities to enable treatment of transmission electron microscopy (TEM) samples under lean, rich, or, stoichiometric conditions, as well as lean-rich cycles. This reactor will be capable of rapid screening of the model catalyst powders for their durability in exhaust under the operating conditions for diesel and gasoline engines.
- Equipped the synthesis laboratory to enable preparation of NO<sub>x</sub> trap materials. The bench-top-flow reactor is being set up.

#### **Future Direction**

- Evaluate model catalyst systems on a bench-top flow reactor for their efficiency and durability as NO<sub>x</sub> traps under simulated diesel and gasoline conditions [with or without sulfur oxides (SO<sub>x</sub>) in the simulated exhaust]. These results will provide a benchmark for evaluation of new materials.
- Carry out microstructural characterization of model NO<sub>x</sub> trap powders after aging under lean, rich, or stoichiometric conditions on the bench-top flow reactor and TEM samples on an ex-situ microreactor.
- Investigate new materials that can withstand NO<sub>x</sub> trap operating conditions without detrimental structural changes.

### **Introduction**

NO<sub>x</sub> traps are at the forefront of various strategies under investigation to treat NO<sub>x</sub> from diesel and lean-gasoline engines.<sup>1</sup> NO<sub>x</sub> traps collect engine-out NO<sub>x</sub> during lean operation and treat it during short rich-operation cycles.<sup>2</sup> Fresh  $NO_x$  traps work very well but cannot sustain their high efficiency over the lifetime of a vehicle. The efficiency loss is believed to be caused by aging due to high-temperature operation and sulfation-desulfation cycles necessitated by the  $SO_x$  in the emissions from the oxidation of sulfur in fuel. In order to design a thermally durable  $NO_x$  trap, there is a need to understand the changes in the microstructures of materials that occur during various modes of operation (lean, rich, and lean-rich cycles). This information can form the basis for selection and design of new NO<sub>x</sub> trap materials that can resist deterioration under normal operation.

NO<sub>x</sub> traps are derived from commercial threeway catalysts installed to treat emissions from engines operating at stoichiometric air-fuel ratios. Therefore, the basic components of NO<sub>x</sub> traps are identical to three-way catalysts. The advanced version of a three-way catalyst is a two-layer system on a honeycomb substrate with the inner layer based on Pt-alumina and the outer layer on rhodium-ceriazirconia. The NO<sub>x</sub> traps derived from advanced three-way catalysts are identical to the catalysts except for a high baria content (the upper limit being close to 20%) in the alumina layer. Thus aging can lead to intermixing of layers, crystallization of bariacontaining phases that are not good NO<sub>x</sub> absorbers, and sintering of precious metals. The first goal of this project is to determine if one or all of the microstructural changes take place and if these changes occur during lean, rich, or lean-rich cycles. The tasks to achieve this goal are as follows:

• Complete microstructural characterization of fresh and thermally aged NO<sub>x</sub> trap materials to

determine the species formed as a result of aging.

- Complete microstructural characterization of fresh NO<sub>x</sub> trap materials after exposure to lean conditions to determine the species formed during lean cycles.
- Complete microstructural characterization of fresh NO<sub>x</sub> trap materials after exposure to rich conditions to determine the species formed during rich cycles.

The second goal of the project is to investigate and design new materials that can withstand  $NO_x$ trap operating conditions without undergoing detrimental structural changes. The results from the first goal will provide insights into changes that occur in  $NO_x$  trap materials at a microstructural level upon extended exposure to  $NO_x$  trap operating conditions, enabling selection and design of materials for the second goal.

## **Approach**

Our approach involves synthesizing new model catalyst systems; treating them under thermal, lean, and rich conditions; and monitoring microstructural changes to understand the deterioration mechanism. In order to rapidly screen model catalyst systems, we have designed an ex-situ reactor system that is being further upgraded to enhance its capabilities. The updated system will operate in the 25–1000°C range and will have the ability to introduce periodic rich pulses while the catalyst is being treated under lean or stoichiometric conditions.

