

# Computational Aerosol Transport

Aerosol Phase Space Tracking to Predict Size-Specific Concentration  
Distribution and Deposition in Space and Time

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# Overview

- Aerosol characterization
- The transport equation
- Simulation of coagulation and deposition
- Simulation of dynamic aerosol transport in confined space + validation of code
- Applications
  - Design of portable wireless aerosol detector
  - Transport in the lung

# Introduction

Definition and Characterization of  
Aerosols

- Definition of Aerosol
  - A colloidal system of fine solid or liquid particles suspended in gas
- Size, Concentration
  - Diameter of particles ranges from  $10^{-9}$  to  $10^{-3}$  m
  - Typical concentration in air is  $10^3$  (clean air) to  $10^5$  (polluted air) [particle/cc]

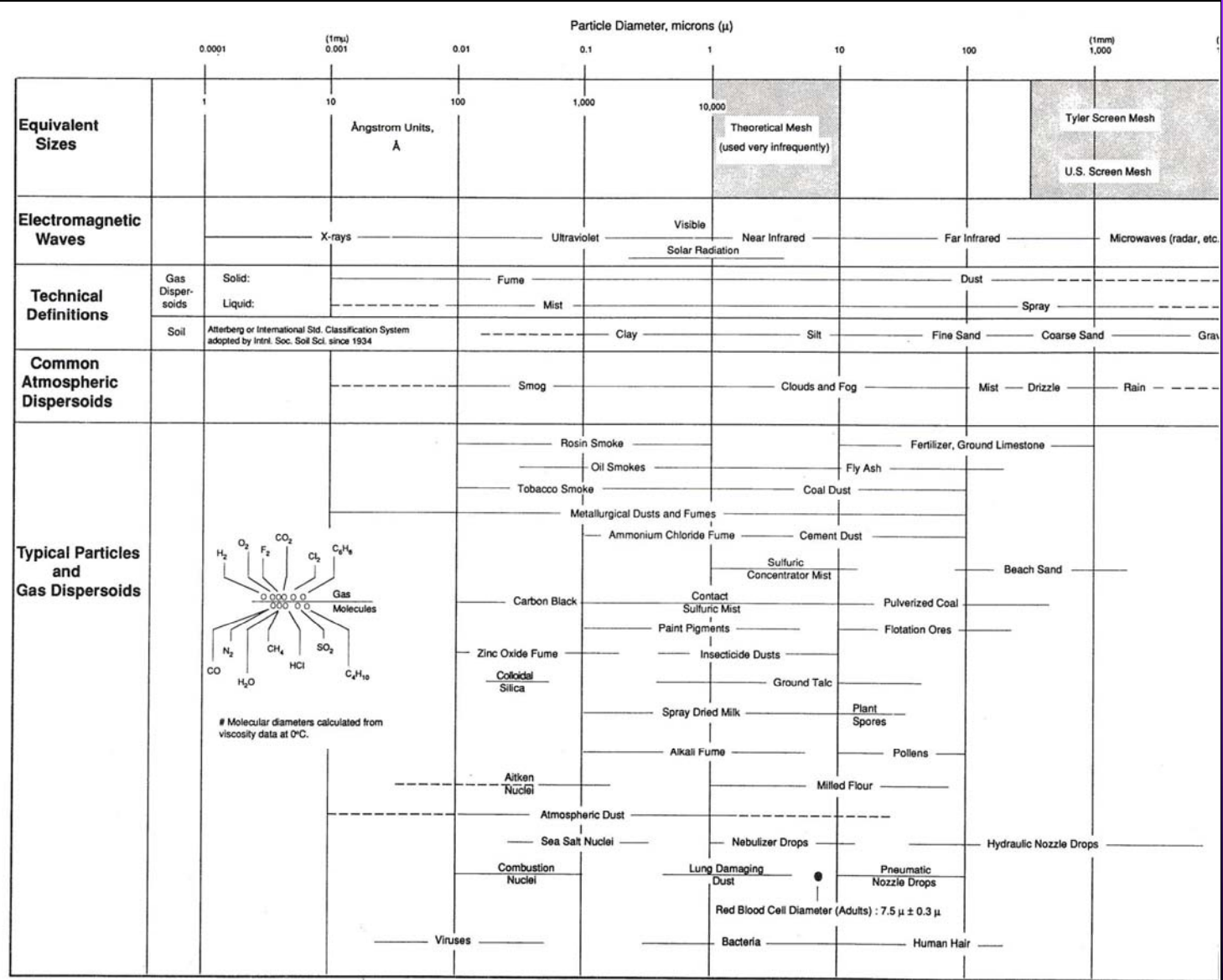
- **Characterization**
  - Volume concentration [ $\mu\text{m}^3/\text{cc}$ ]
  - Mass concentration [ $\mu\text{g}/\text{cc}$ ]
  - Number concentration [particles/cc]
  - Surface concentration [ $\mu\text{m}^2/\text{cc}$ ]
- **Volume distribution as property of interest**
  - Conserved quantities are easier to treat when solving the transport equation
  - But, large variation in magnitude ( $\sim 20$  orders)

