

LARP

HQS Progress Report

High Field Nb₃Sn Quadrupole Magnet

Shlomo Caspi

LBNL

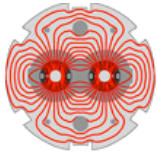
Collaboration Meeting – CM11

FNAL

October 27-28, 2008



S. Caspi, LBNL



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Introduction

- large bore (120mm)
 - high field (15.2T) (3000 A/mm², 4.2K, 12T)
 - Gradient 219 T/m at 1.9 K
 - Accelerator quality

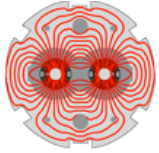
Collaboration :

- BNL – reaction and potting tooling
- FNAL – magnetic design, Islands, wedges, “end” spacers
- LBNL – cable, winding & curing tooling, mechanical design, magnet assembly.

Outline :

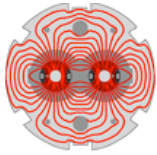
- Magnetic design
- Mechanical design
- Tooling design.





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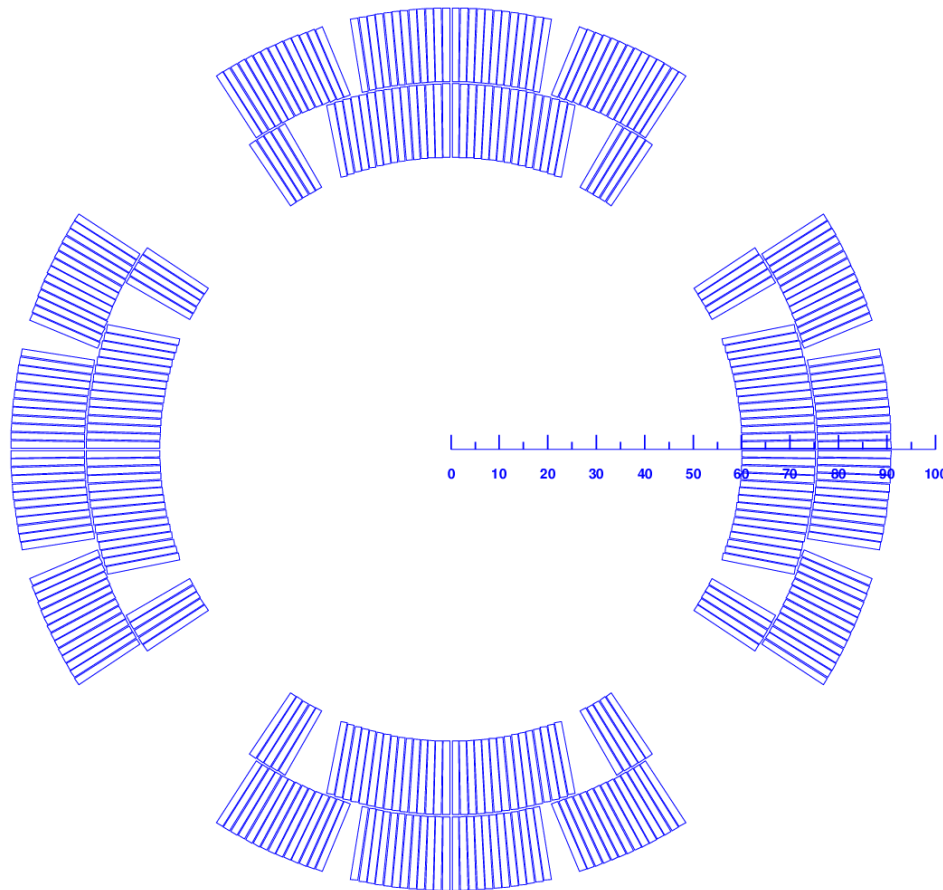
Magnetics



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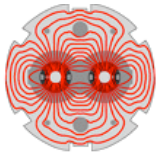
Coil cross-section and parameters

Courtesy of V. Kashikhin



Coil aperture	mm	120	
Yoke OR	mm	260	
Cable reference name	-	HQ-KC2	
Bare cable width	mm	15.150	
Bare cable mid-thickness	mm	1.437	
Cable keystoneing angle	deg	0.750	
Cable insulation thickness	mm	0.100	
Turns per quadrant IL/OL	-	20/26	
Minimum pole width	mm	23.82	
Midplane shim per octant	mm	0.140	
Quench* gradient @ 1.9K	T/m	219.78	
Quench* peak field @ 1.9K	T	15.29	
Quench* current @ 1.9K	kA	19.57	
Inductance @ quench*	mH/m	7.71	
Stored energy @ quench*	MJ/m	1.48	
Octant forces @ quench	F_x total	MN/m	3.38
	F_y total	MN/m	-5.03
	F_θ IL/OL	MN/m	2.63/3.15

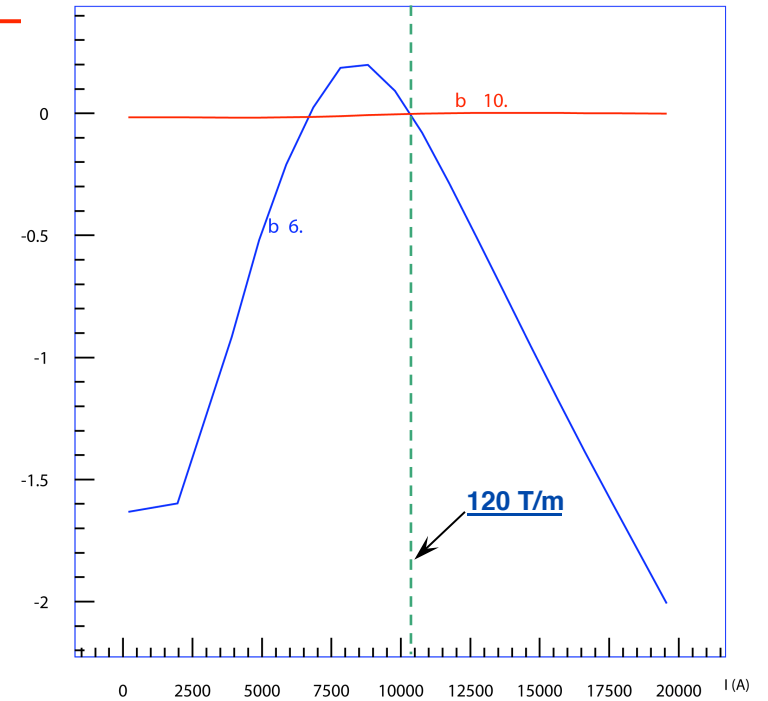
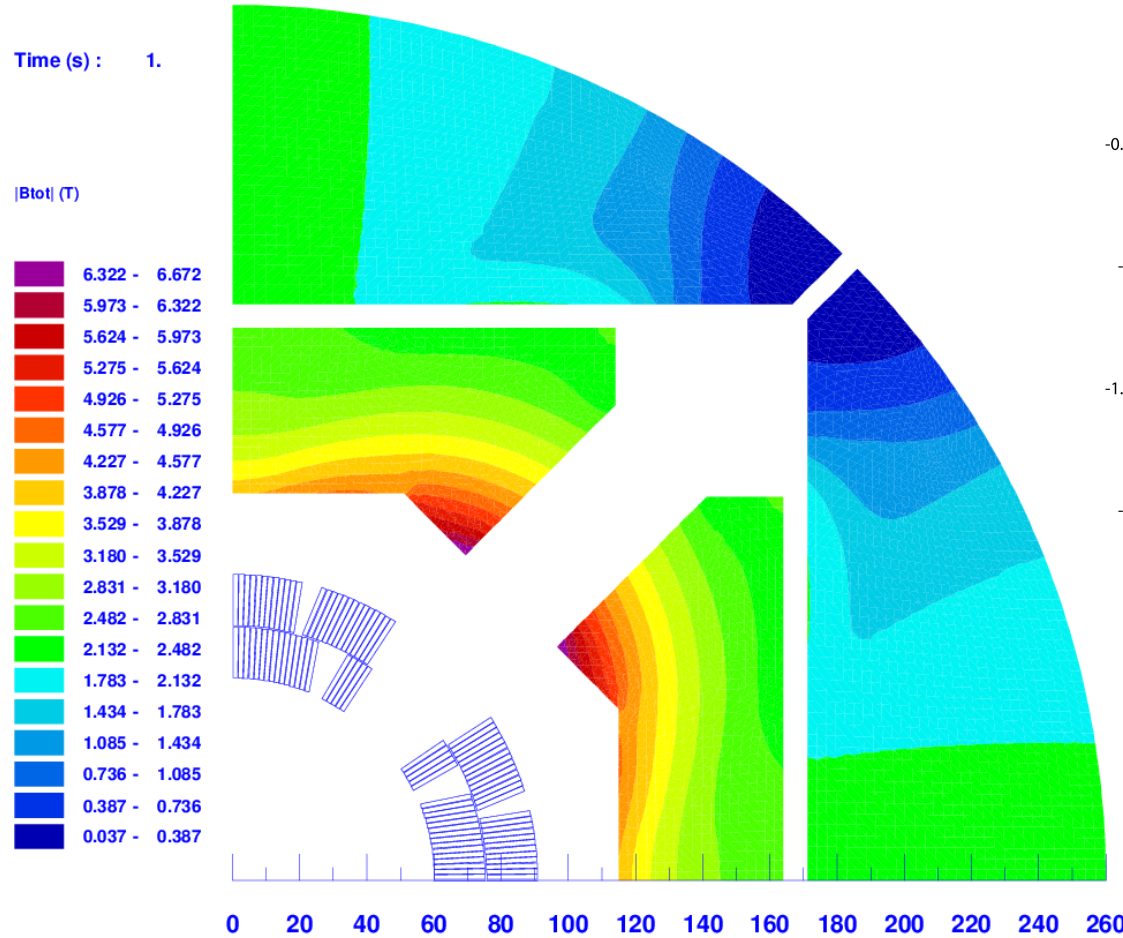
* $J_c(12T, 4.2K) = 3000A/mm^2$, $K_{cu/nonCu} = 0.87$



