

**U.S. DEPARTMENT OF ENERGY  
OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT**

**NUCLEAR WASTE TECHNICAL REVIEW BOARD  
PANEL ON STRUCTURAL GEOLOGY & GEOENGINEERING**

**SUBJECT:       GEOCHEMICAL  
                  CONSIDERATIONS IN SEALING**

**PRESENTER:     DR. THOMAS E. HINKEBEIN**

**PRESENTER'S TITLE  
AND ORGANIZATION:   SENIOR MEMBER OF TECHNICAL STAFF  
                                  SANDIA NATIONAL LABORATORIES  
                                  ALBUQUERQUE, NEW MEXICO**

**PRESENTER'S  
TELEPHONE NUMBER:   (505) 844-6985**

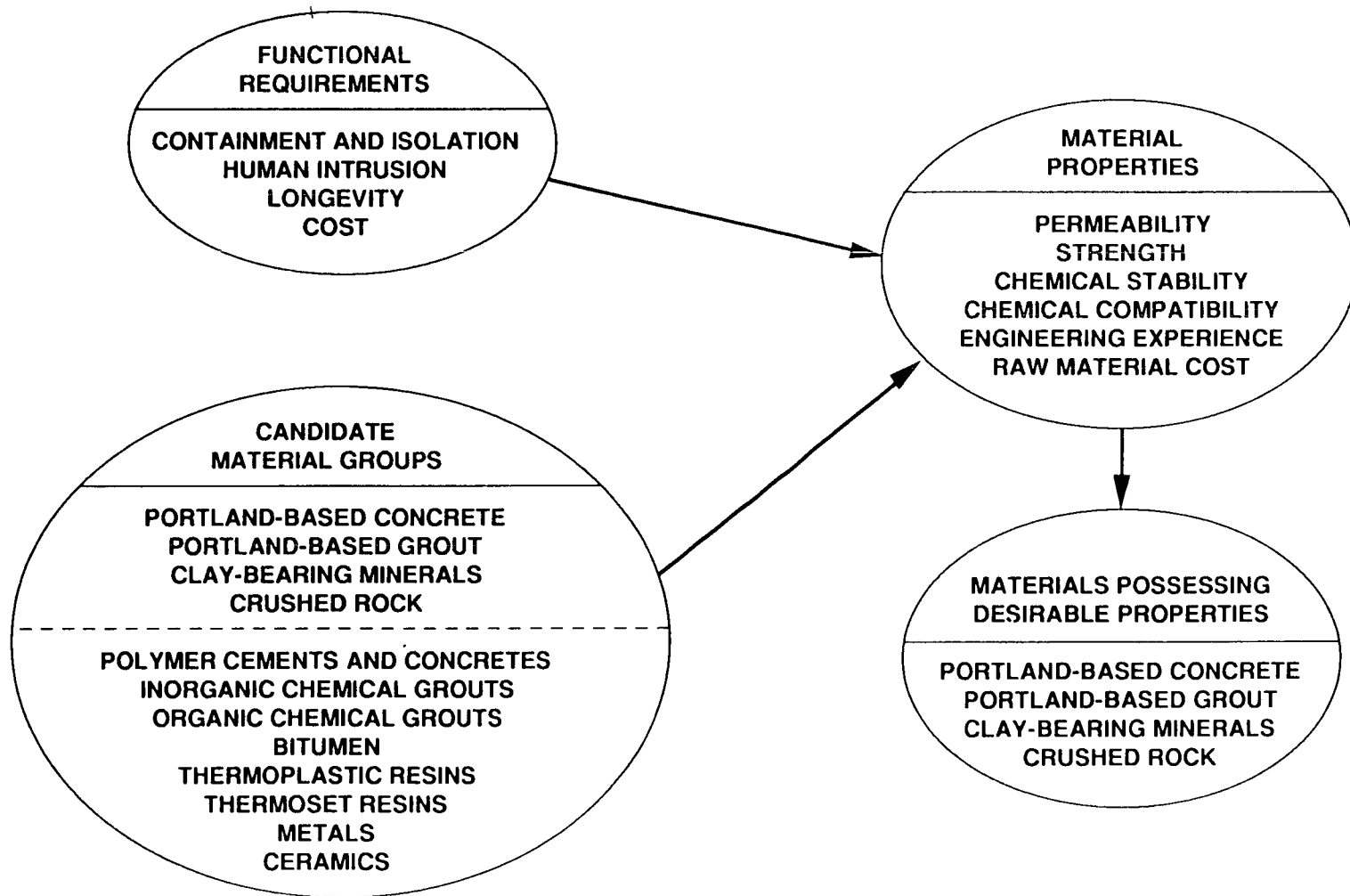
**NOVEMBER 12-13, 1991**

# **Overview of the Material Selection Methodology**

## **Process Consists of Repeated Material Evaluations**

- **Qualitative comparison to seal functional and design requirements**
  - **Quantitative comparison to specific design requirements**
    - **evaluation of material properties**
- 
- **Future evaluations as seal requirements are refined**
    - **evaluation of material properties**

# Initial Material Screen



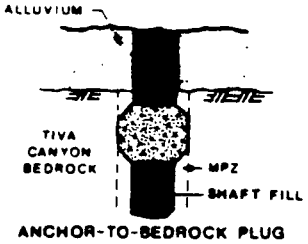
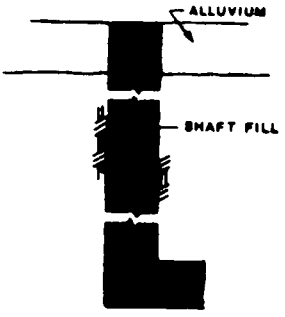
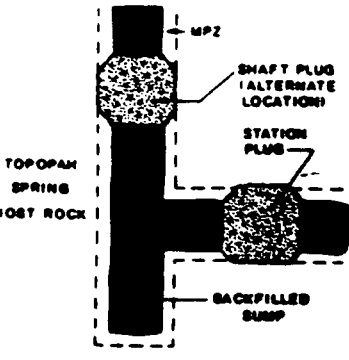
# **Second Material Evaluation**

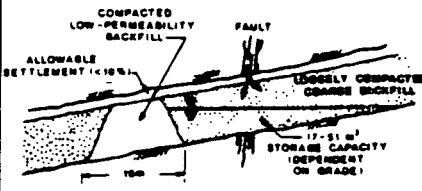
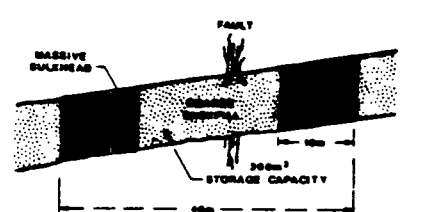
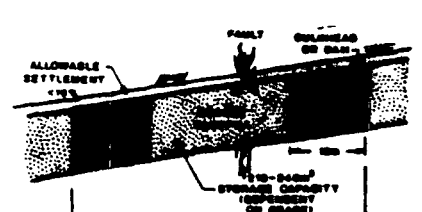
## **General Design Requirements Developed For**

- **Strength**
- **Emplacement considerations**
- **Seal-groundwater chemistry**
- **Environmental conditions**

## **Specific Design Requirements Developed For**

- **Hydraulic conductivity**

DESIGN OPTIONS	DESIGN REQUIREMENTS	CANDIDATE MATERIAL
 <p>ANCHOR-TO-BEDROCK PLUG</p>	<ul style="list-style-type: none"> <li>■ <math>K \leq 10^{-5}</math> TO <math>10^{-4}</math> cm/s</li> </ul>	<ul style="list-style-type: none"> <li>■ STANDARD CONCRETE</li> </ul>
 <p>GENERAL SHAFT BACKFILL</p>	<ul style="list-style-type: none"> <li>■ <math>K \leq 10^{-2}</math> cm/sec</li> </ul>	<ul style="list-style-type: none"> <li>■ CRUSHED TUFF</li> </ul>
 <p>STATION AND SHAFT PLUGS</p>	<ul style="list-style-type: none"> <li>■ <math>K \leq 10^{-6}</math> to <math>10^{-5}</math> cm/s</li> </ul>	<ul style="list-style-type: none"> <li>■ STANDARD CONCRETE OR COMPACTED EARTH</li> </ul>