# Applications

- Homeland Security
  - NBC aerosol dispersion in confined and open spaces
- Nuclear Safety
  - Understanding aerosol evolution and transport is critical importance in estimating and controlling nuclear accidents.
- Indoor Air Quality
  - Air pollutants such as radon, radon daughter product, volatile organic compounds can easily attach to aerosol particles and inhalation of those may cause significant health hazard.
- Atmospheric Science
  - The formation of fog and cloud, ozone depletion and solar-radiative interactions depend strongly on particulate generation and transport process
- Aerosol Medicine and Toxicology
  - Systemic and local delivery of therapeutic and imaging agents

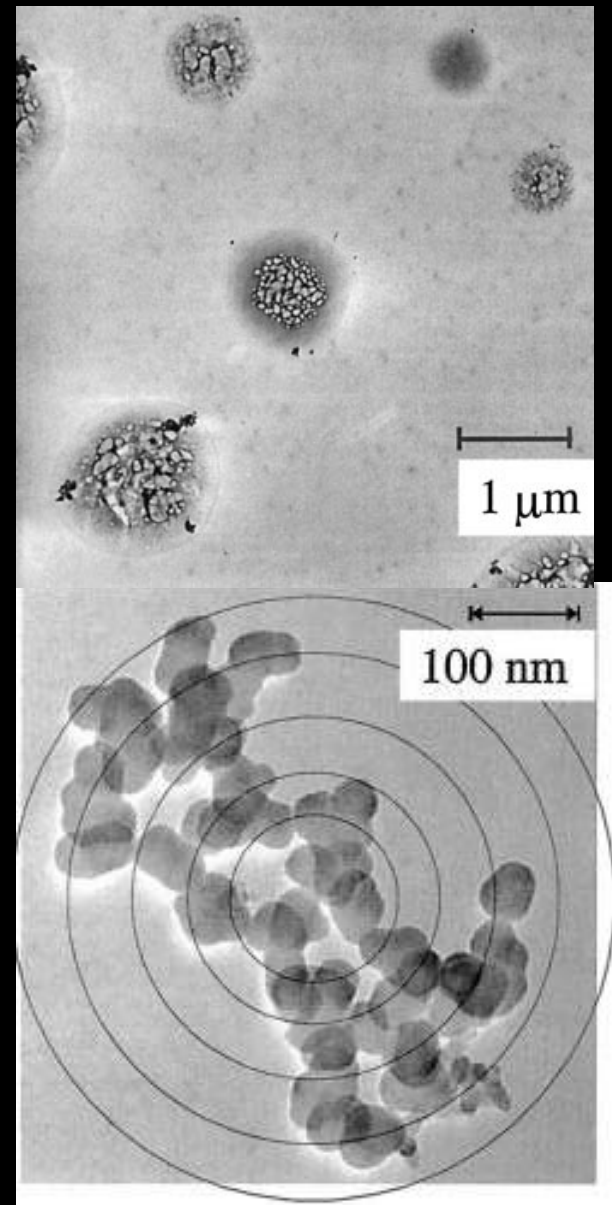
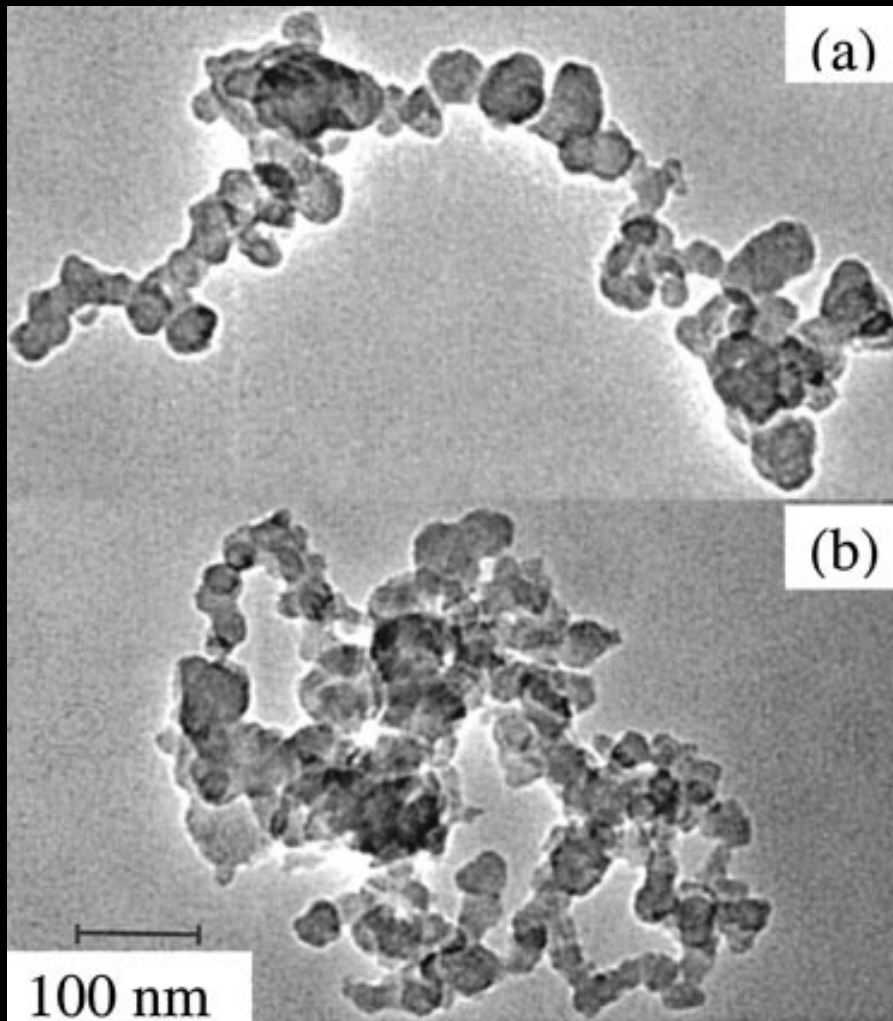
# Introduction