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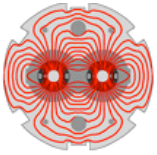
Iron saturation & field quality - Roxie

Courtesy of V. Kashikhin



Field reference radius		mm	40
Harmonics @ 10 T/m	b ₆	-	-1.6317
	b ₁₀	-	-0.0156
	b ₁₄	-	-0.0106
	b ₁₈	-	-0.3910
Harmonics @ 120 T/m	b ₆	-	0.0000
	b ₁₀	-	-0.0021
	b ₁₄	-	-0.0118
	b ₁₈	-	-0.4059

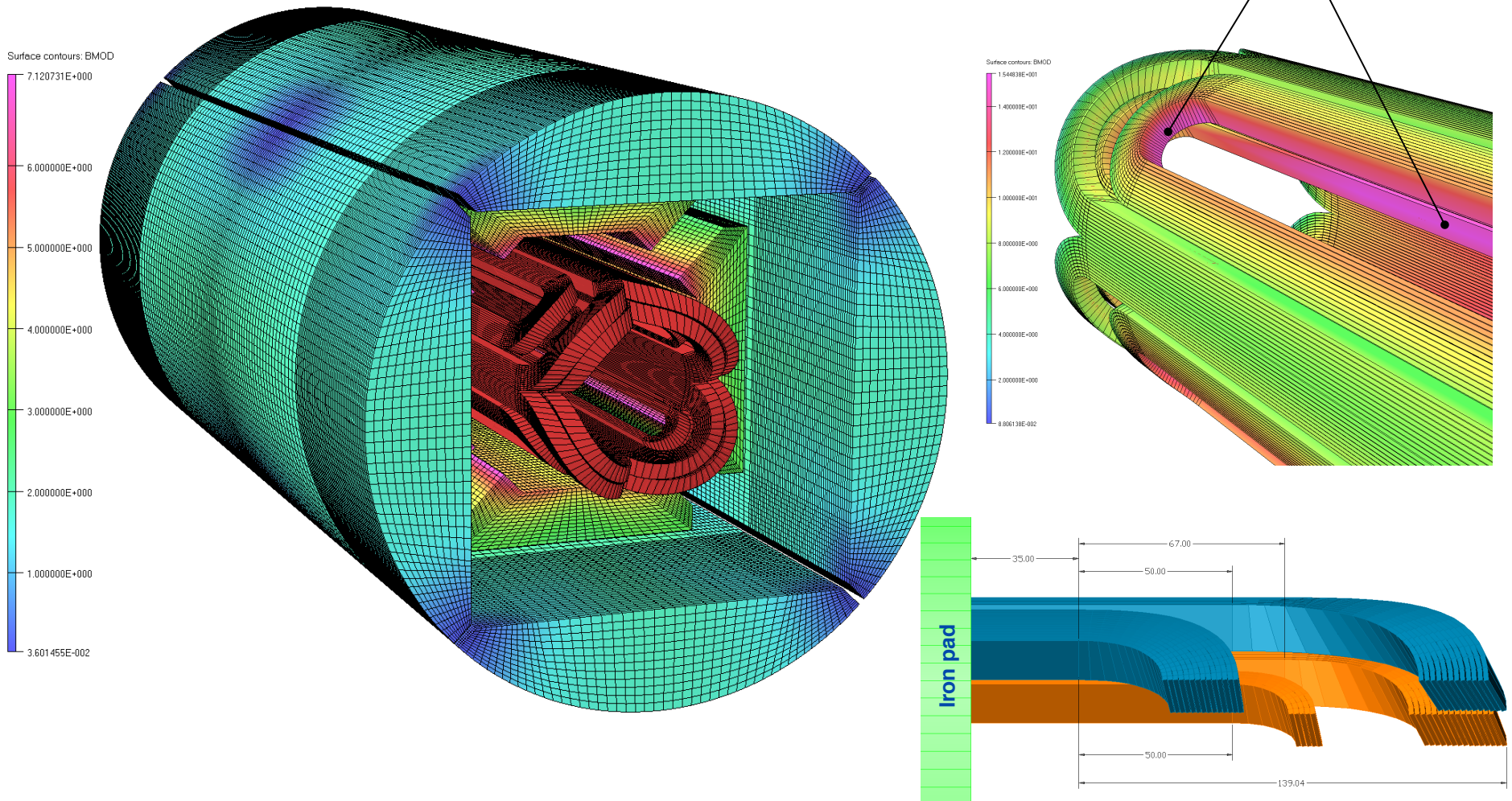


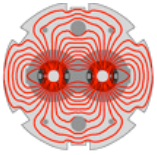


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3D analysis - Tosca

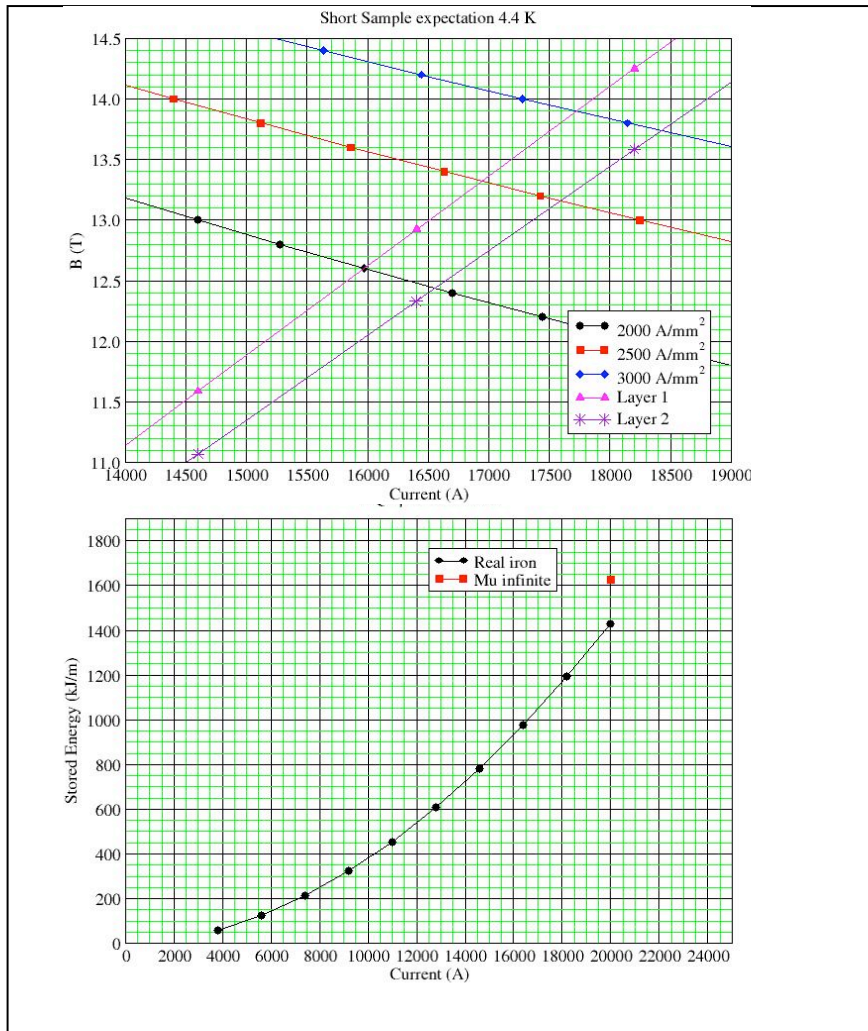
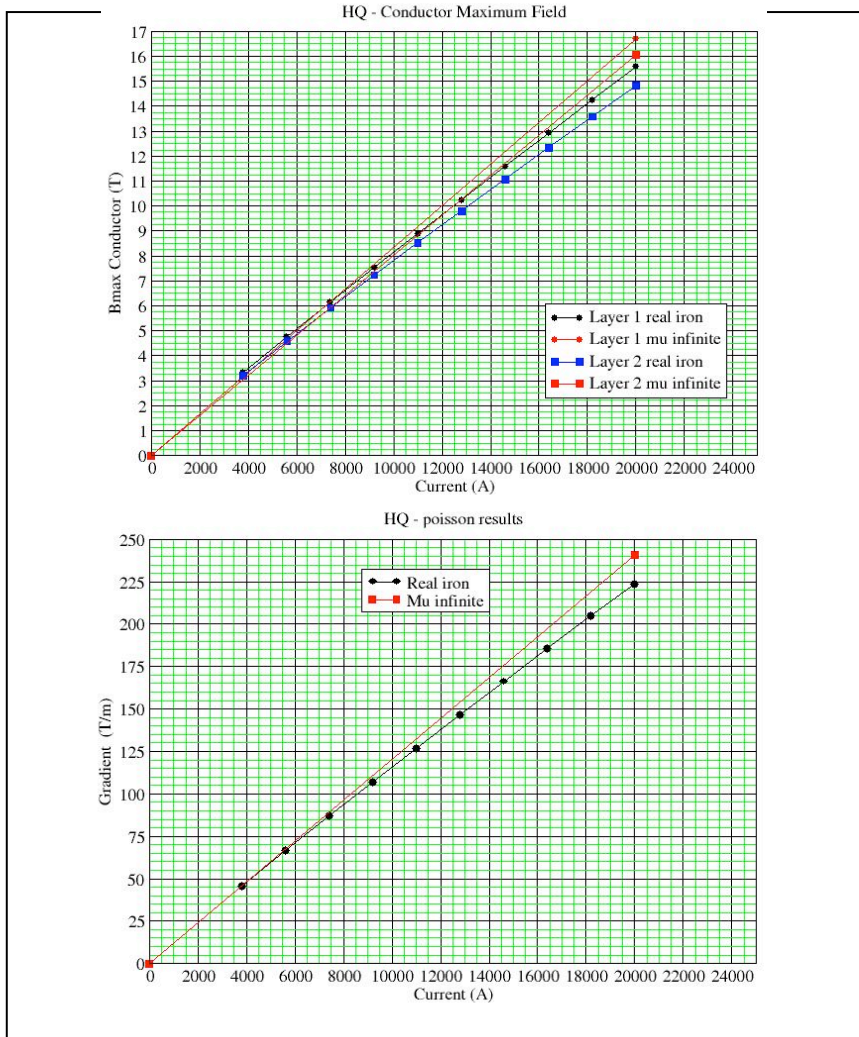
Courtesy of V. Kashikhin