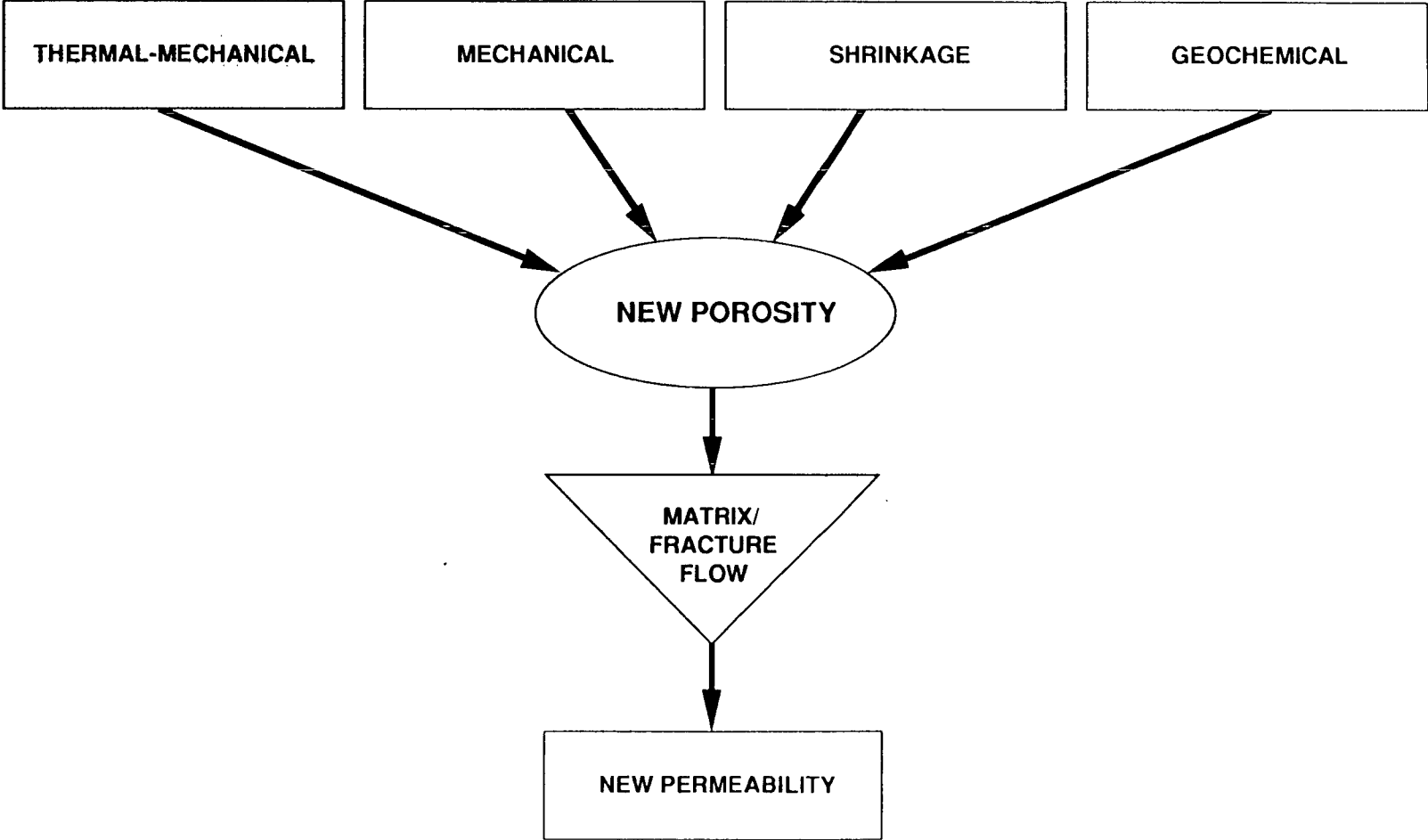
DESIGN OPTIONS	DESIGN REQUIREMENTS	CANDIDATE MATERIAL
 <p>(A) SINGLE DAM OR SINGLE BULKHEAD WITH SETTLEMENT</p>	<ul style="list-style-type: none"> <li>■ EMPLACEMENT DRIFT <math>K \leq 10^{-5}</math> TO <math>10^{-4}</math> cm/s</li> </ul>	<ul style="list-style-type: none"> <li>■ COMPACTED EARTH OF HIGH-TEMPERATURE CONCRETE</li> </ul>
 <p>(B) DOUBLE BULKHEAD (NO SETTLEMENT)</p>	<ul style="list-style-type: none"> <li>■ <math>K \leq 10^{-8}</math> TO <math>10^{-7}</math> cm/s</li> </ul>	<ul style="list-style-type: none"> <li>■ HIGH-TEMPERATURE CONCRETE OR COMPACTED EARTH</li> </ul>
 <p>(C) DOUBLE DAM OR DOUBLE BULKHEAD WITH SETTLEMENT</p>	<ul style="list-style-type: none"> <li>■ <math>K \leq 10^{-5}</math> TO <math>10^{-4}</math> cm/s</li> </ul>	<ul style="list-style-type: none"> <li>■ COMPACTED EARTH</li> </ul>

## Observed Properties of Candidate Seal Materials

PROPERTY	CEMENTITIOUS MATERIALS	EARTHEN MATERIALS
HYDRAULIC CONDUCTIVITY	TYPICAL: $10^{-8}$ - $10^{-6} \frac{\text{cm}}{\text{sec}}$ BEST: $10^{-10} \frac{\text{cm}}{\text{sec}}$	TYPICAL: $10^{-5}$ - $10^{+2} \frac{\text{cm}}{\text{sec}}$ BEST: $10^{-10} \frac{\text{cm}}{\text{sec}}$
STABILITY	CHEMICAL ALTERATION	DEHYDRATION
GROUNDWATER CHEMISTRY INTERACTIONS	INCREASED LEVELS OF $\text{OH}^-$ , $\text{Na}^+$ , $\text{K}^+$ , $\text{SO}_4^{=}$ , Si, and $\text{Ca}^{++}$  STABILIZING EFFECT OF TUFF	INCREASED LEVELS OF $\text{Na}^+$ , $\text{K}^+$ , $\text{Ca}^{++}$ , $\text{Mg}^{++}$ , Si, Al  CONCENTRATION INCREASES CONTROLLABLE
STRENGTH	HIGH CONTROLLABLE	CRACKING POTENTIAL SWELLING

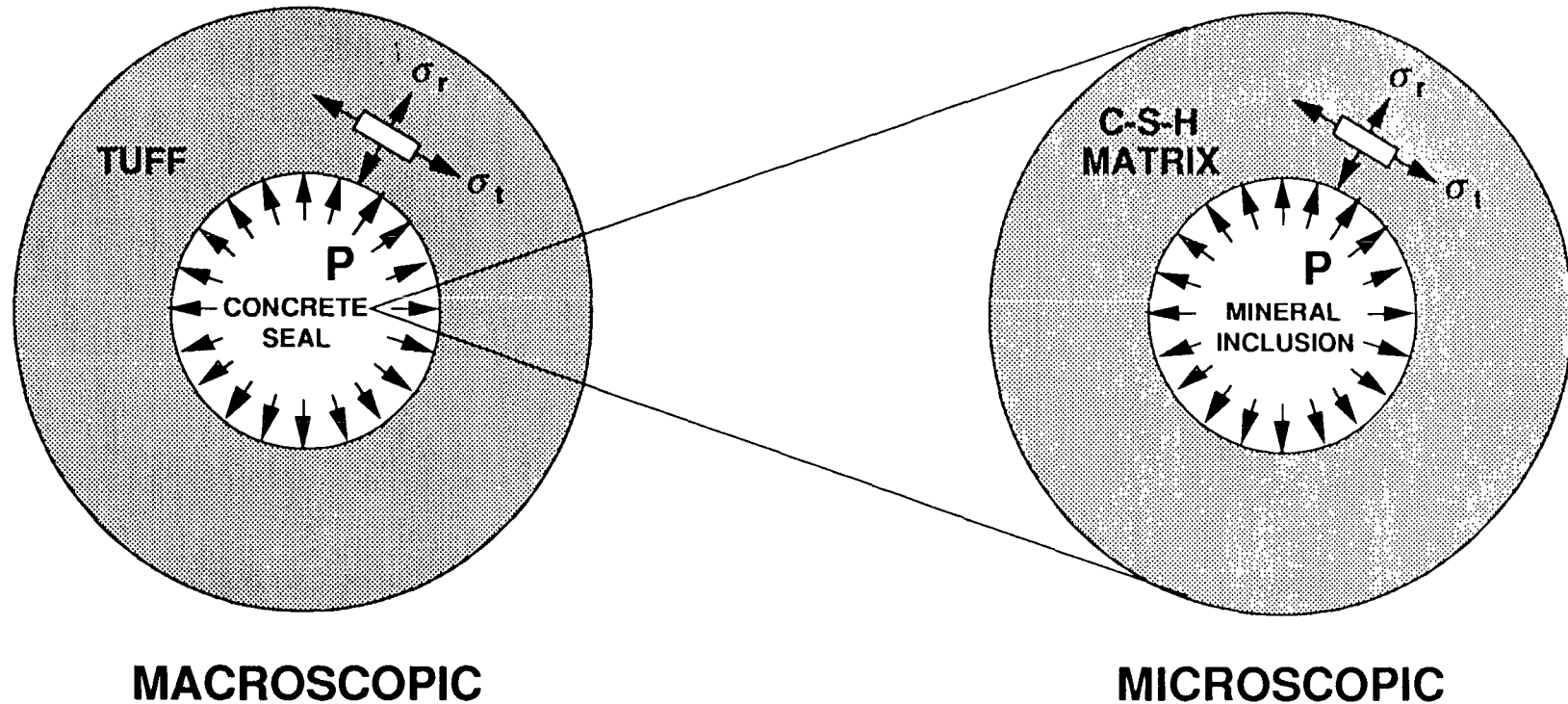
# Overview

## Cementitious Sealing Material Degradation Model





## Thermal-Mechanical Interactions



- Differential expansion causes pressure
- Microscopic and macroscopic analyses based upon spherical/cylindrical analysis of Timoshenko and Goodier