## The Aerosol Size Spectrum



# Particle Morphology

coagulation



Courtesy of C Xiong and SK Friedlander, UCLA



# Transport Phenomena

- Convective transfer
- Diffusion
- Deposition, resuspension
- Thermophoresis
- Electrophoresis
- Sedimentation (gravitational settling)
- Coagulation
- Condensation, evaporation

## Where are We?

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## Problem Statement for Aerosol Transport

- Aerosol spectrum changes *en route*
  - Especially near-field
- Significant aerosol physics far field
  - Phoretic effects, condensation, evaporation, gravitational settling, deposition, etc.
- Intricate thermal-hydraulics
- Low air velocities but high gradients
- No current comp. model considers all

# Current Aerosol Models

- Confined spaces
  - CONTAM / COMIS: simple mass balance with well-mixed hypothesis, no aerosol dynamics.
  - MAEROS: coagulation with geometric constraint, homogeneous turbulence, no transport.
- Outdoors
  - HPAC: size specific deposition and removal but no dynamics. Deposition via dep. velocities.
- Dummy particles in all computational models except for MAEROS

# Objective

- Develop a comprehensive computational tool to predict the aerosol phase space  $n(v,r,t)$  using full physics
  - Based on first principles – Boltzmann Eq.
  - Coagulation treatment using sectional approach
  - Deposition handled via boundary layer theory
  - Convective and diffusive transport
  - Thermophoresis, electrophoresis
  - Condensation and evaporation
  - Confined or open atmospheres w/ obstructions
  - Time dependent source term, including  $\delta(t-t_0)$

# Aerosol Transport Equation

Distribution Function and Method of  
Solving the Transport Equation

# Aerosol characterization

- Differential property:  $q(v, t) = \alpha v^\gamma n(v, t)$ 
  - Volume concentration  $[(\mu\text{m})^3/\text{cc}]$
  - Mass concentration  $[\mu\text{g}/\text{cc}]$
  - Number concentration  $[\text{particles}/\text{cc}]$
- Integral property:  $Q(t) = \int_0^\infty q(v, t) dv$
- Number concentration is not conserved

# Aerosol Distribution Function

- Log-Normal Distribution Function

$$n(d) = \frac{N}{\sqrt{2\pi} \ln(\sigma_g) d} \exp \left[ \frac{[\ln(d) - \ln(d_g)]^2}{2[\ln(\sigma_g)]^2} \right]$$