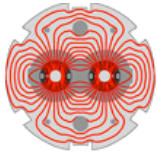




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Field, Gradient, Stored-energy - Poisson

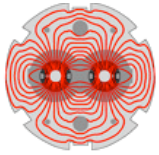




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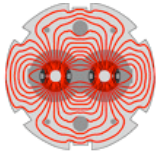
Short-sample straight section

1.9 K / 4.4 K	Layer 1			Layer 2		
A/mm²	2000	2500	3000	2000	2500	3000
I_{max} (kA)	17.5/15.98	18.58/16.95	19.45/17.72	18.14	19.30	20.22
B_{max} (T)	13.72/12.59	14.52/13.3	15.17/13.9	13.55	14.34	14.98
G_{max} (T/m)	197/181	208/191	219/199			



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Mechanics

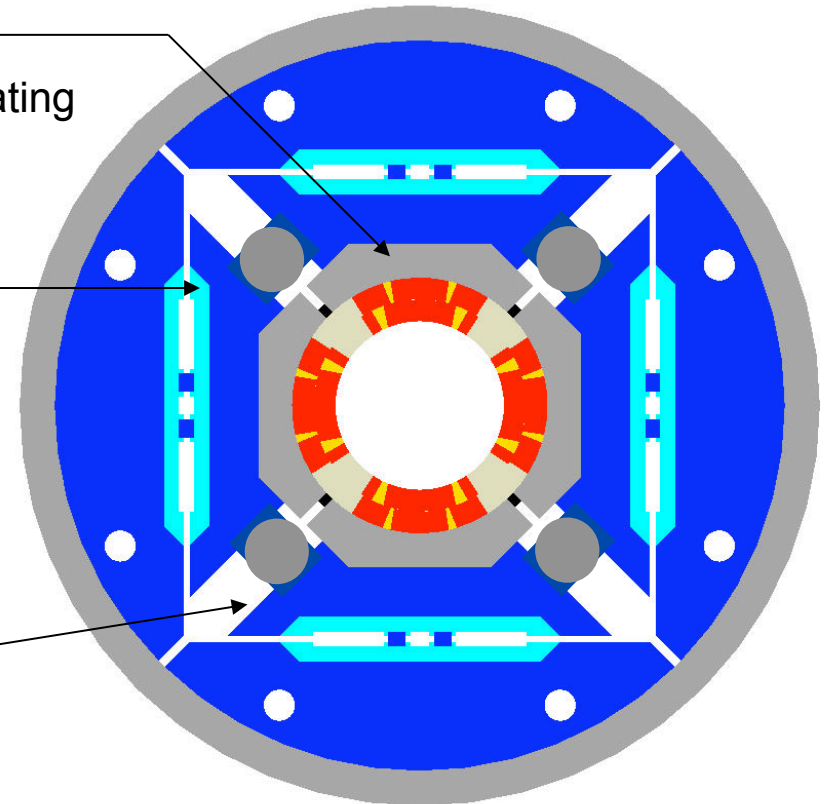


HQS – Mechanical Shell based Structure

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Components

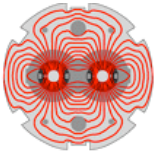
- Aluminum bolted collars => alignment
 - remains in compression from assembly to operating conditions
- Iron pads and yoke
- Iron master key => alignment
- axial rods => axial preload
- 25 mm aluminum shell => azimuthal preload
 - Coil and collar in compression
- Cooling area



Assembly

- 60 mm bladders located outside the key span
- 38 MPa pressure (600 + 50 microns clearance for 220 T/m)
- Collars, pads and key locations optimize to minimize stress

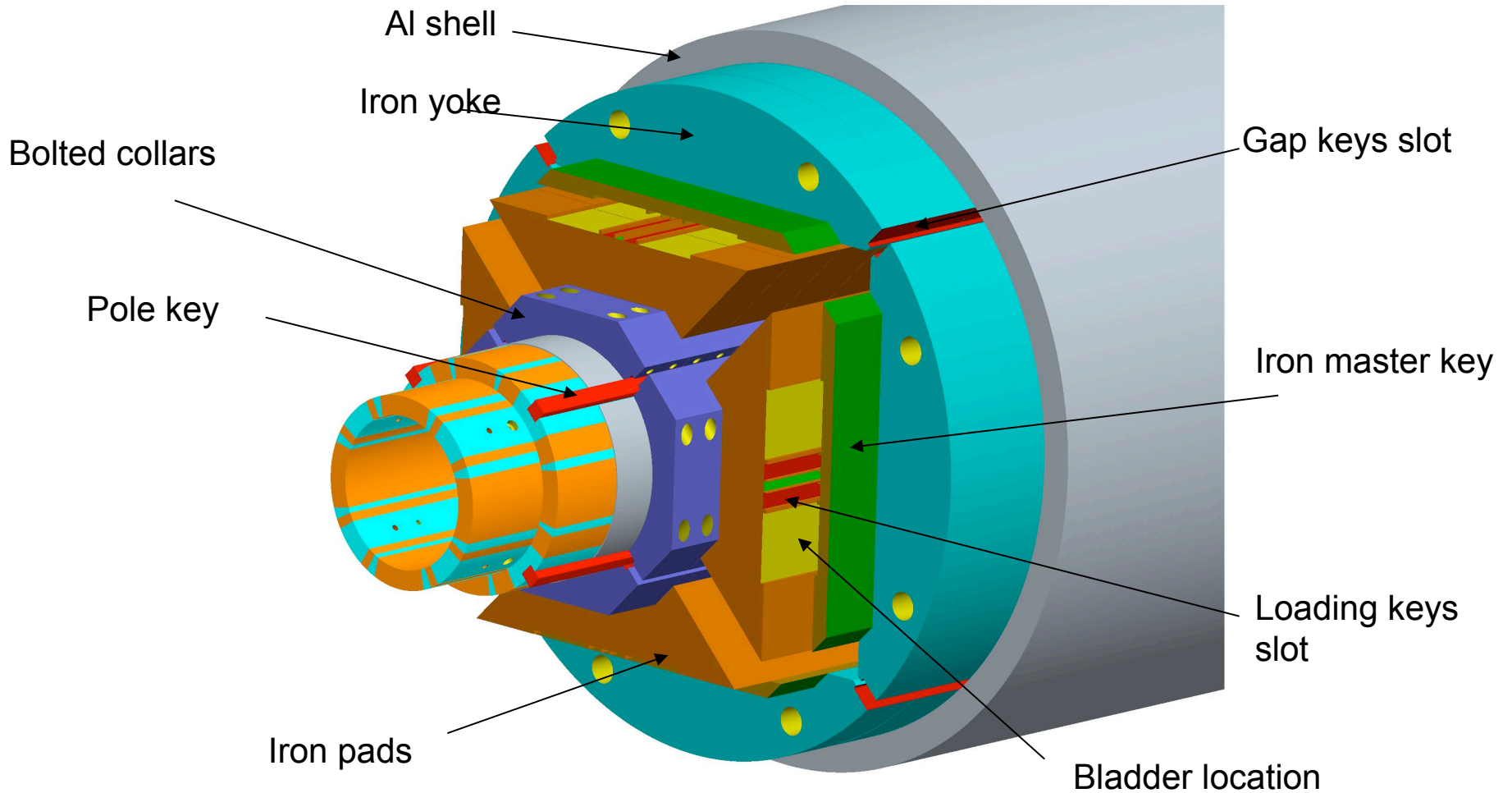
570 mm outer diameter

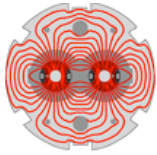


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HQ – CAD Model

Courtesy of D. Cheng

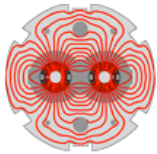




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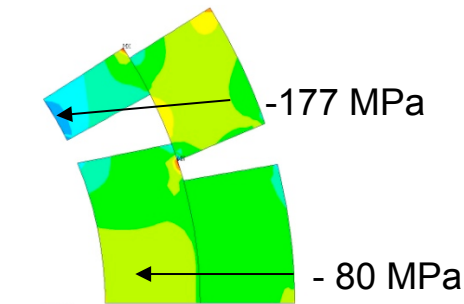
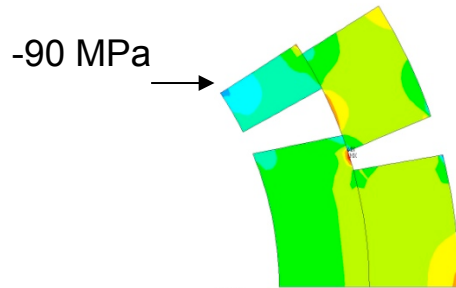
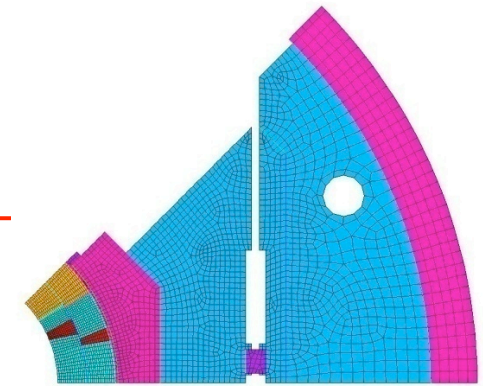
Design Concept and Guidelines