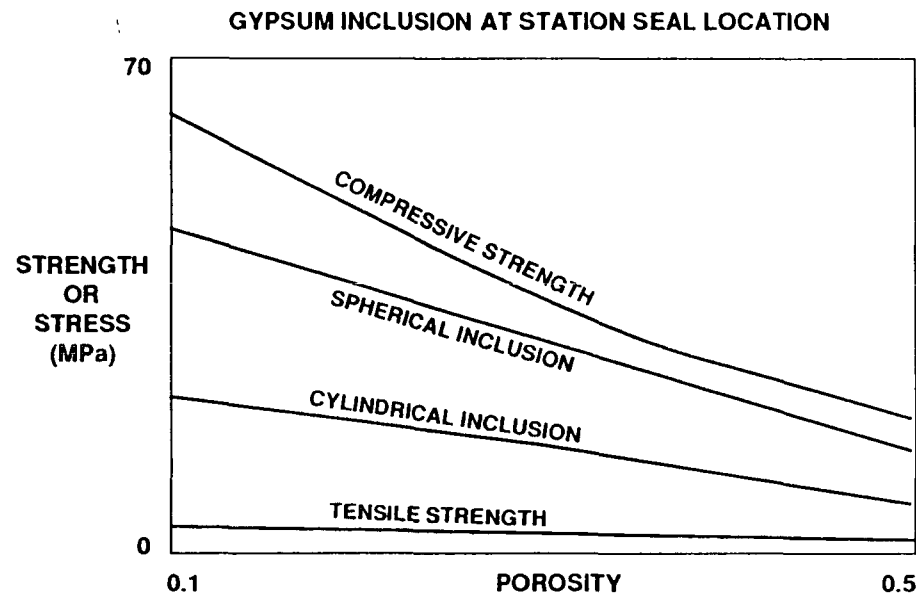
# **Thermal-Mechanical Interactions**

## **Microscopic Analyses**

- **Microscopic inclusions in C-S-H Matrix**
  - **Ettringite**
  - **Hydrogarnet**
  - **Portlandite**
  - **Silica**
  - **Gypsum**
  - **Unreacted cement phases**
  - **Fine aggregate**
  - **Coarse aggregate**
  
- **Tensile stresses compared to**
  - **Confining stress**
  - **Tensile strength**

# Thermal-Mechanical Interactions

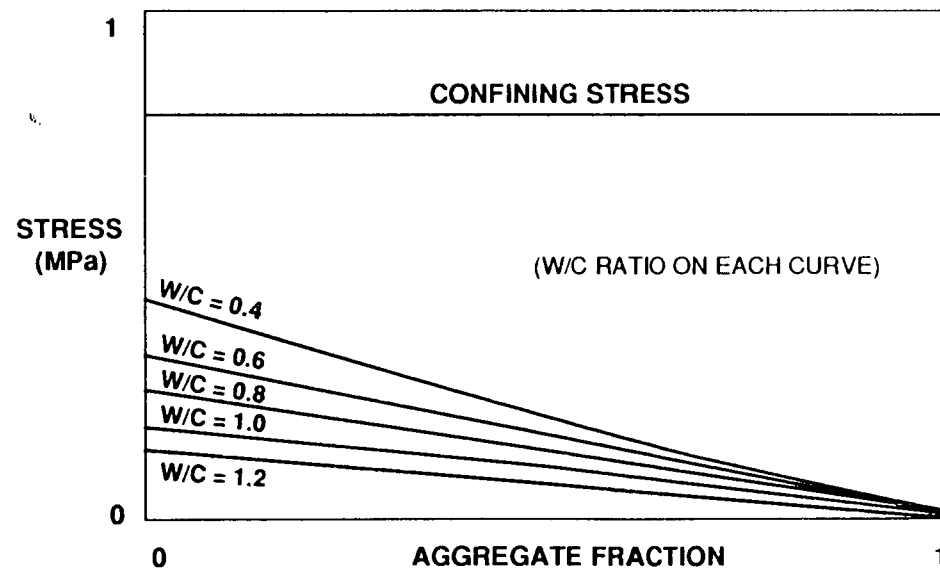
## Microscopic Analyses



- **Stress greater than tensile strength or confining stress**
  - Plug unstable to thermal expansive stresses
- **Similar results obtained for**
  - Portlandite
  - Unreacted cement phases
- **Amounts of gypsum, Portlandite, and unreacted cement phases must be controlled**

# Thermal-Mechanical Interactions

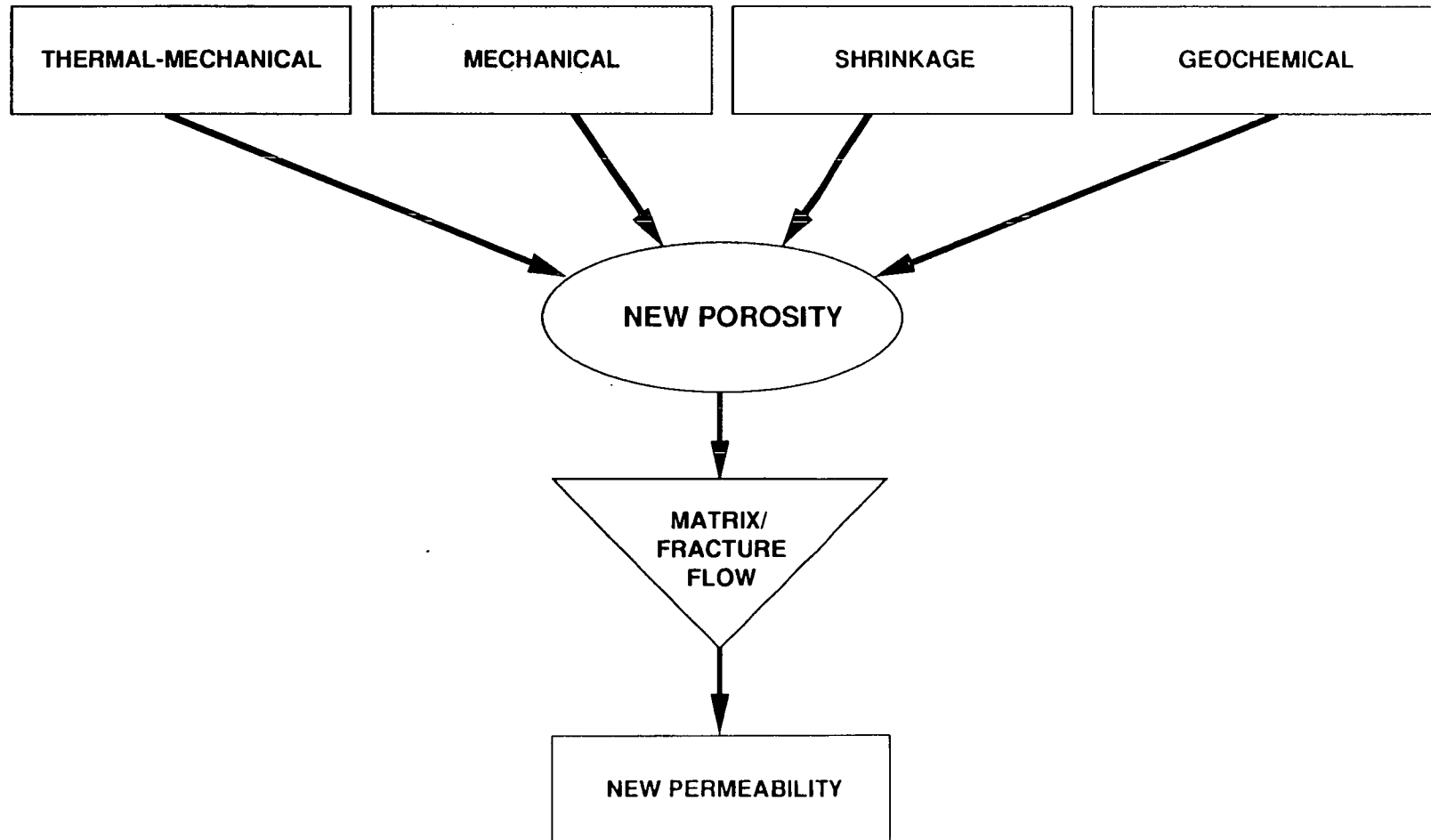
## Macroscopic Effects Anchor-to-Bedrock Seal



- Thermally-induced stresses less than half of confining stresses
- Similar results obtained for Station seal and Calico Hills seal