$n(d)$  = number of particle per unit volume  
at particle diameter  $d$ ;

$N$  = total number of particles;

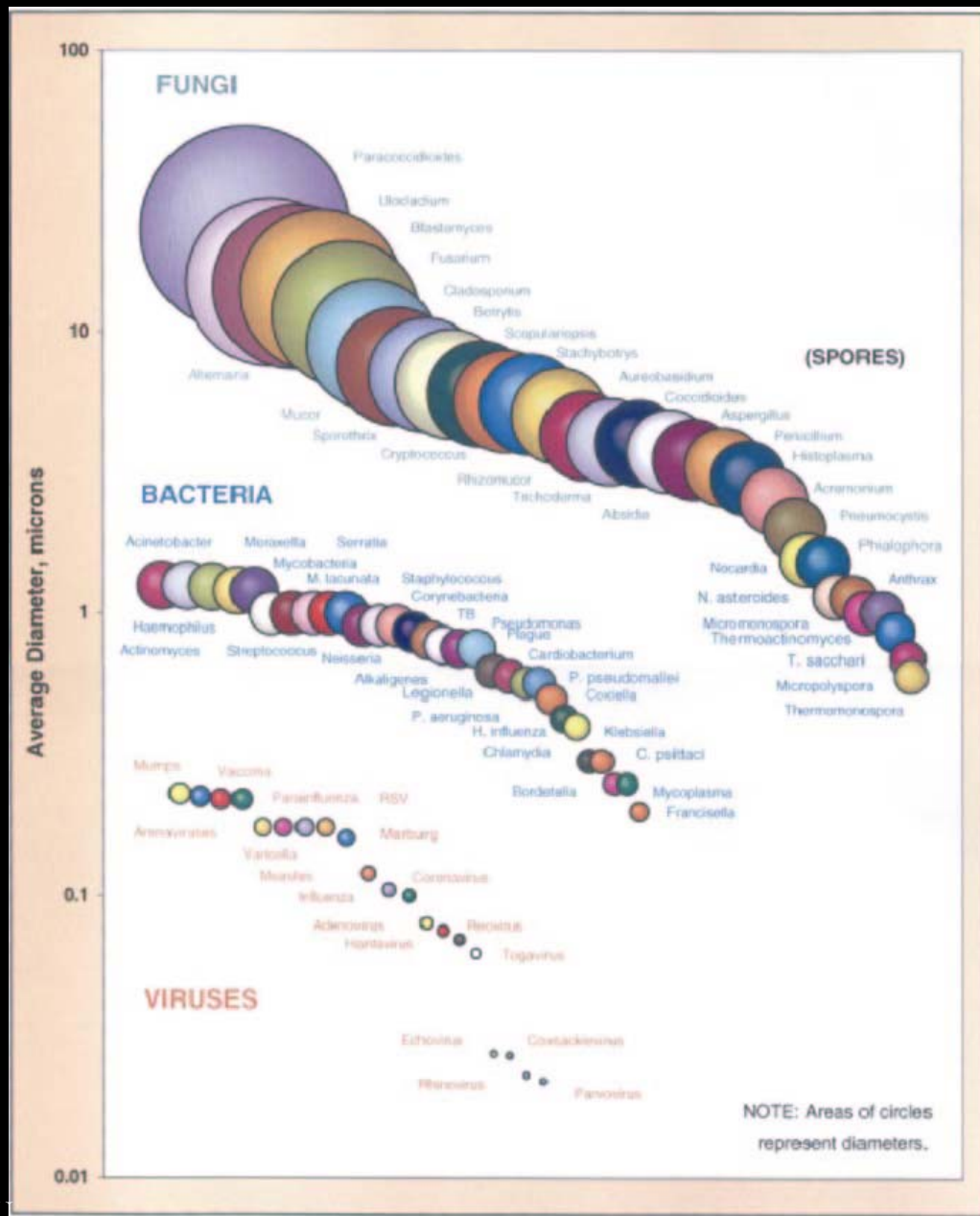
$d_g$  = median diameter of aerosol;

$\sigma_g$  = geometric standard deviation.