The information from this study will be used to design thermally durable catalyst systems and will be tested on a bench-top flow reactor system.

## **Results**

Over the last 2 years, we determined the microstructural changes that occurred in a supplier lean  $NO_x$  trap system (based on Pt/BaO-Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>-ZrO<sub>2</sub> materials) upon being aged on (1) a pulsator at Ford Motor Company, (2) a dynamometer at Ford, and (3) vehicles with gasoline direct-injection, spark-ignition (DISI) engines in Europe.

- After pulsator aging, lean and rich aged samples showed that the sintering of Pt particles occurs during aging, and barium migrates into the ceria-zirconia layer. Both of these factors reduce the Pt-barium oxide surface area where NO<sub>x</sub> adsorption and reduction take place during lean and rich cycles, respectively. The stoichiometric aging also leads to the migration of barium into the ceria-zirconia layer, but the sintering of Pt is less severe.
- The dyno-aged samples showed extensive sintering of Pt and its migration into the ceriazirconia layer. The sintering of rhodium was also observed. The migration of barium into ceria-zirconia and the sintering of the precious metal component could explain the deterioration of performance
- The analysis of the samples evaluated on-vehicle after 32,000 km and 80 km showed that the bulk of the sintering of precious metals occurred in the stages of on-vehicle aging.

These results primarily show precious metal sintering and barium migration to be the cause of performance deterioration in NO<sub>x</sub> trap materials in gasoline engine exhaust conditions. While the laboratory aging protocols for diesel engines are in development, we have compiled data showing earlystage changes in model NO<sub>x</sub> trap materials under diesel conditions. We assumed that lowertemperature simulated diesel exhaust would slow down the aging compared with gasoline engine exhaust. Thus we completed a series of thermal aging, diesel lean aging, and diesel rich aging cycles of a model NO<sub>x</sub> trap and a model NO<sub>x</sub> trap modified with manganese oxide, as well as Pt/Al2O3, for comparison purposes. The results are summarized in the following paragraphs.

## Synthesis of New Model Catalysts

 $Pt/Al_2O_3$ : The Pt/alumina was prepared by the impregnation method using  $H_2PtCl_6$  salt. X-ray powder diffraction (XRD) shows broad diffraction peaks for alumina and no peaks due to Pt, as expected because of the small particle size of Pt in the freshly prepared sample (Figure 1).



Figure 1. X-ray diffraction patterns of Pt/Al<sub>2</sub>O<sub>3</sub>.

2%Pt, 5%MnO2, 93%[10%CeO2-ZrO2, 90%(2%La2O3, 98% BaO.6Al2O3)]: The model catalyst was synthesized by impregnating 2%Pt, 97%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)] with manganese nitrate and subsequent decomposition.

## Microstructural Changes in Model Catalysts

The microstructural changes in model catalysts (Pt/Al<sub>2</sub>O<sub>3</sub>), (2%Pt, 98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)]), and (2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)]) after thermal treatment at 500, 600, 700, 800, and 900°C; lean treatment at 500°C for 4 h; and rich treatment at 500°C were followed with XRD and transmission electron microscopy (TEM). Here lean and rich treatment refers to exposure of sample in an ex-situ reactor (Figure 7a, described previously) to diesel lean and diesel rich conditions. A summary of changes in the precious metal (Pt) is presented in Table 1.