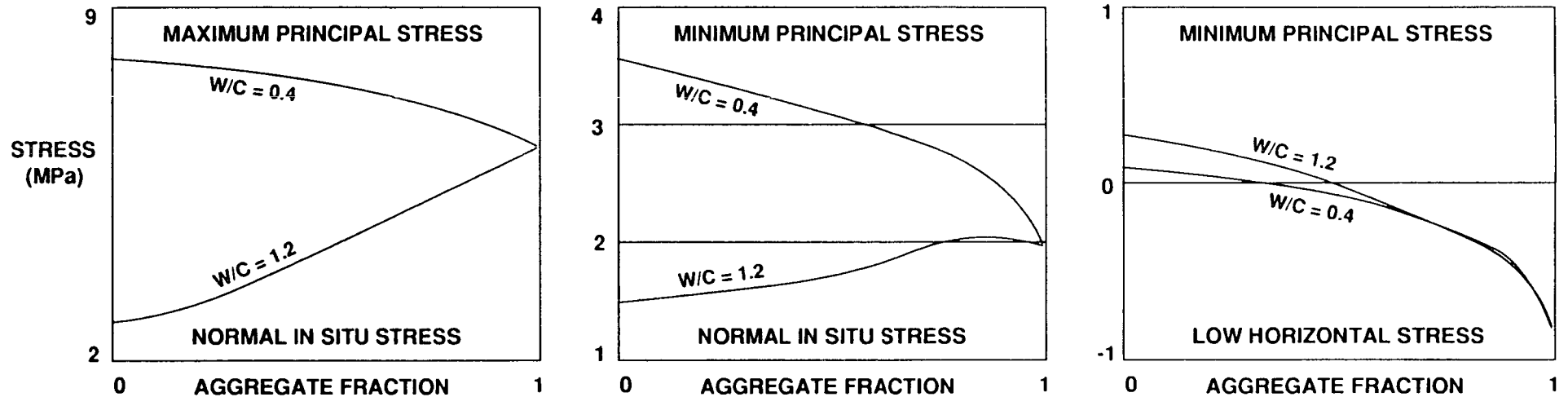
# Overview

## Cementitious Sealing Material Degradation Model



# Mechanical Interactions

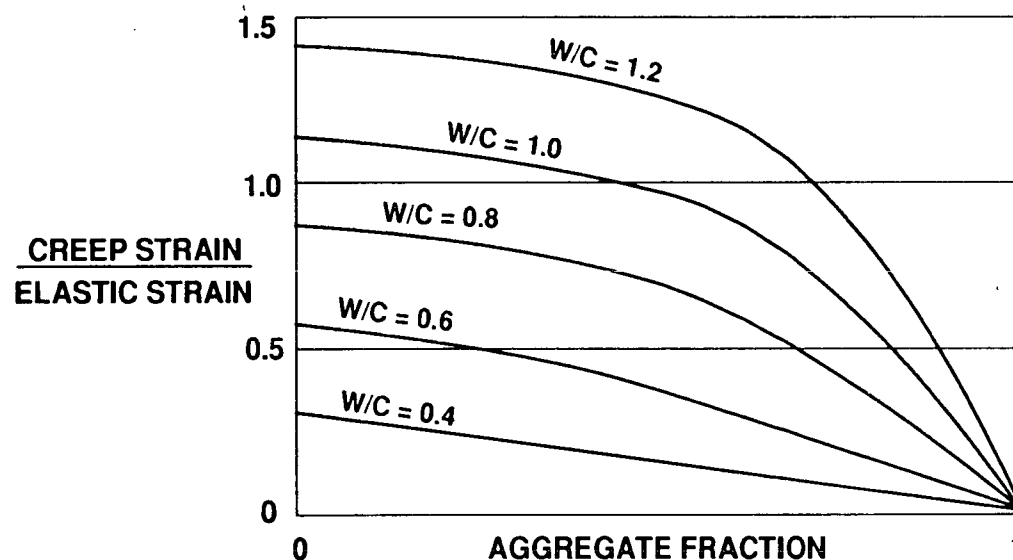
- Minimum and maximum principal stresses--spherical inclusion (Jaeger and Cook)



- For normal in situ stresses--plug stresses are minor
- For low horizontal stresses--high water/cement ratios and low aggregate fractions are preferred

# Mechanical Interactions

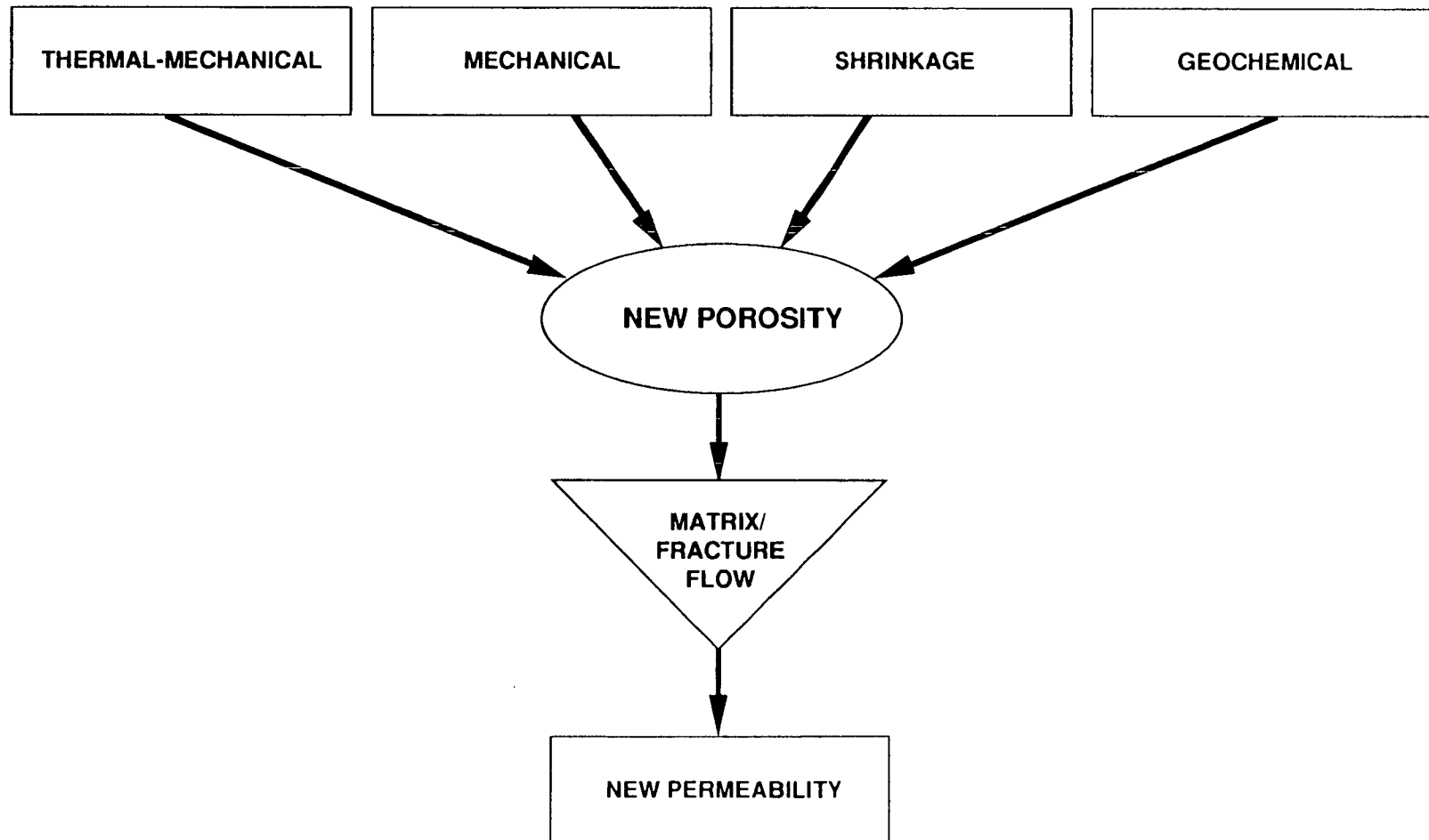
## Creep



- Comité Européen du Béton method
- Creep increases with higher water-to-cement ratios
- Creep increases with lower aggregate fractions
- Higher water-to-cement ratios and lower aggregate fractions preferred