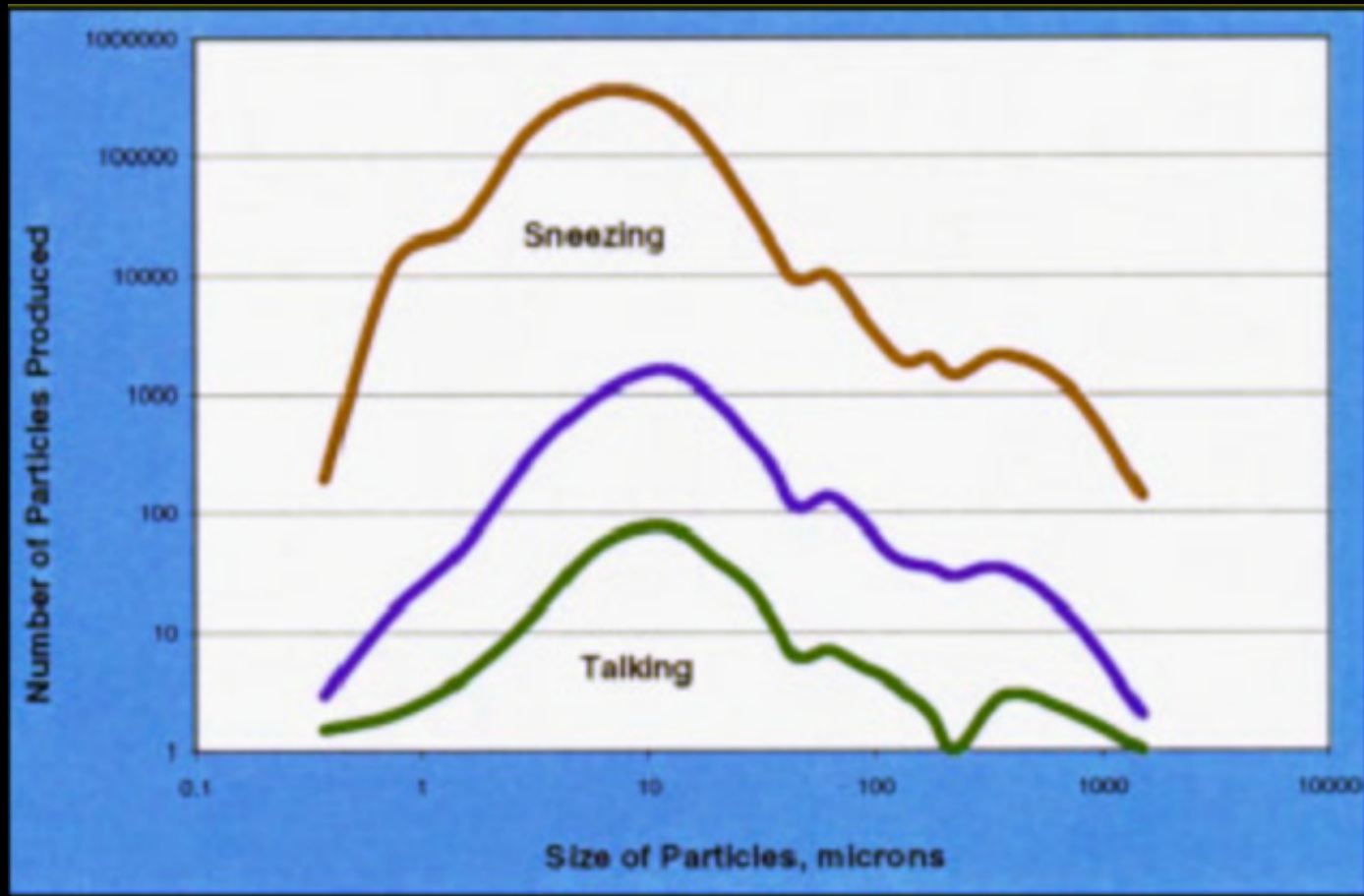
# Bio-aerosols and Microbes

- Anthrax: 1.0  $\mu$
- Corona virus: 0.1  $\mu$
- Narrow distribution
  - $\sigma_g = 1.02$  to 1.05



Courtesy of WJ Kowalski and W Bahnfleth, Penn State U.

# Respiratory Aerosol Generation



Courtesy of WJ Kowalski and W Bahnfleth, Penn State U.