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Sample	e Treatment conditions				
	Fresh	Thermal treatment (XRD of powders)	Thermal treatment at 500°C on ex-situ reactor	Treatment under lean conditions on ex-situ reactor	Treatment under rich conditions on ex-situ reactor
Pt/Al <sub>2</sub> O <sub>3</sub>	1–1.2 nm	600°C, 3.4 nm 700°C, 17.1nm 800°C, 26.1nm 900°C, 39.5nm	2–4 nm	8–10nm	2–4 nm
Model NO <sub>x</sub> trap catalyst I: 2%Pt-98%[10%CeO <sub>2</sub> - ZrO <sub>2</sub> -90%(2%La <sub>2</sub> O <sub>3</sub> - 98%BaO.6Al <sub>2</sub> O <sub>3</sub> )]	1–2nm	600°C, 2.6 nm 700°C, 21.3nm 800°C, 37.2nm 900°C, 48.4nm	1–2 nm	1–2nm	1.5–3.5 nm
Model NO <sub>x</sub> trap catalyst II: 2%Pt, 5%MnO <sub>2</sub> - 93%[10%CeO <sub>2</sub> -ZrO <sub>2</sub> - 90%(2%La <sub>2</sub> O <sub>3</sub> -98% BaO.6Al <sub>2</sub> O <sub>3</sub> )]	1–2 nm	700°C, 20.7nm 800°C, 27.0nm 900°C, 34.0nm	1–2 nm	2–3nm	1–2nm

**Table 1.** Summary of Pt particles size changes under various treatment conditions in model catalysts I, II, and III

## **Thermal Treatment**

- Thermal treatment of samples was carried out at 500, 600, 700, 800, and 900°C in a bench-top furnace in air.
- Pt/Al<sub>2</sub>O<sub>3</sub>: In XRD patterns (Figure 1) of • Pt/Al<sub>2</sub>O<sub>3</sub>, diffraction peaks due to Pt particle size start to grow in 500-900°C range. The calculated Pt particle sizes (using the Scherrer formula, assumes spherical particles) are 3.4, 17.1, 26.1, and 39.5 nm at 600, 700, 800, and 900°C, respectively. At 500°C, the alumina is a mixture of  $\gamma$ -alumina and hydrated  $\gamma$ -alumina. At 800°C, a broad peak assignable to the alpha phase can be seen. At 900°C, the diffraction peaks due to  $\alpha$ - and  $\gamma$  - alumina are observed. TEM of the fresh sample shows that the Pt particle size is in the 1–1.2 nm range (Figure 2). This particle size grows to 2-4 nm on thermal treatment in a furnace at 500°C for 4 h.
- 2%Pt, 98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)]: In XRD patterns (Figure 3), diffraction peaks due to Pt particle size start to grow in the 500–900°C range. The calculated Pt particle sizes (using the Scherrer formula, assumes spherical particles) are 2.6, 21.3, 37.2, and 48.4 nm at 600, 700, 800, and 900°C, respectively. TEM of the fresh sample shows that the Pt particle size is ~1 nm (Figure 4). This



**Figure 2.** TEM of fresh and thermally aged (500°C, 4 h)  $Pt/Al_2O_3$ .



**Figure 3.** XRD patterns of 2%Pt-98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98%BaO.6Al<sub>2</sub>O<sub>3</sub>)].



**Figure 4.** TEM of fresh and thermally aged (500°C, 4 h) 2%Pt-98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98%BaO.6Al<sub>2</sub>O<sub>3</sub>)].

particle size grows to 1–2 nm upon thermal treatment in a furnace at 500°C for 4 h.

 2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)]: In XRD patterns (Figure 5), diffraction peaks due to Pt particle size start to grow in the 500–900°C range. The calculated Pt particle sizes (using the Scherrer formula, assumes spherical particles) are 20.7, 27, and 34 nm at 700, 800, and 900°C respectively. TEM of the fresh sample shows that the Pt particle size is ~1 nm (Figure 6). This particle size grows to 1–2 nm upon thermal treatment in a furnace at 500°C for 4 h.



**Figure 5.** XRD patterns of 2%Pt, 5%MnO<sub>2</sub>–93% [10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98% BaO.6Al<sub>2</sub>O<sub>3</sub>)].