- Use modified pads and collars for coil alignment
 - Collars for azimuthal alignment (**not for pre-stress**)
 - Bolted pads for coils assembly
 - Keys, bladders and Aluminum shell during final azimuthal assembly
 - Axial rods to control axial forces
- Final pre-stress during cool-down by a shell based Aluminum structure
- Maintain full azimuthal contact between coil-island and island-collar
 - Bladder and key locations optimized
- Structure to maintain pre-stress up to expected “short-sample” but coil pre-stress can be reduced if adjusted to the operating point.

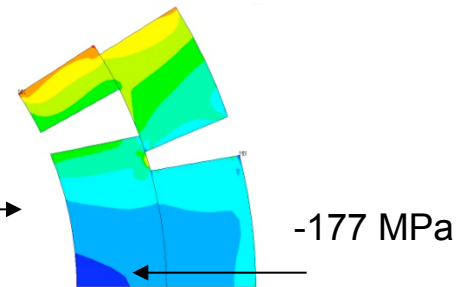
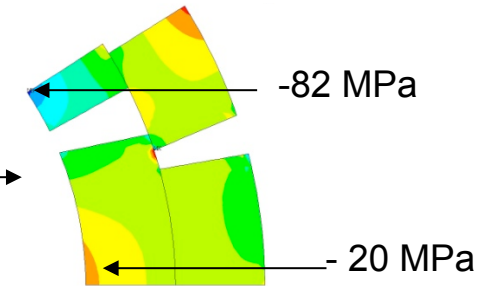


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HQ – Mechanical analysis Azimuthal stress in the coil



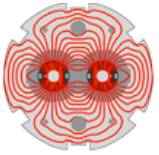
	Target 219 T/m
During bladder operation	-90 MPa
With loading key	-82 MPa
At 1.9 K	-177 MPa
With Lorentz forces	-177 / 20 MPa



=> High but acceptable stress at short sample

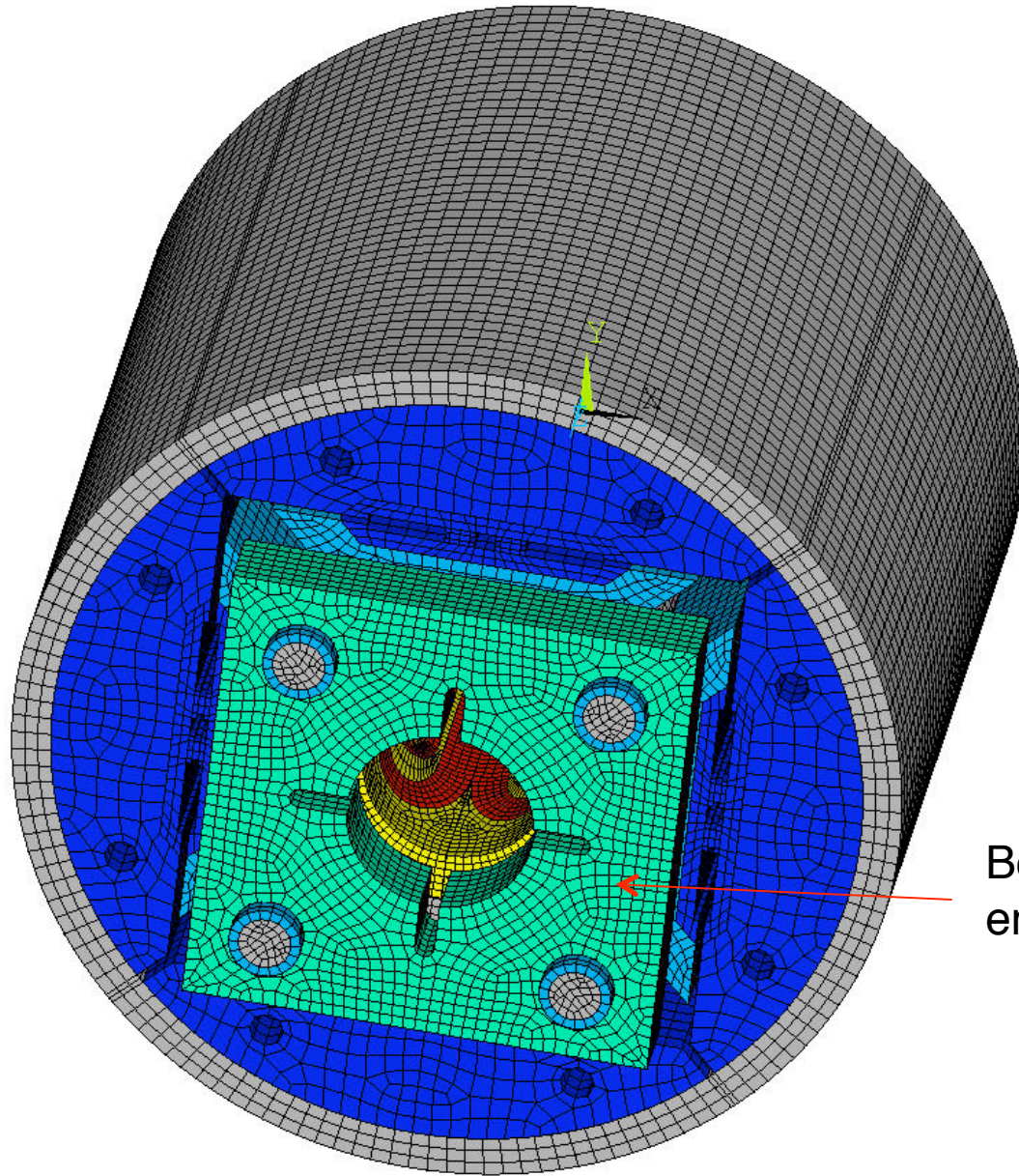
Courtesy of H. Felice



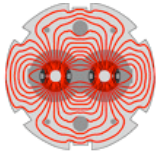


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Axial
Aluminum
rods

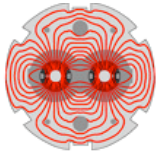


Bolted to a Nitronic
endplate



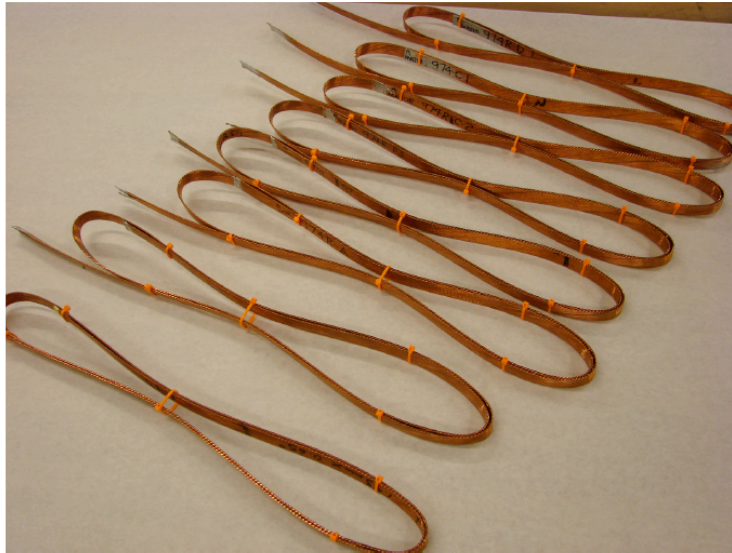
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Winding-Curing-Reaction-Potting



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HQ – Cable optimization



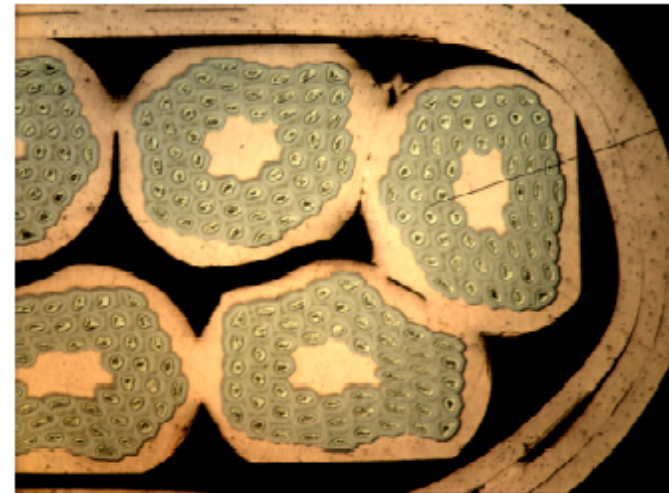
Test winding samples

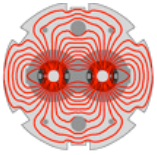
Variation of the keystone angle, thickness...