# Overview

## Cementitious Sealing Material Degradation Model





# Shrinkage Interactions

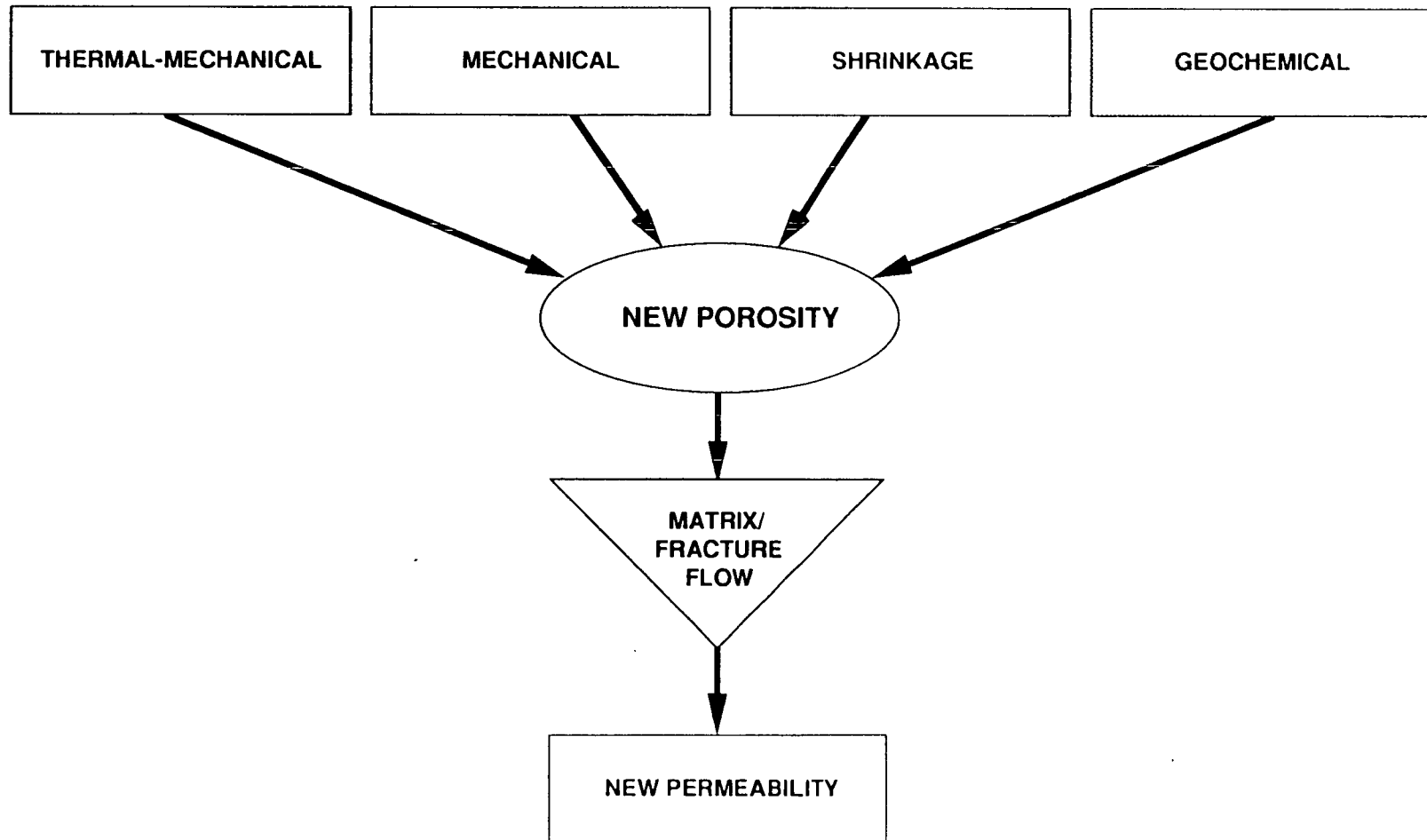
- Shrinkage-swelling effects controlled by relative humidity variations
  - For in situ saturations between 0.4 and 1.0, the relative humidity is bounded between 0.97 and 1.0
- 

## Conclusion

- Saturation variation will have little effect on shrinkage-swelling effects

# Overview

## Cementitious Sealing Material Degradation Model



# **Geochemical Interactions**

- **Cement - J-13 water interactions**
- 

## **Future Considerations**

- **Cement-tuff-water interactions**
- **Kinetic effects**
- **Leaching effects**
- **Validation**

# EQ3NR/EQ6 Geochemical Code Assumptions for the Interaction of Concretes with J-13 Water

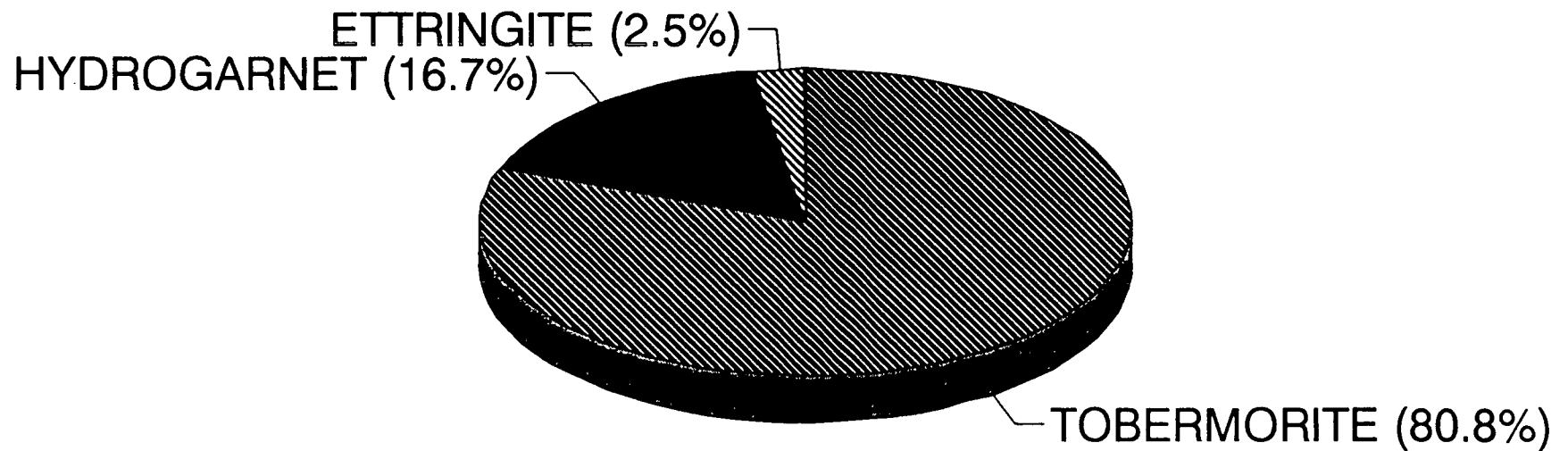
- Use of surrogates

BASE MATERIAL	SURROGATE
C-S-H GEL	TOBERMORITE
$C_3AH_6$	HYDROGARNET
SULPHATE CEMENT PHASE	ETTRINGITE
$SiO_2$	CRISTOBALITE

- Local equilibrium assumed
- Closed system assumed--dissolved gases limited
- Minerals suppressed