### Lean and Rich Treatment in Ex-situ Reactor

The aging of model catalysts was carried out in our ex-situ reactor system (schematics in Figure 7) under lean or rich diesel exhaust conditions at 500°C for 4 h [CO, CO<sub>2</sub>, H<sub>2</sub>, HC, NO<sub>x</sub>, H<sub>2</sub>O, flow rate 100cc/min] showed some sintering of Pt particles,



**Figure 6.** TEM of fresh and thermally aged (500°C, 4 h) 2%Pt, 5%MnO<sub>2</sub>–93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98% BaO.6Al<sub>2</sub>O<sub>3</sub>)].



**Figure 7.** a. Schematics of current ex-situ reactor; b. Schematics of modified ex-situ reactor.

and the size grew to  $\sim 2.5$  nm. However, the sintering was significantly less than that observed upon thermal aging ( $\sim 30$ –40 nm) at 500°C in air.

It is important to note that the experiments in the ex-situ reactor system do not precisely duplicate the aging of  $NO_x$  traps during normal operation. The alternating lean/rich conditions are not present in our experiments; instead, our samples are exposed to lean conditions, and a lack of control of space velocity due to the very small amount of catalyst leads to  $NO_x$  absorber saturation conditions. The saturation condition persists throughout our treatment.

#### Lean Treatment

• Pt/Al<sub>2</sub>O<sub>3</sub>: TEM of the fresh sample shows that the Pt particle size is in the 1–1.2 nm range (Figure 8). This particle size grows to 8–10 nm in diesel lean simulated exhaust in the ex-situ reactor at 500°C for 4 h.

- 2%Pt, 98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)]: TEM of the fresh sample shows that the Pt particle size is ~1 nm (Figure 9). This particle size grows to 1–2 nm upon lean treatment in the ex-sit reactor at 500°C for 4 h.
- 2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)]: TEM of the fresh sample shows that the Pt particle size is ~1 nm (Figure 10). This particle size grows to 2–3 nm in diesel lean simulated exhaust in the ex-situ reactor at 500°C for 4 h.



Figure 8. TEM of fresh and lean aged (500°C, 4 h)  $Pt/Al_2O_3$ .



**Figure 9.** TEM of fresh and lean aged (500°C, 4 h) 2%Pt-98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98%BaO.6Al<sub>2</sub>O<sub>3</sub>)].



**Figure 10.** TEM of fresh and lean aged (500°C, 4 h) 2%Pt, 5%MnO<sub>2</sub>–93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98% BaO.6Al<sub>2</sub>O<sub>3</sub>)].

# **Rich Treatment**

• Pt/Al<sub>2</sub>O<sub>3</sub>: TEM of the fresh sample shows that the Pt particle size is in the 1–1.2 nm range (Figure 11). This particle size grows to 2–4 nm in diesel rich simulated exhaust in the ex-situ reactor at 500°C for 4 h.

- 2%Pt, 98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)]: TEM of the fresh sample shows that the Pt particle size is ~1–1.2 nm (Figure 12). This particle size grows to 1.5–3.5 nm in diesel rich simulated exhaust in the ex-situ reactor at 500°C for 4 h.
- 2%Pt, 5%MnO<sub>2</sub>, 93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98% BaO.6Al<sub>2</sub>O<sub>3</sub>)]: TEM of the fresh sample shows that the Pt particle size is ~1 nm (Figure 13). This particle size grows to 1–2 nm in diesel rich simulated exhaust in the ex-situ reactor at 500°C for 4 h.



**Figure 11.** TEM off fresh and rich aged (500°C, 4 h) Pt/Al<sub>2</sub>O<sub>3</sub>.



**Figure 12.** TEM of fresh and rich aged (500°C, 4 h) 2%Pt-98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98%BaO.6Al<sub>2</sub>O<sub>3</sub>)].



**Figure 13.** TEM of fresh and lean aged (500°C, 4 h) 2%Pt, 5%MnO<sub>2</sub>–93%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98% BaO.6Al<sub>2</sub>O<sub>3</sub>)].

