## X-band Structure Design For The NLC

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## **Design Considerations**

- Emittance preservation, tolerance specs wakefield suppression
  - Short-range wakefields  $\propto a^{-3.8}$ : set lower limit on aperture:  $a \cong 0.18\lambda$
  - Long-range wakefields: mode detuning and damping
- Minimizing surface field
- Reducing breakdown damage
- Minimizing RF pulse heating
- Cost effective
- ...

## **Continuing Improvements**

- Breakdown problems with 1.8m structure (RDDS, DDS)
  - Low achievable gradient
  - Severe damage, large frequency shift
- C.Adolphsen theory

$$- \cdot \frac{G^2 v_g^2}{(R/Q)^2} \frac{\sin(\phi)}{\phi \sin(\phi) + 2v_g \cos(\phi)}$$

- Low v<sub>g</sub> or low RF power/structure
- Structure design approach
  - Traveling:  $v_g/c \sim 3-5\%$
  - Standing wave:  $v_g=0$

# Low v<sub>g</sub> With Large Aperture

- Traveling wave
  - Magnetic coupling
  - High phase advance
- Standing wave

(rf heating?)
(bandwidth?)
(short length)

## Traveling Wave Approach

High Phase Advance – 150<sup>0</sup>/cell

- With Phi=150 deg, one can
  - reduce  $v_g$
  - maintain large aperture
  - maintain good rf efficiency
- Shorter length due to low  $v_g$
- Low input power per structure
- Low surface field

IIGNIC2 Standard			
HOUVUS Structure	T <sub>fill</sub> (ns)	110	
	τ	0.54	
	P <sub>RF</sub> (MW)	58.85	
	I (A)	0.9	
	G <sub>RF</sub> (MV/m)	65.0	
	G <sub>B</sub>	-13.8	
	GL	51.0	



#### Standing Wave Approach PI-mode *vs* PI/2 Bi-periodic



#### PI-mode



#### Bi-periodic Structure m=0 Mode

Bi-periodic Structure, a=4.7mm



A = 
$$4.7$$
mm  
F =  $11.424$  GHz  
Q =  $8463$   
R =  $70.2$  M $\Omega$ /m  
R/Q =  $8291$   
Es/Ea =  $3.314$ 

- Large mode separation, can be longer in length
- Major concern multi-pactoring in coupling cell
- Twice as many cells
- Efficient (with thin disk, but maybe high in Es/Ea)

#### PI-mode SW Structure

PI-mode SW Structure, a=4.75mm



A = 4.75 mmF = 11.424 GHzQ = 8820R =  $68.0 \text{ M}\Omega/\text{m}$ R/Q = 7710Es/Ea = 2.646

- Dense modes at PI
- Short structure length
- Low surface field with thick disk

## Standing Wave Design

- PI-mode
- Short length
- Low input power and stored energy in structure
- Structure always operate at loaded gradient (55MV/m vs 70MV/m unloaded)
  - Coupling design for nominal current.
  - Adjust rf power at beam injection for different current



## Cell Profile



	DLWG	Ellip iris	Round
	Thin T	Thick T	
A (mm)	4.75	4.75	4.75
T (mm)	2.6	3.6	3.6
R (MΩ/m)	67.7	64.2	71.7
R/Q	7742	7519	7478
Es/Ea	2.53	2.08	2.09

- PI mode
- Rounded cell
- Detuned
- Average  $a: 0.18\lambda$
- Es/Ea designed to be about 2

#### Dipole Mode Detuning



- Need similar detuning as TW  $\Delta F_1 = 8 \sim 10\%/4\sigma$
- Cannot detune within one structure
- Detune in 8 sections, 15 cells each (20cm)(not interleaved)
- 120 cells to detune full 8-10% spectrum

### Tapered Structure Parameters (round iris)

- Inverse taper in "t" for wider bandwidth at small "a"
- Adjust cell parameters to obtain flat field



#### RF Parameters Of 8X15 Sections

	<b>S</b> 1	S2	<b>S</b> 3	<b>S</b> 4	<b>S</b> 5	<b>S</b> 6	<b>S</b> 7	<b>S</b> 8
$R(M\Omega/m)$	52.1	55.0	57.6	60.0	62.6	65.5	69.0	74.0
P(MW) for	18.5	17.5	16.7	16.1	15.4	14.7	14.0	13.0
G=70MV/m								
G(MV/m) for	71.1	73.1	75.8	76.3	78.0	79.8	81.9	84.8
P=22MW								

#### 8X15 Detuned Dipole Dispersion



#### Dipole Mode Kick Factor



### 8x15 Stack Dipole Kick Factors





Linear

#### Detuned Standing Wave Structure (?) Field Symmetric



#### Detuned Standing Wave Structure Assembly



#### Flattening Field By Adjusting End-"b"

![](_page_19_Figure_1.jpeg)

#### Flattening Field By Adjusting End-plate

![](_page_20_Figure_1.jpeg)

![](_page_20_Figure_2.jpeg)

#### KEK SW20A375 Stack

Parameters	SW20A375
a (mm)	3.75000
b (mm) (with square corners)	10.55666
t (mm)	2.6000
a <sub>nose</sub> (mm)	2.2000
L (mm)	13.12117
R (MΩ/m)	81.92
Q	8621
Es/Ea	2.046
"b" with two r0.51mm fillets	10.56721
ZERO mode frequency	11.2247

## **Optimizing Field Profile**

- Half of 15-cell stack
- Boundary:M-E
- "b" of coupler cell 10-µm larger

![](_page_21_Figure_4.jpeg)

#### Simulation Of 15-cell Tapered Structure

#### 

![](_page_22_Figure_2.jpeg)

![](_page_22_Figure_3.jpeg)

N	F1 (Hz)	a (mm)	b (mm)	t (mm)
0	1.42E+10	4.85462	10.87390	2.65200
1	1.42E+10	5.14991	10.83400	2.81487
2	1.42E+10	5.13882	11.00350	2.80825
3	1.43E+10	5.12785	10.99830	2.80174
4	1.43E+10	5.11700	10.99330	2.79534
5	1.43E+10	5.10627	10.98830	2.78904
6	1.43E+10	5.09565	10.98340	2.78285
7	1.43E+10	5.08502	10.97850	2.77669
8	1.43E+10	5.07450	10.97370	2.77063
9	1.43E+10	5.06411	10.96890	2.76468
10	1.43E+10	5.05384	10.96420	2.75883
11	1.43E+10	5.04355	10.95950	2.75300
12	1.43E+10	5.03324	10.95490	2.74720
13	1.43E+10	5.02320	10.95030	2.74157
14	1.43E+10	5.01300	10.94570	2.73589
15	1.43E+10	4.85462	10.80320	2.65200
N	F1 (Hz)	a (mm)	b (mm)	t (mm)
0	1.42E+10	4.85462	10.87390	2.65200
1	1.42E+10	5.14991	10.83700	2.81487
2	1.42E+10	5.13882	11.00350	2.80825
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14	1.43E+10	5.01300	10.94570	2.73589

Test SW (#1 of 4) cell 1-15 R= 63 MΩ/m

Flat field can be obtained in tapered structure

#### **Plunger Measurement Simulation**

![](_page_23_Figure_1.jpeg)

## Pulse Heating (G=70MV/m)

![](_page_24_Figure_1.jpeg)

- Slots perturb current of accelerating mode. Current concentration at slots produce RF heating
- ∆T: RDDS1: 25<sup>0</sup>C 55<sup>0</sup>C; RDS : <14<sup>0</sup>C