# Aerosol Transport Equation

$$\frac{\partial q(v, \vec{r}, t)}{\partial t} + \nabla \cdot [\vec{U}(v, \vec{r}, t)q(v, \vec{r}, t)] - \nabla \cdot [D(v, \vec{r}, t)\nabla q(v, \vec{r}, t)] + \frac{\partial}{\partial v} [I(v, \vec{r}, t)q(v, \vec{r}, t)] = S(v, \vec{r}, t) + \left( \frac{\partial q(v, \vec{r}, t)}{\partial t} \right)_{coag}$$

$U$  = velocity of aerosol

$D$  = diffusion coefficient

$I$  = rate of growth due to condensation and evaporation

$S$  = independent source term

# Method of Solution

- Treat coagulation using the sectional method; Coagulation appears as source.
- Solve coagulation under uniform mixing first.
- Reduce compartment size.
- Add convective transfer, sweep the domain
- Add phoretic effects, deposition, etc.
- Assumption: No slip in the convective term
- Neglected in this version:
  - Condensation & evaporation
  - Diffusion when convective velocity is large

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# Coagulation

- Binary collision or many-body problem?
  - [morphology](#)
- Non-linear Integro-differential equation

$$\left(\frac{\partial n(v,t)}{\partial t}\right)_{coag} = \frac{1}{2} \int_0^v du K(u, v-u) n(u,t) n(v-u,t) - n(v,t) \int_0^\infty du K(u, v) n(u,t)$$

$K(u,v)$  = coagulation kernel. Represents the physical process of collision between two particles. Typical processes leading to coagulation are e.g., Brownian motion, gravitational settling, and turbulence.

Source term in the [Transport Equation](#)

# Some Coagulation Kernels:

## Brownian coagulation

$$K_B(u, v) = \frac{2kT}{3\mu} \left( 2 + \left( \frac{u}{v} \right)^{1/3} + \left( \frac{v}{u} \right)^{1/3} \right)$$

$k$  = Boltzmann's constant

$T$  = temperature of surrounding fluid

$\mu$  = fluid dynamic viscosity

$u$  and  $v$  are volumes of particles

## Gravitational coagulation

$$K_G(u, v) = \frac{\rho g}{6\mu} \left( \frac{3}{4\pi} \right)^{1/3} (v^{2/3} + u^{2/3}) \left| v^{2/3} C_v - u^{2/3} C_u \right|$$

$\rho$  = density of particle

$g$  = gravitational acceleration

$C_v$  and  $C_u$  are Cunningham coefficients for slip correction

# Kernels in transition flow regimes:

- Rapidly becoming intractable
- Combined Brownian and Gravitational kernel:

$$\frac{K_{BG}(u,v)}{K_B(u,v) + K_G(u,v)} = \frac{4\pi}{\beta(\beta + 4)} \sum_{n=0}^{\infty} (2n + 1) \frac{I_{n+\frac{1}{2}}\left(\frac{\beta}{2}\right)}{K_{n+\frac{1}{2}}\left(\frac{\beta}{2}\right)}$$

$$\beta \propto uv|u^2 - v^2|, \quad \beta \in (0, \gg 1)$$



# Discrete Coagulation Equation

- Integral quantity of aerosol property in section  $l$

$$Q_l = \int_{v_{l-1}}^{v_l} q(v, t) dv$$

- Discrete coagulation equation

$$\frac{\partial Q_l}{\partial t} = \frac{1}{2} \sum_{i=1}^{l-1} \sum_{j=1}^{l-1} \beta_{i,j,l} Q_i Q_j - Q_l \sum_{i=1}^{l-1} \beta_{i,l} Q_i - \frac{1}{2} \beta_{l,l} Q_l^2 - Q_l \sum_{i=l+1}^m \beta_{i,l} Q_i$$

# Sectional coagulation coefficients

Symbol	Condition	Sectional coefficient
${}^1\beta_{i,j,l}$	$2 \text{---} l \text{---} m$ $1 \text{---} i < l$ $1 \text{---} j < l$ ${}^1\beta_{i,j,l} = {}^1\beta_{j,i,l}$	$\int_{v_{i-1}}^{v_i} \int_{v_{j-1}}^{v_j} \frac{\theta(v_{l-1} < u + v < v_l)(u + v)K(u, v)}{uv(v_i - v_{i-1})(v_j - v_{j-1})} dudv$
${}^2\beta_{i,l}$	$2 \text{---} l \text{---} m$ $i < l$ ${}^2\beta_{i,l} \textcircled{=} {}^2\beta_{l,i}$	$\int_{v_{i-1}}^{v_i} \int_{v_{l-1}}^{v_l} \frac{[\theta(u + v > v_l)u - \theta(u + v < v_l)v]K(u, v)}{uv(v_i - v_{i-1})(v_l - v_{l-1})} dudv$
${}^3\beta_{l,l}$	$1 \text{---} l \text{---} m$	$\int_{v_{l-1}}^{v_l} \int_{v_{l-1}}^{v_l} \frac{\theta(u + v > v_l)uK(u, v)}{uv(v_l - v_{l-1})^2} dudv$
${}^4\beta_{i,l}$	$1 \text{---} l < m$ $i > l$ ${}^4\beta_{i,l} \textcircled{=} {}^4\beta_{l,i}$	$\int_{v_{i-1}}^{v_i} \int_{v_{l-1}}^{v_l} \frac{uK(u, v)}{uv(v_i - v_{i-1})(v_l - v_{l-1})} dudv$