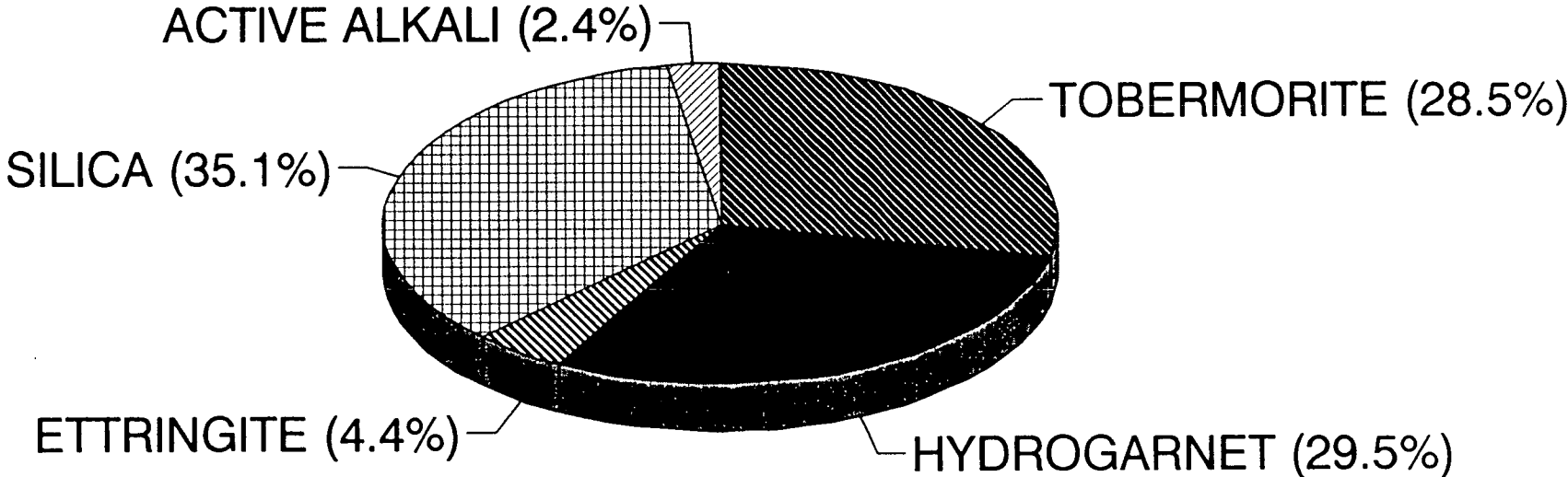
## OPC-B Concrete

OPC with Balanced Silica and Calcium



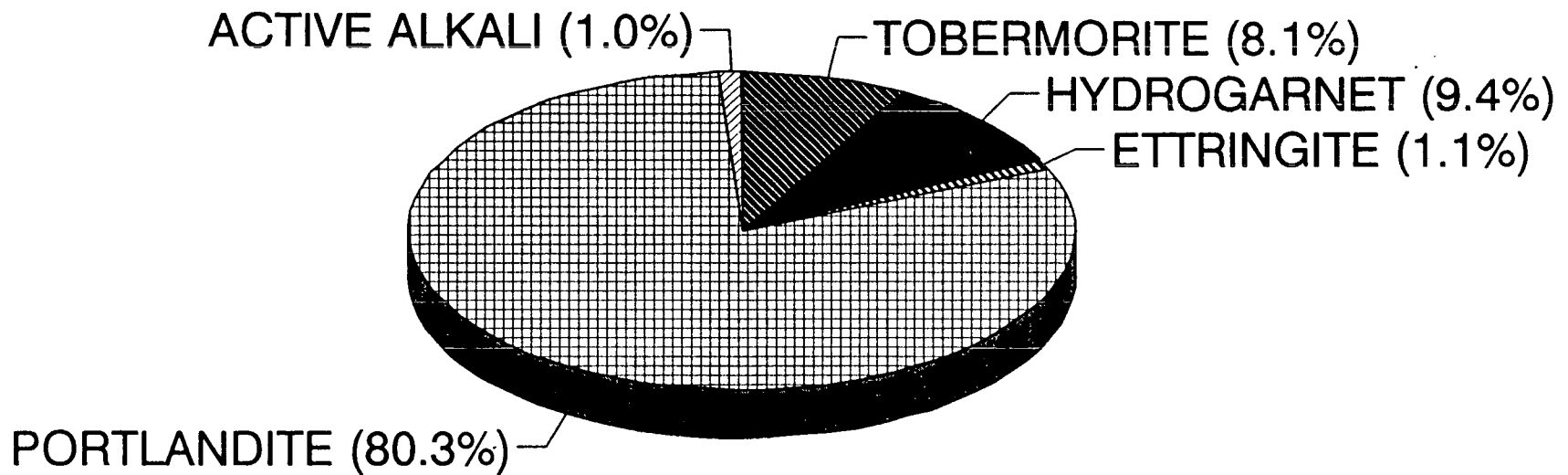
# EPC-S Concrete

Silica-Rich, Ettringite-Rich Concrete



# OPC-C Concrete

Calcium-Rich, OPC Concrete



## J-13 Water Composition

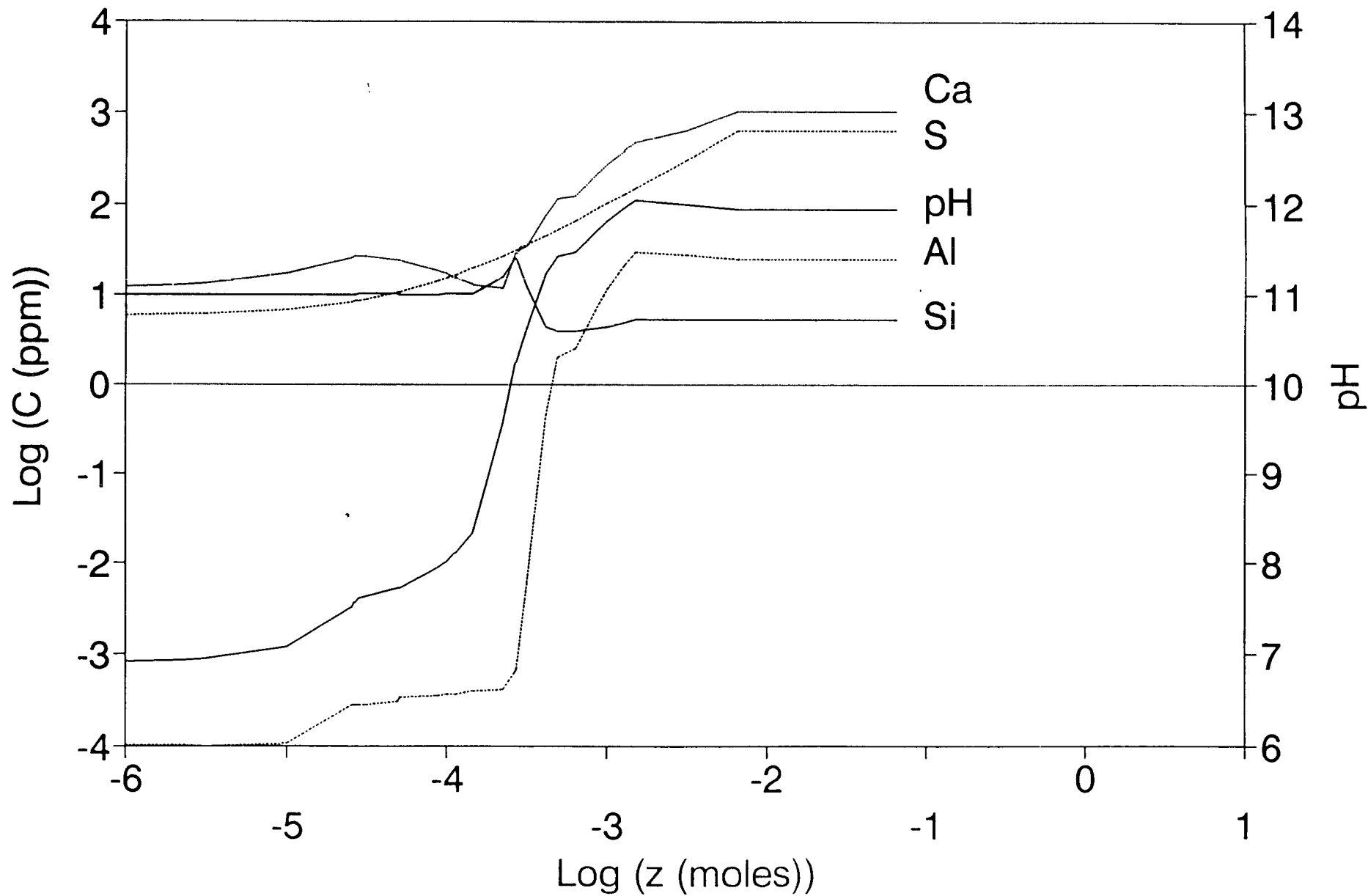
SPECIES	CONCENTRATION (mg/L)
Ca	11.62
Mg	1.75
Na	45.1
K	5.32
Li	0.062
Fe	0.045
Mn	0.001
Al	0.027
Si	30.05
F <sup>-</sup>	2.1
Cl <sup>-</sup>	6.4
SO <sub>4</sub> <sup>-2</sup>	18.25
NO <sub>3</sub> <sup>-</sup>	9.92
HCO <sub>3</sub> <sup>-</sup>	142.8 <sup>(1)</sup>

pH	6.9
Eh	0.120 V

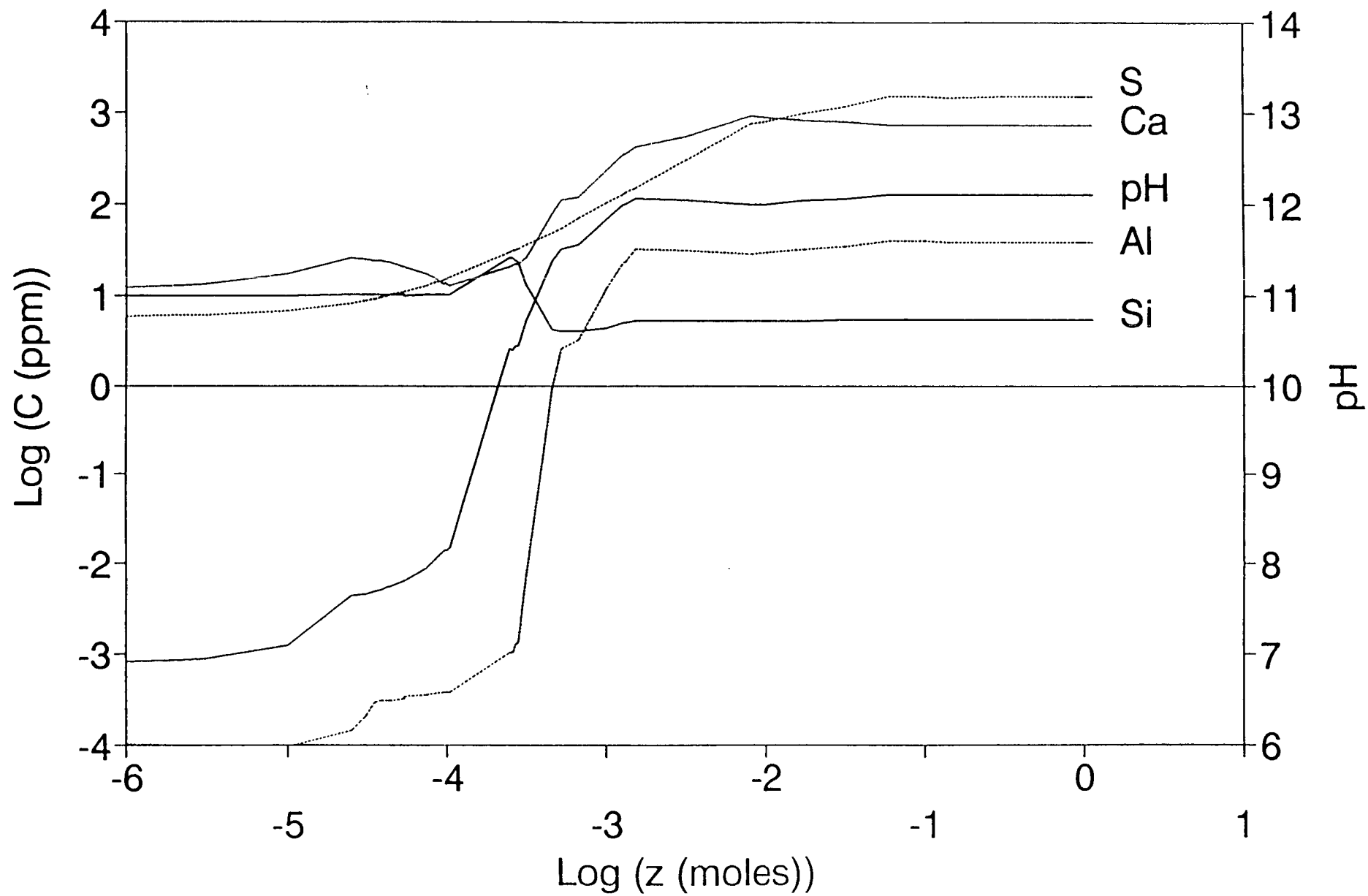
1. Titration alkalinity expressed as HCO<sup>3-</sup>.