Up to now, 8 cables evaluated

Micrographs analyzed for each sample

- Edge deformation – strand distortion
- Deformation of the sub-elements
- Barrier
- Size of the facets on the surface of the cable





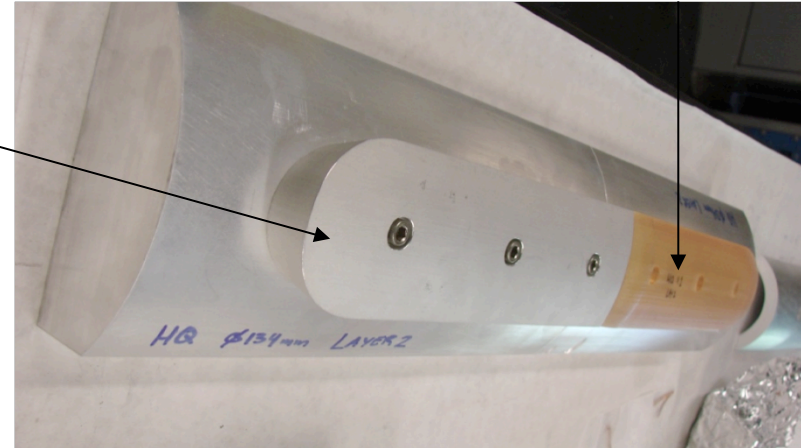
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HQ – Winding tests

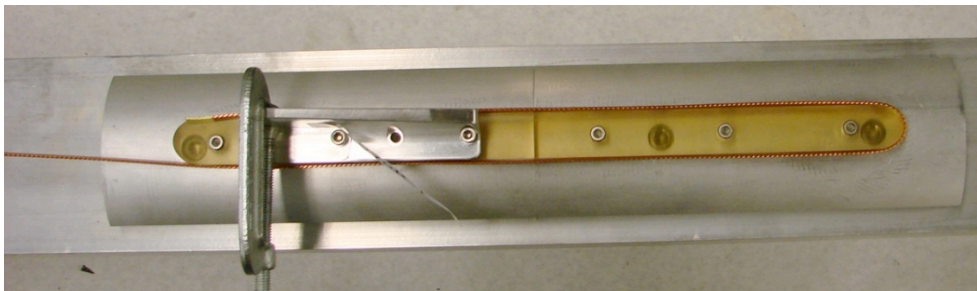
EDM part return end



Rapid Prototype (RP) part lead end



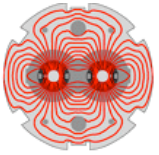
114 mm aperture mandrel



134 mm aperture mandrel

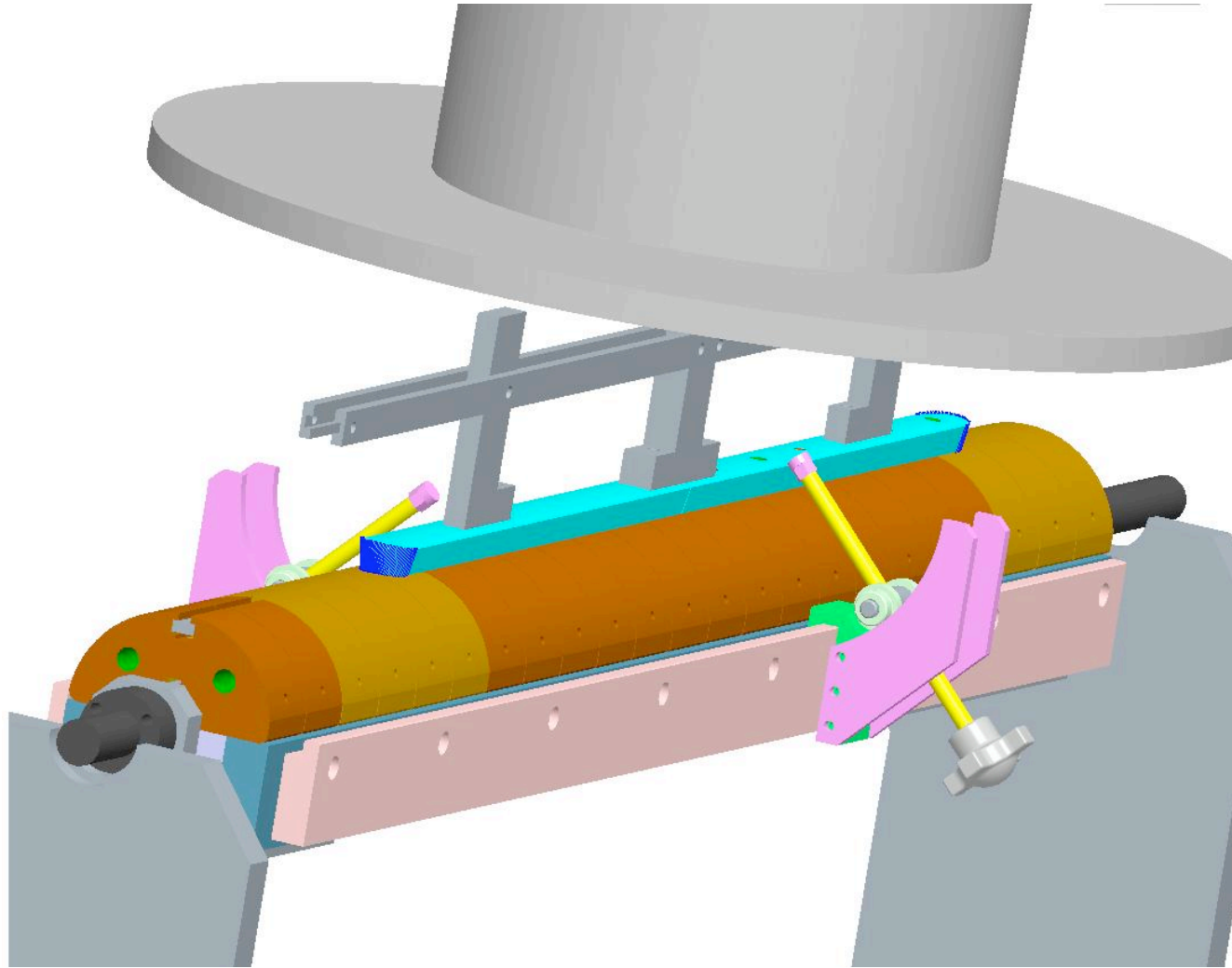


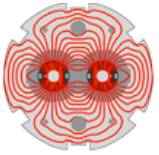
=> 120 mm cross-section: minimum pole width 23.8 mm



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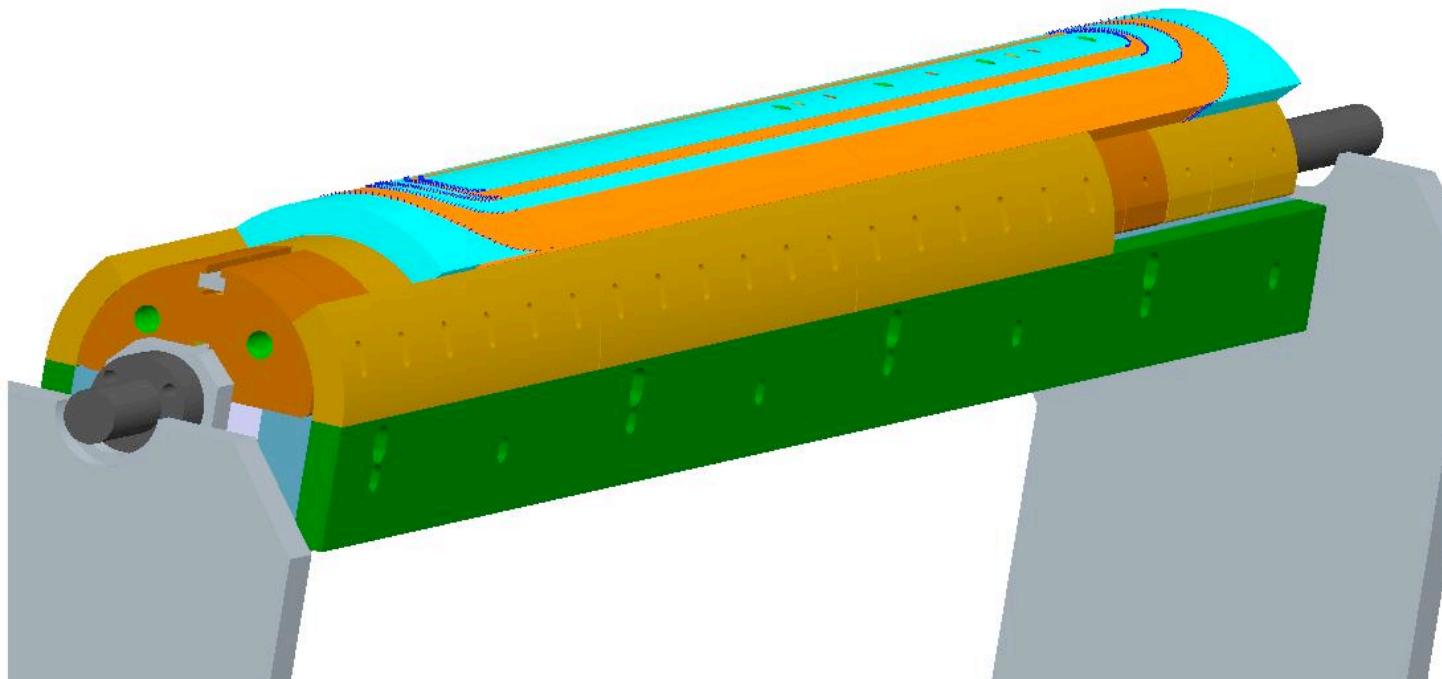
Winding tooling