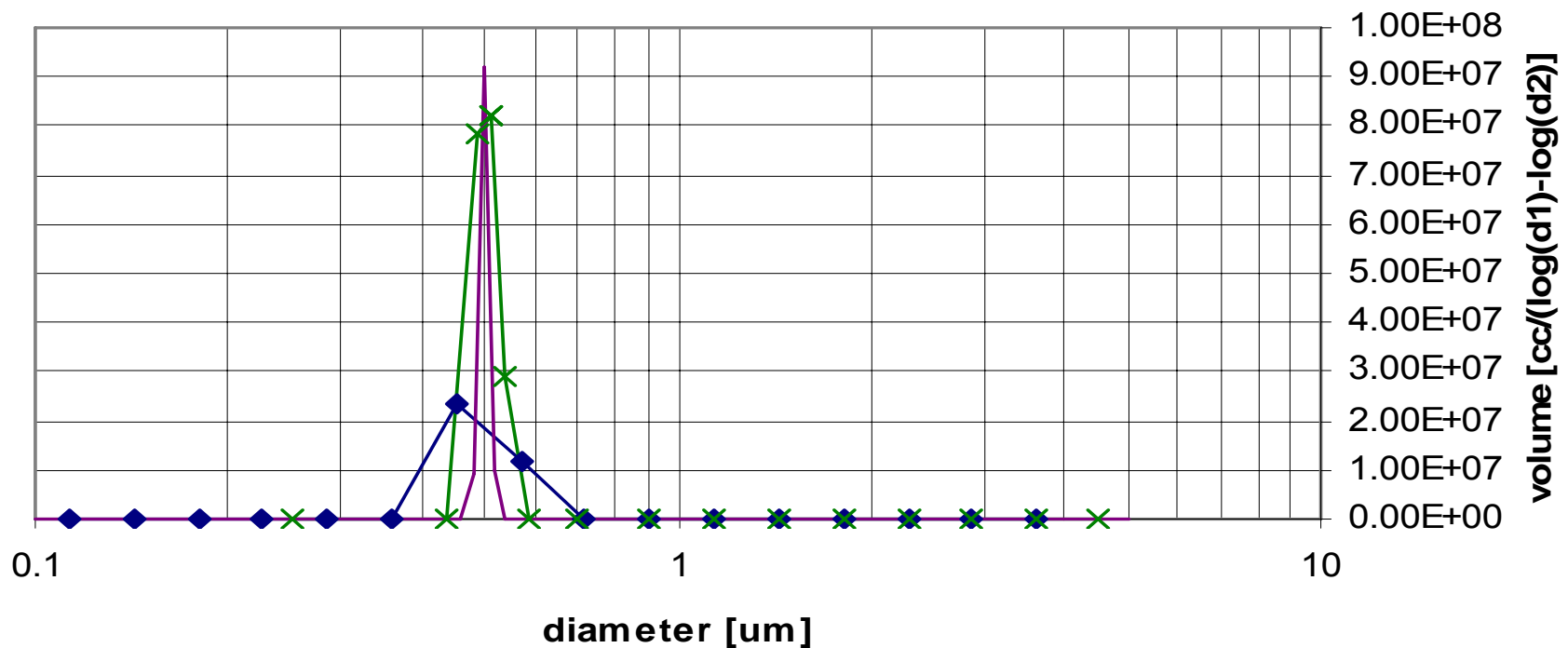
# Simulation of coagulation and deposition

- Coagulation: sectional representation
  - Logarithmic groups (geometric constraint)

$$v_l \geq 2 v_{l-1}$$

- Advantage:
  - Flux into group  $l$  is possible only from group  $l-1$ . This reduces the computational cost of  $\beta_{i,j,l}$
- Disadvantage:
  - It is not possible to resolve narrow distributions predominant for bio and therapeutic aerosols
- SAEROSA: Arbitrary sectionalization

# Fit of a Narrow Distribution IC



—◆— initial distribution with geometric constraint —×— initial distribution with arbitrary groups  
— analytical distribution