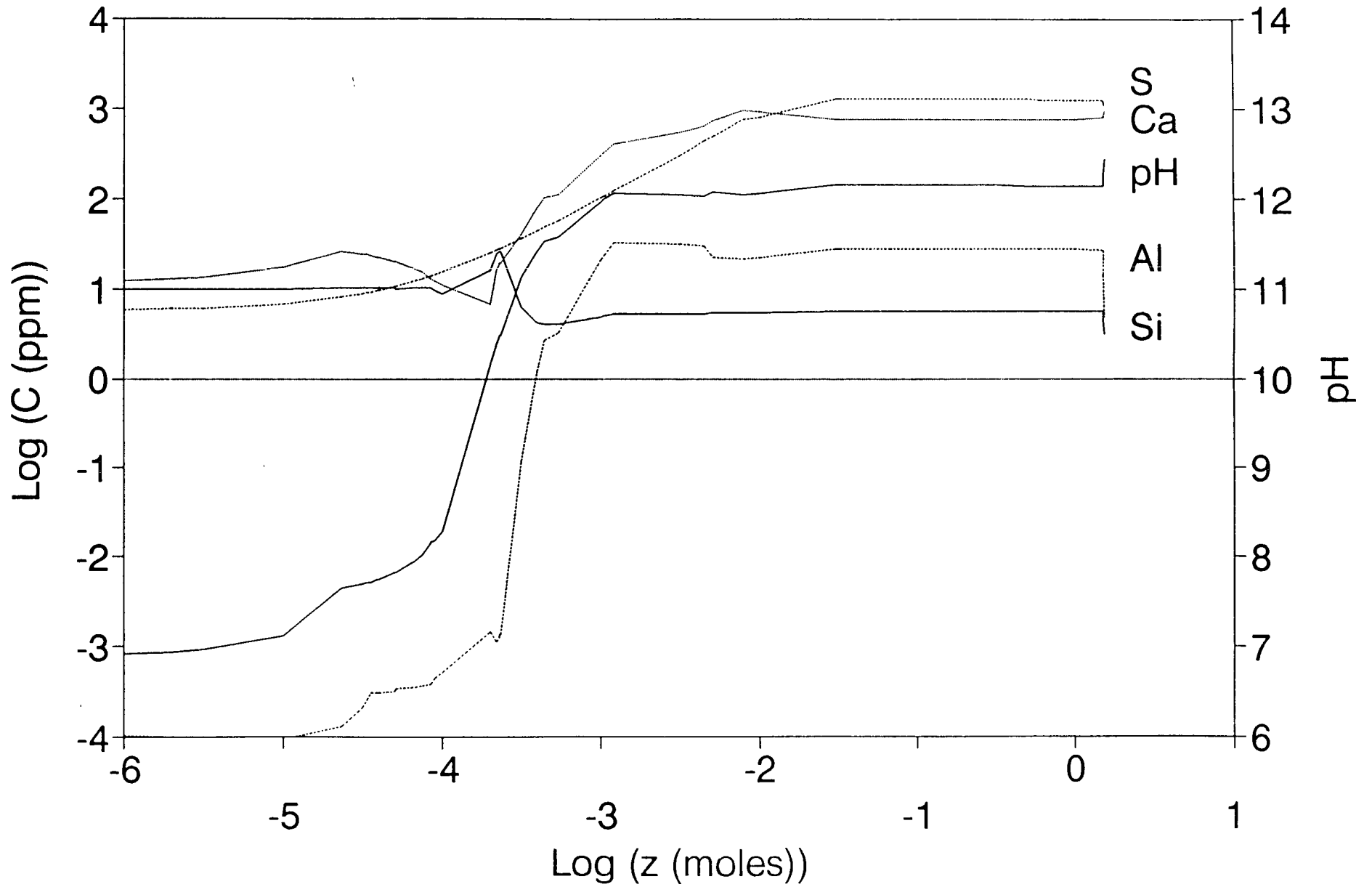
# OPC-B Concrete



# EPC-S Concrete

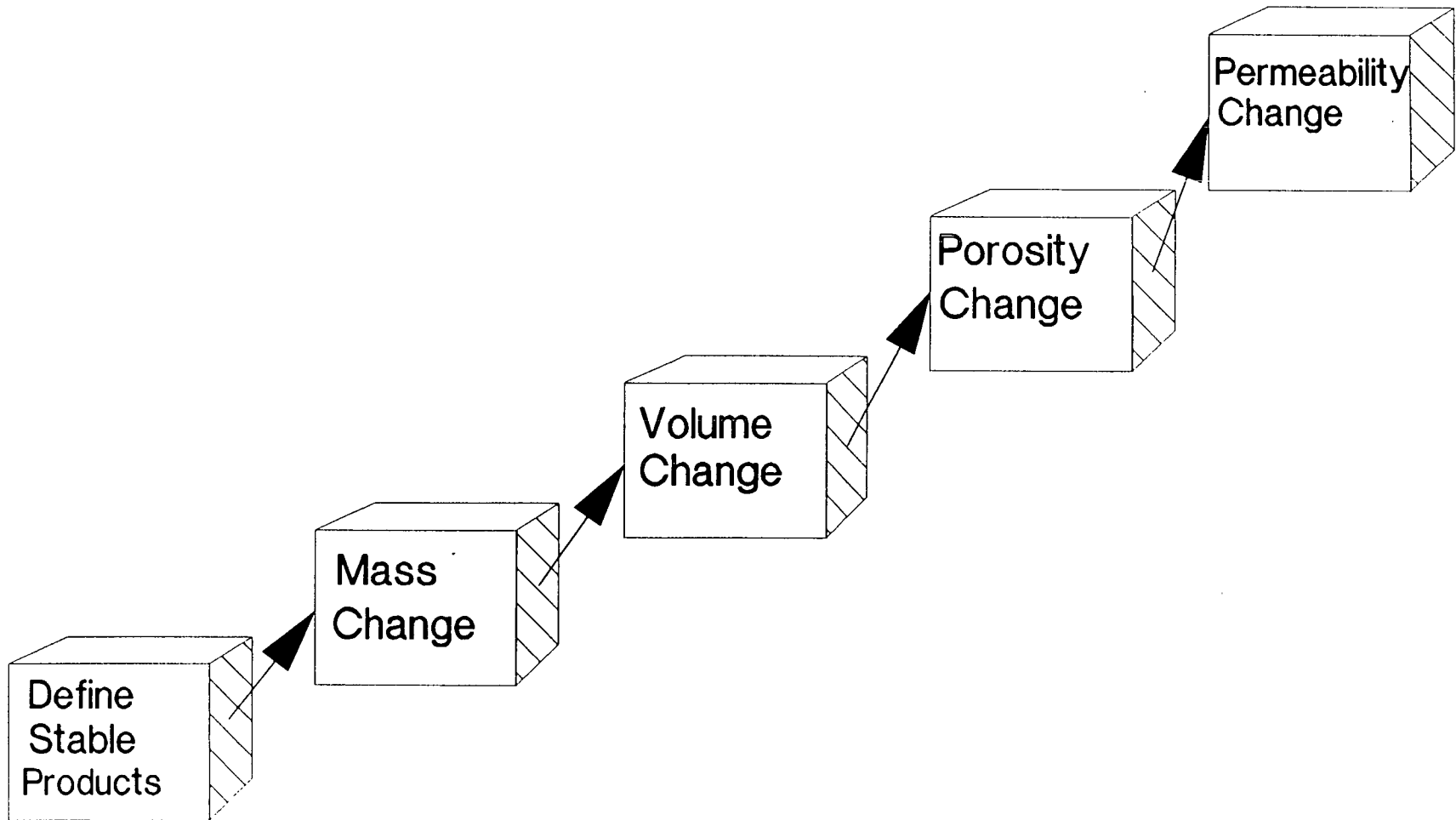


# OPC-C Concrete

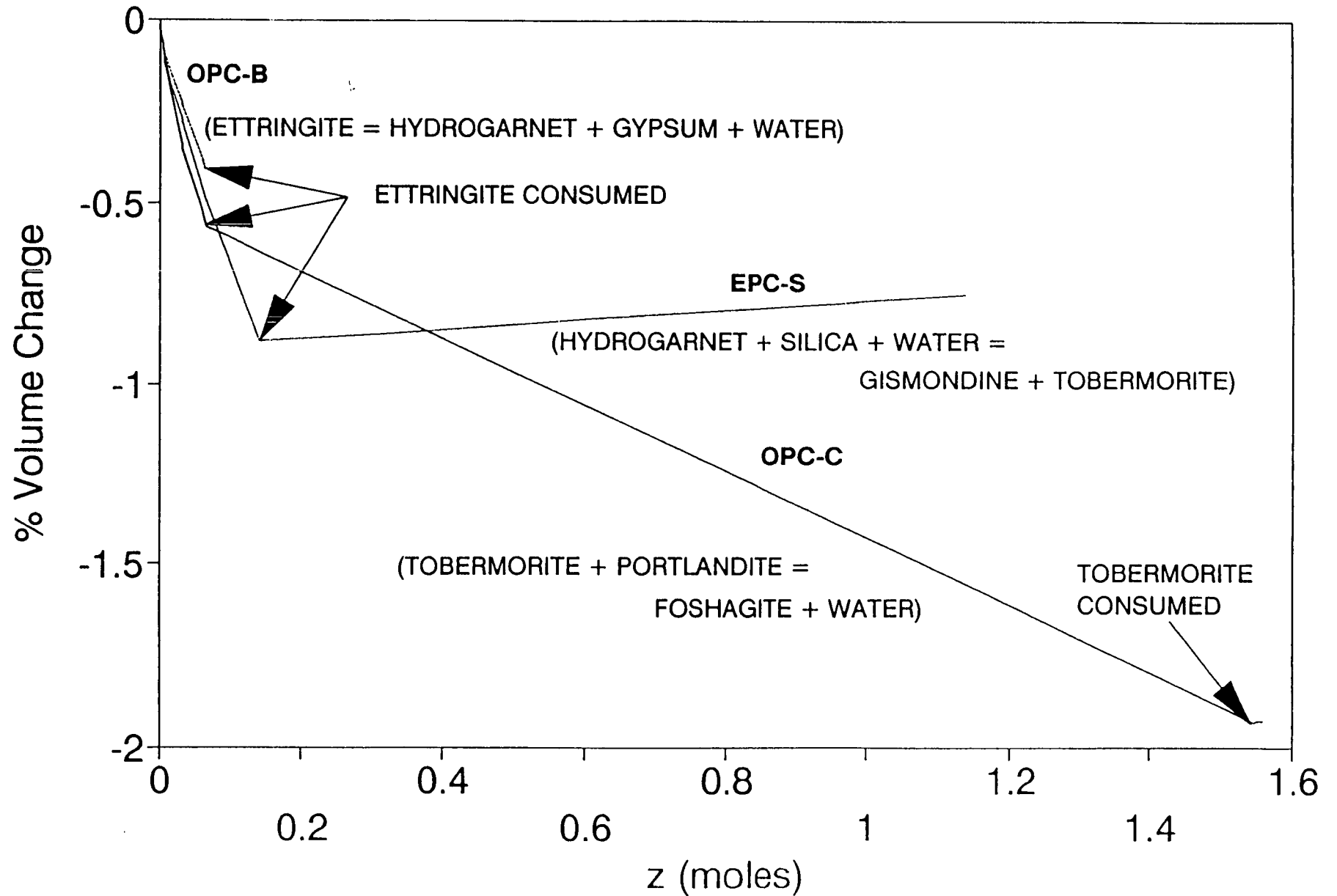


# Steps in Modeling Cement

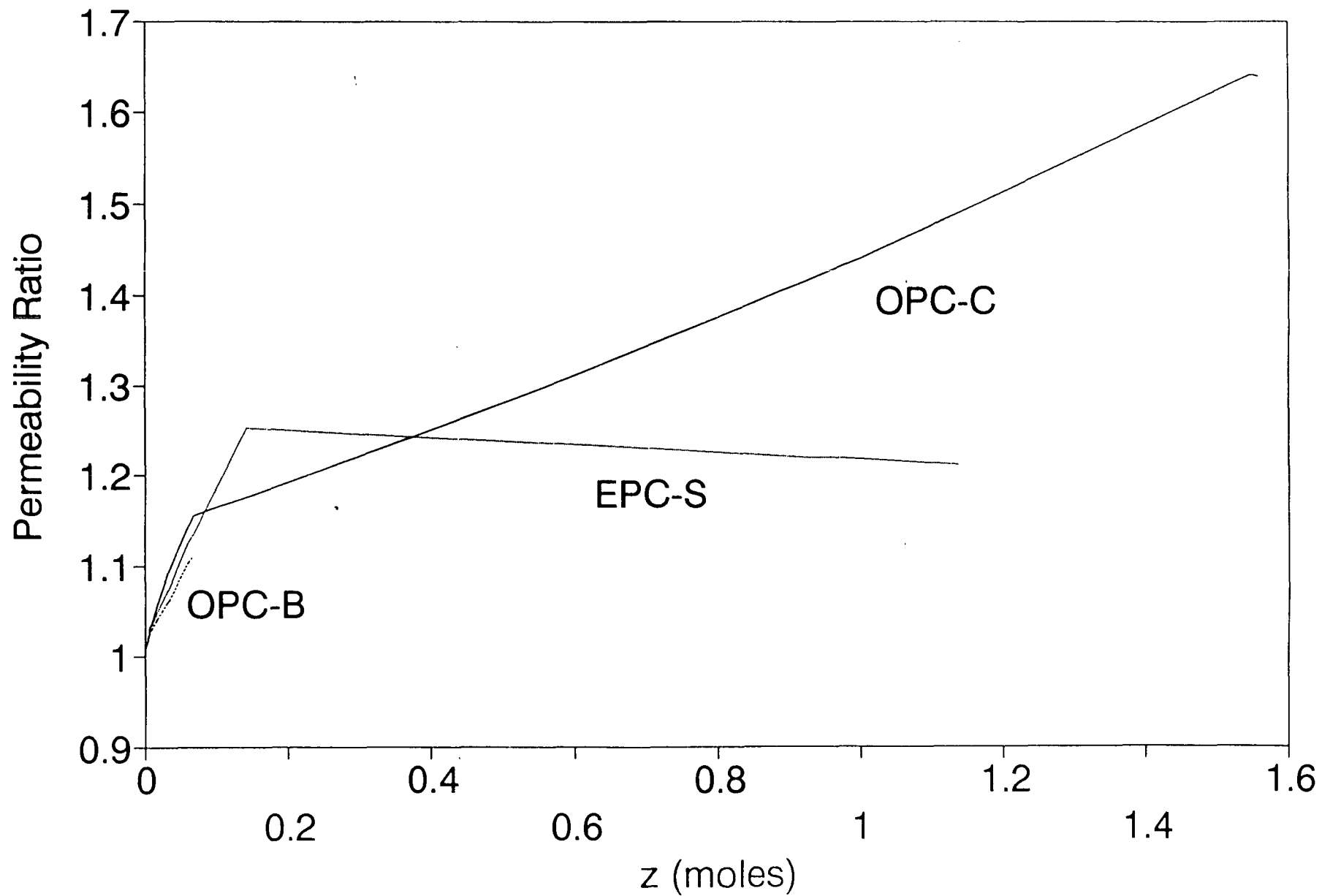
## Permeability Modification



# Projected Change in Volume



# Projected Change in Permeability



# Summary of Geochemical Interactions

## Water Chemistry

- Calcium-rich and silica-rich concretes have similar responses in J-13 water
  - Small concrete addition--solution strongly buffered by J-13 water
  - Large concrete addition--concrete dominates solution

## Concrete Alteration

- For closed system--reducing conditions and minimal carbonate formation
- Mass and volume change is described by a few chemical reactions
  - Ettringite and Portlandite open concrete structure
  - Excess silica tightens the concrete structure
- Permeability changes for this study are small

## **Conclusions from Geochemical Considerations**

- **Material screens indicate that both cements and earthen materials are potentially suitable as sealing materials**
- **Cementitious material evaluations indicate that high-quality cementitious sealing materials may be achievable by controlling the cement composition**
  - **Important factors**
    - **Calcium-to-silica ratio**
    - **Water-to-cement ratio**
    - **Aggregate weight percent**
    - **Gypsum**
    - **Portlandite**
    - **Unreacted cement phases**