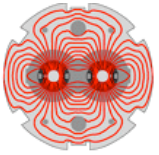




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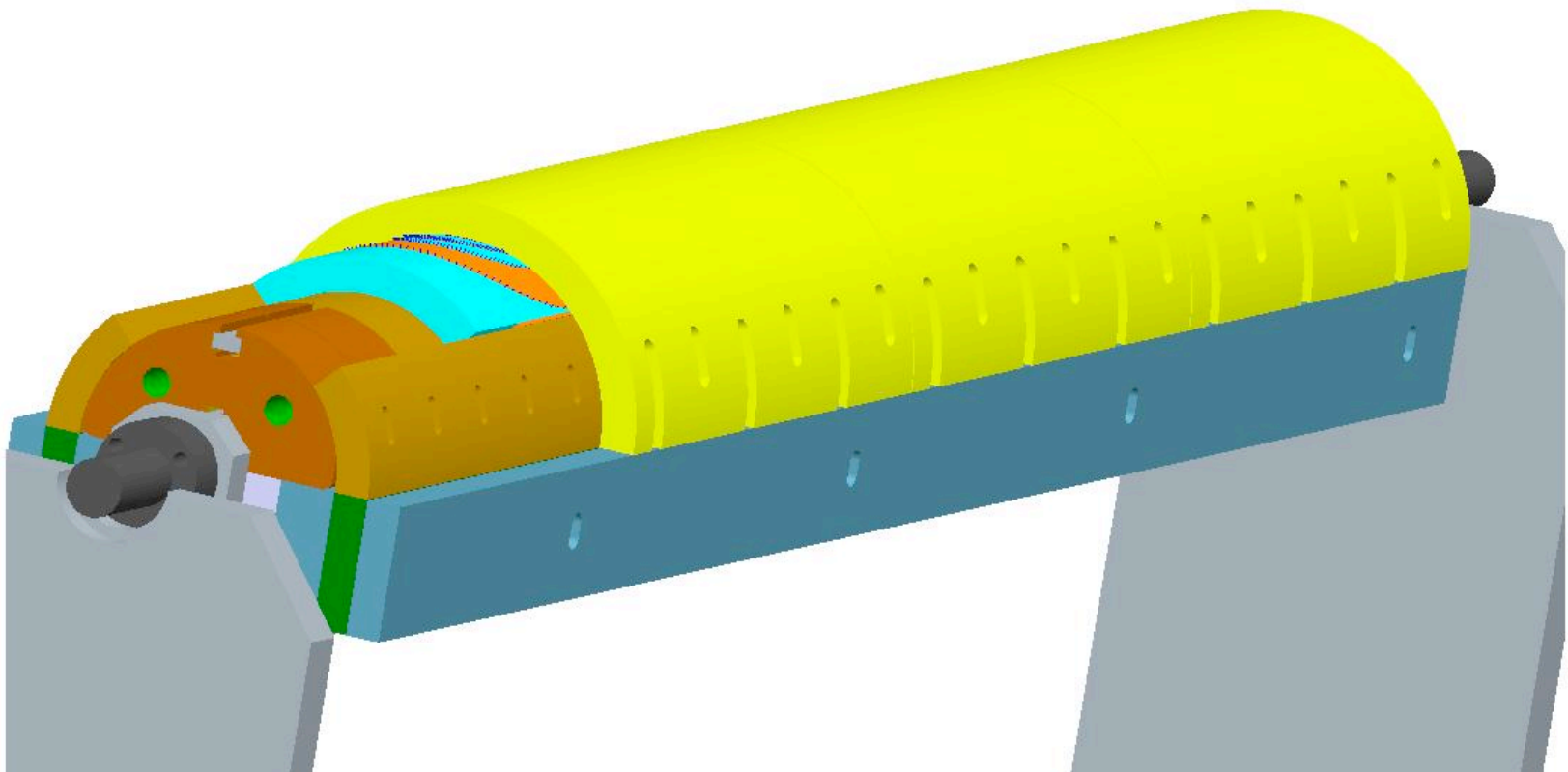
Winding layer 1

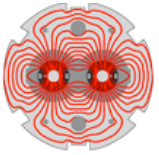




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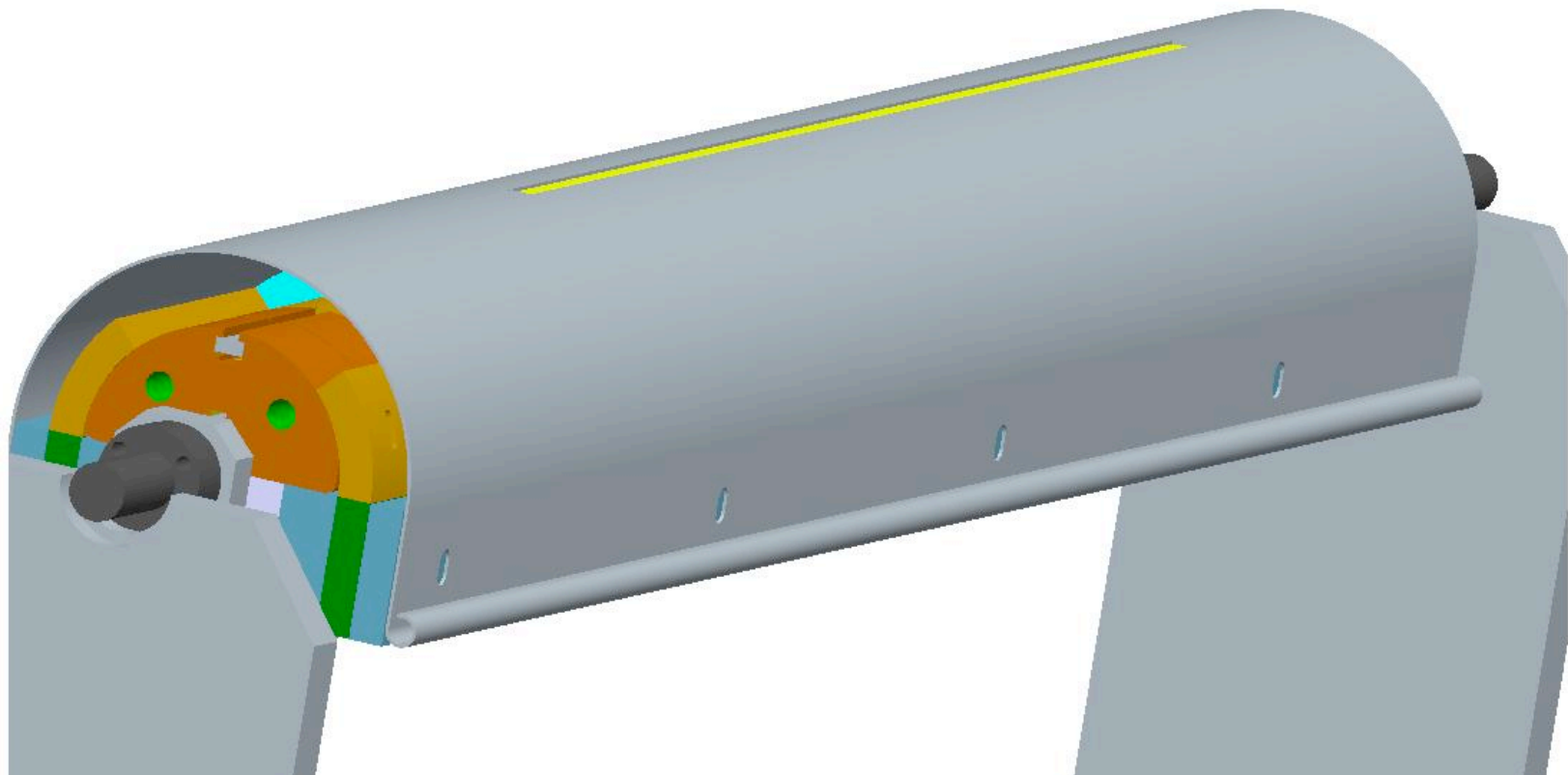
Layer 2 spacer