# Modifications in Ex-situ Reactor

The ex-situ reaction is under modification to include the ability to cycle through lean and rich conditions. This involves the addition of a gas-flow controller and installation of solenoid valves that can be controlled through a computer using the Labview software system. The installation of plumbing is complete, and the new ex-situ reactor should be in operation shortly. The schematics of the modified reactor are shown in Figure 7b.

## <u>Surface Studies of Fresh and Aged Model</u> <u>NO<sub>x</sub> Trap Catalyst</u>

The results of X-ray photoelectron spectroscopy analysis (XPS) of 2%Pt, 98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>, 90%(2%La<sub>2</sub>O<sub>3</sub>, 98%BaO.6Al<sub>2</sub>O<sub>3</sub>)] are presented in Table 2. Powder samples of the fresh, thermally aged (500°C in air for 4h), and lean simulated exhaust-exposed (after thermal aging) catalysts were pressed onto an indium foil and then analyzed. The high concentration of Pt and lathanum in fresh samples is due to the migration of these elements to the surface. Thermally aged samples probably achieve a redistribution of elements, leading to a reduced concentration of these elements on the surface. When a thermally aged sample is exposed to simulated lean NO<sub>x</sub> conditions for about 4 h at 500°C, the surface composition does not change significantly. The lack of a significant increase in nitrogen or carbon after extended exposure to lean diesel exhaust is puzzling. Further experiments are in progress to determine if it is just a surface phenomenon, or if the bulk material loses nitrate during our cooling protocol.

#### **Conclusions**

Our results from the study of microstructural changes in a supplier lean  $NO_x$  trap system (based on Pt/BaO-Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>-ZrO<sub>2</sub> materials) upon aging on (1) a pulsator at Ford, (2) a dynamometer

at Ford, and (3) vehicles in gasoline DISI engines in Europe show that precious metal sintering and barium migration occurs. This could be a cause of performance deterioration in  $NO_x$  trap materials.

We have successfully employed an ex-situ reactor to study aging in model  $NO_x$  trap catalysts. This system has allowed us to study changes in samples in a selected area under thermal, lean diesel, or rich diesel conditions. We have updated the ex-situ reactor to a lean–rich cycle  $NO_x$  trap system. This protocol will allow us to rapidly screen catalyst systems without having to do start-and-stop experiments to understand aging.

Our next goal is to complete the bench-flow reactor and start evaluating new model catalyst systems for their performance and relate them to microstructural changes.

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Element	Fresh		Thermally aged at 500°C in air for 4 hours		Aging under simulated lean diesel exhaust at 500°C for 4 hours	
	Atomic %	Wt %	Atomic %	Wt %	Atomic %	Wt %
0	57.8	33.5	59.3	34.9	61.7	37.7
Al	26.6	26.0	27.6	27.4	26	26.8
С	6.3	2.7	3.7	1.6	4.1	1.9
Ba	3.9	19.4	5.9	29.8	5.1	26.7
La	2.2	11.0	0.5	2.5	0.6	3.2
N	0.3	0.2	0.2	0.1	0	0
Pt	1	7.1	0.5	3.6	0.5	3.7

Table 2. XPS analysis of 2%Pt-98%[10%CeO<sub>2</sub>-ZrO<sub>2</sub>-90%(2%La<sub>2</sub>O<sub>3</sub>-98%BaO.6Al<sub>2</sub>O<sub>3</sub>)]

# **Presentations**

C. K. Narula, "Recent Advances in Lean NO<sub>x</sub> Treatment in Automotive Exhaust," invited seminar at Purdue University, West Lafayette, Indiana, April 22, 2004. C. K. Narula, "Applied Catalysis Program," a presentation of results to the Science and Technology Technical Review Panel, National Transportation Research Center, Oak Ridge, TN, 2004.