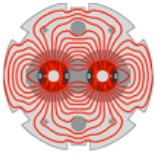




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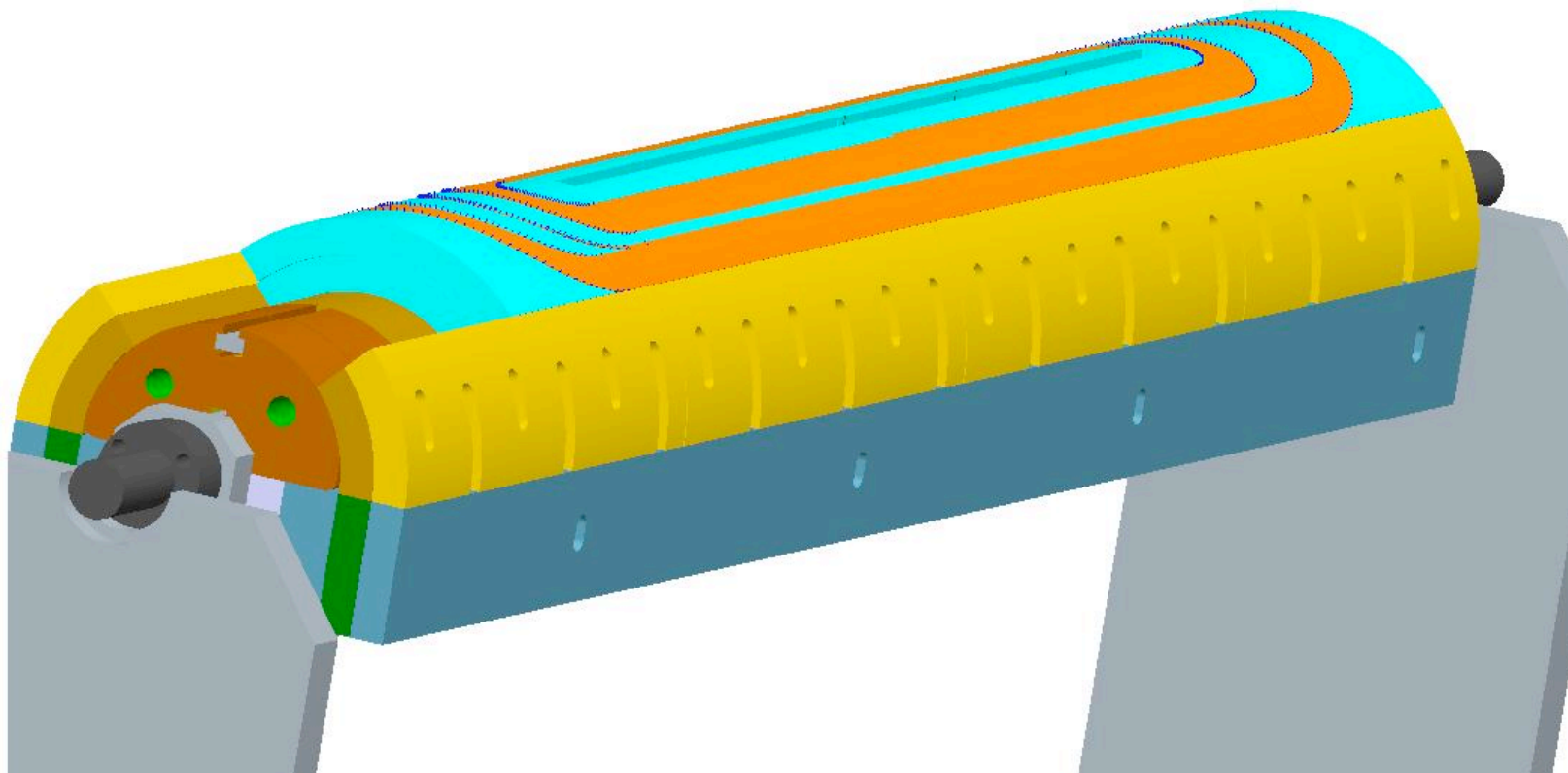
Curing layer 1

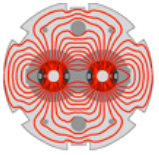




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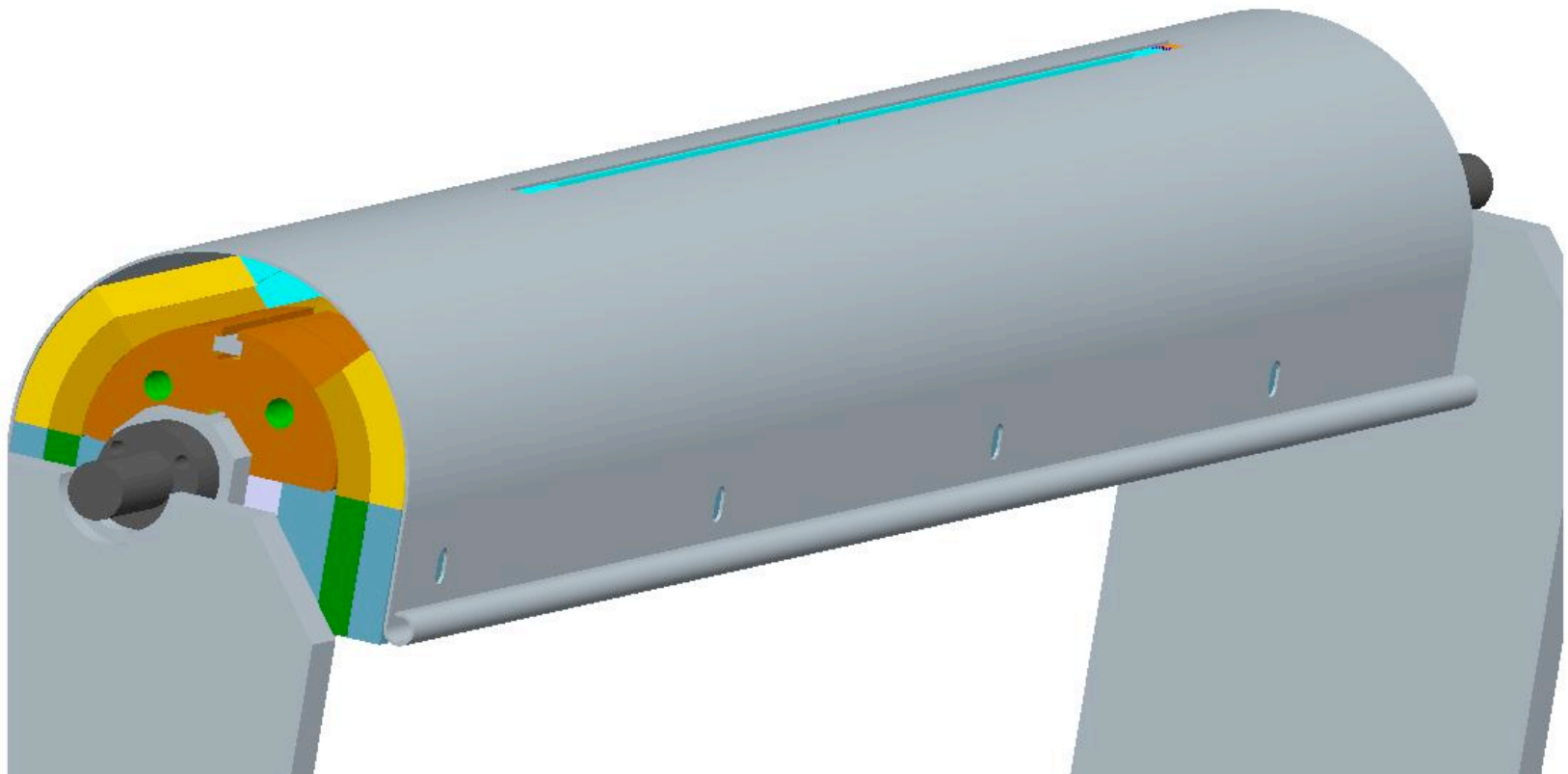
Winding layer 2

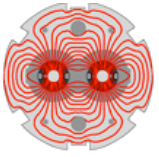




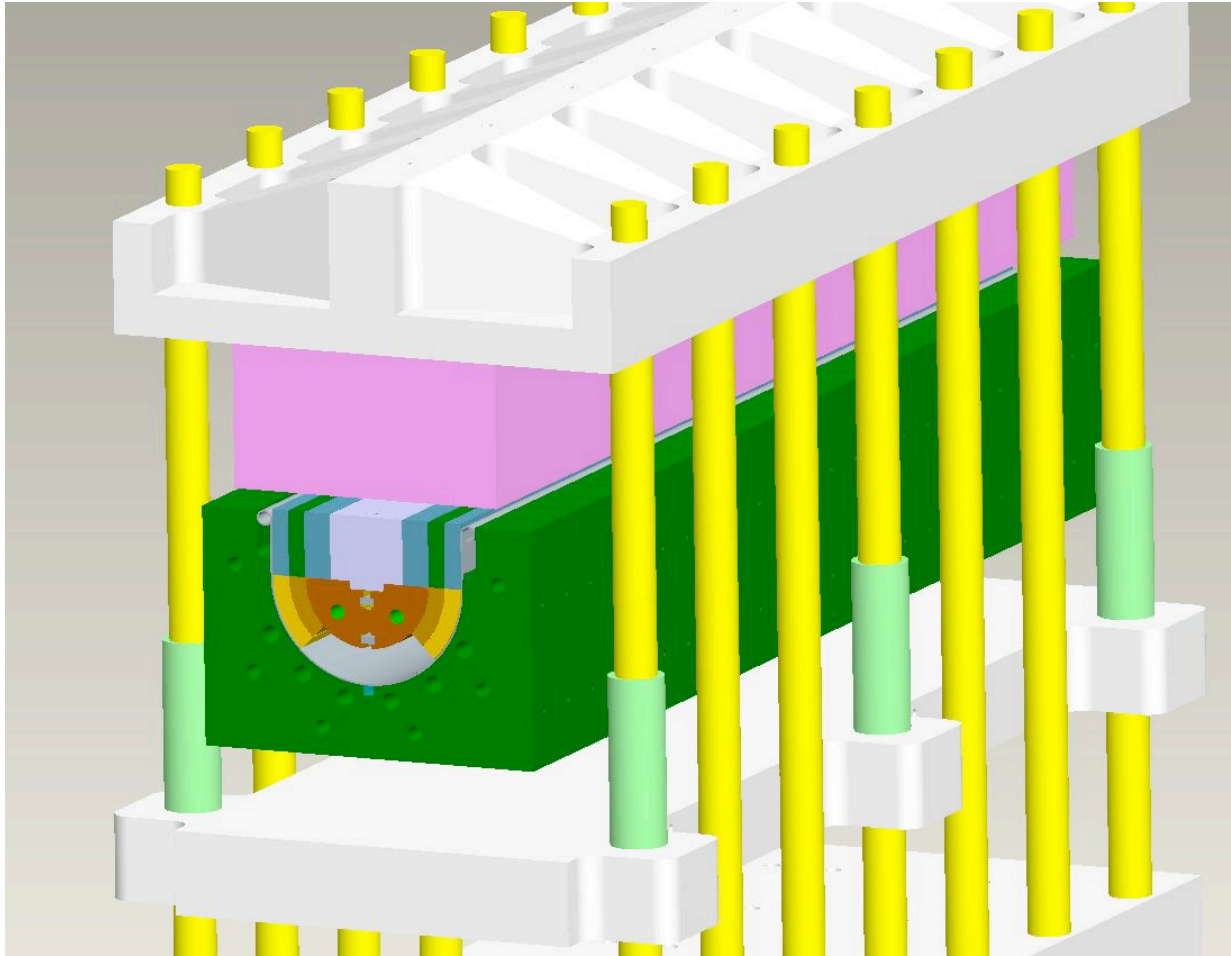
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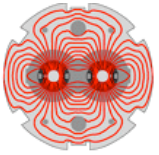
Curing layer 2





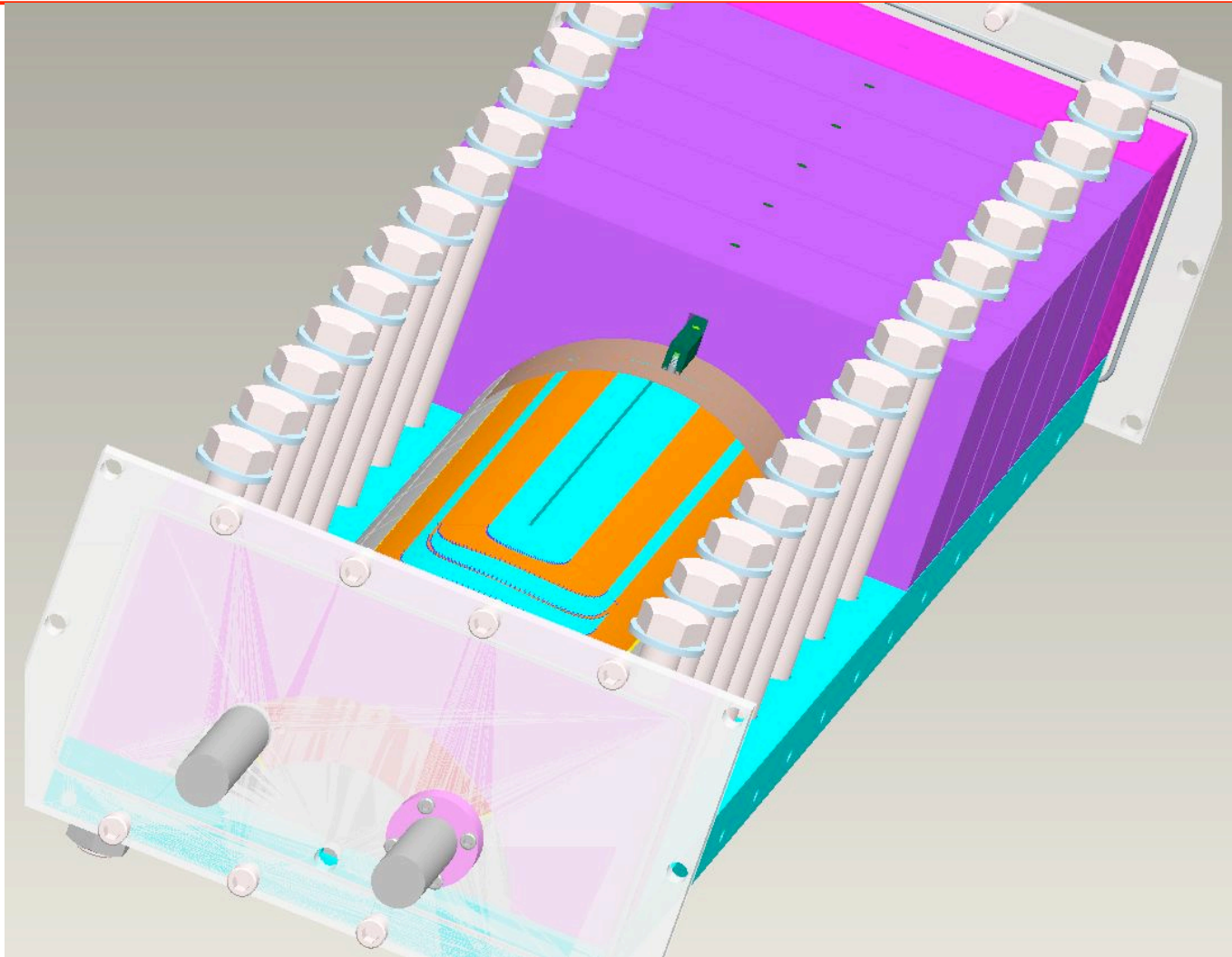
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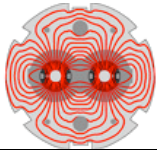




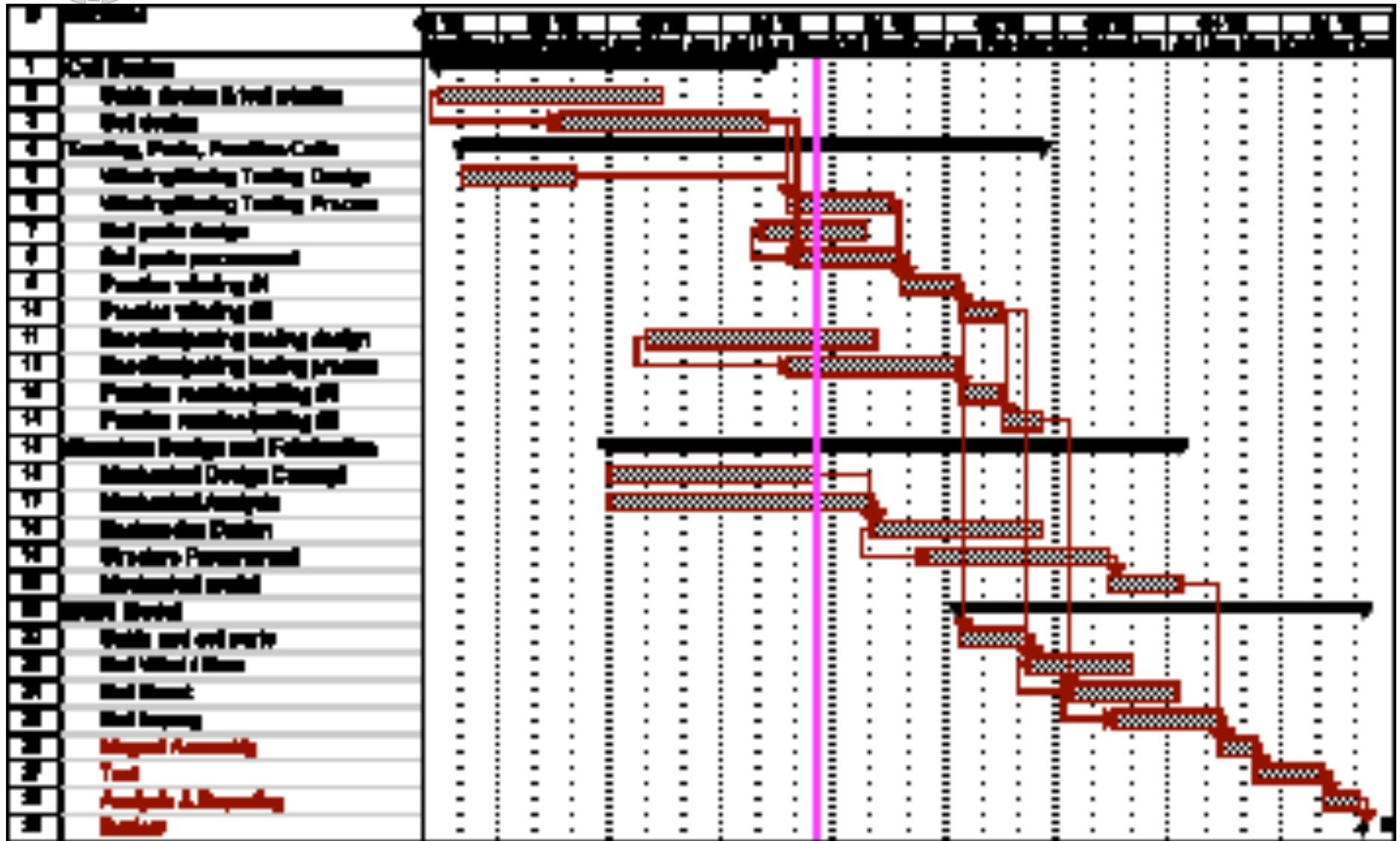
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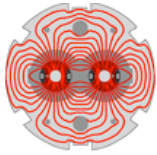
Reaction tooling





HQ Schedule (updated 9/18/08)





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Summary

- We have 90m of cable to wind first practice coil
- Design of coils, spacers, end-shoes, layer-to-layer transition completed.
- Shipment of tooling for winding and curing in the next few weeks
- Reaction and potting tooling in final design stage.
- 3D magnetic design completed.
- 3D analysis of structure and assembly underway.