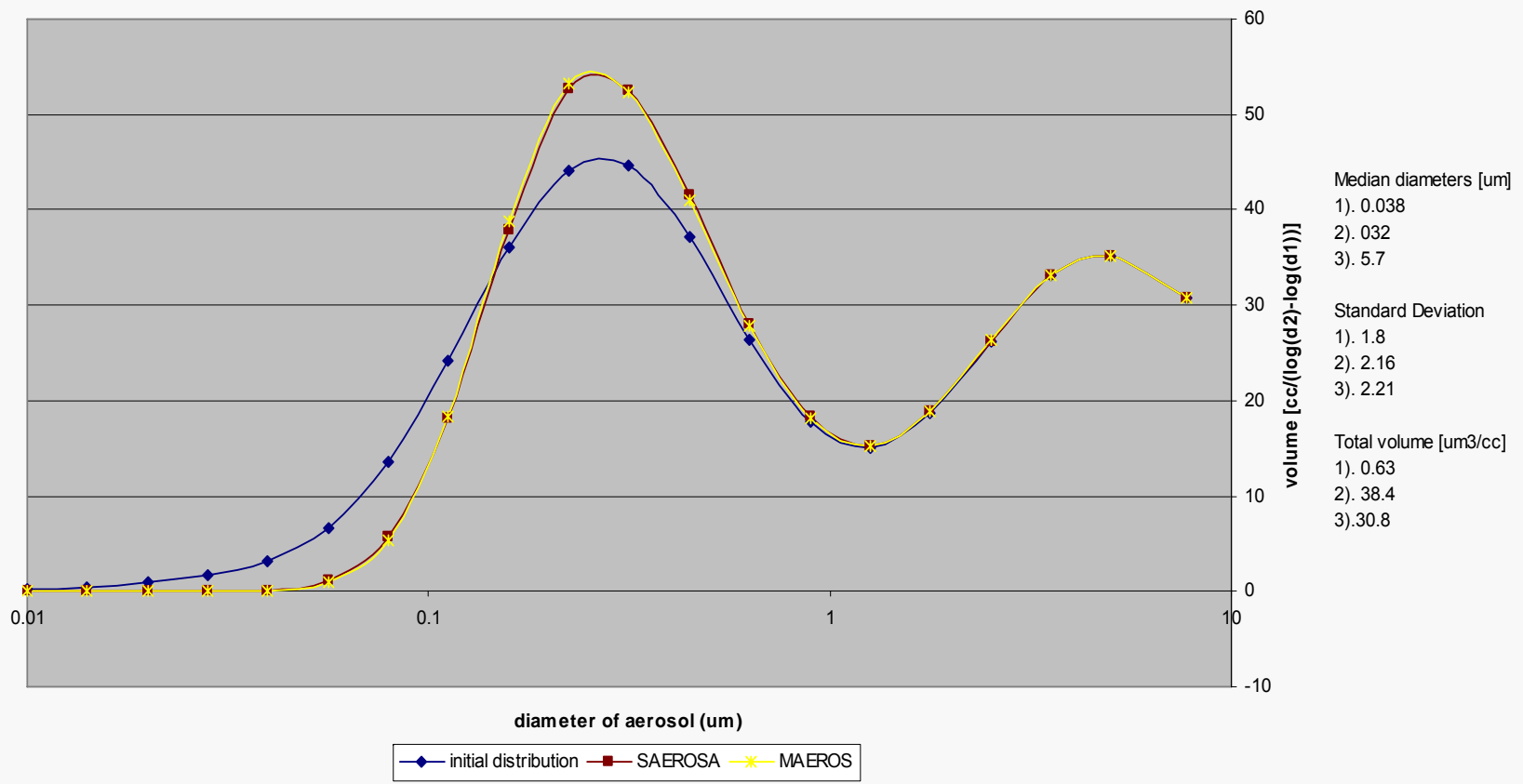
# Model Comparison

Name		SAEROSA	MAEROS
Capability	Coagulation	YES	YES
	Deposition	YES	YES
	Condensation	NO	YES
	Species	Single	Multi-species
Group structure	Sectional Method	Arbitrary	Geometric Constraint
	Maximum Groups	Unlimited	20 groups
Kernel treatment		True kernels	Sum kernels
Numerical scheme		R-K, 5-6 <sup>th</sup> Adaptive $\Delta t$	R-K, 4-5 <sup>th</sup>
Computational time	(for 24hr simulation with 20 groups)	~1 min	~1 min

# Coagulation Benchmark 1

without deposition

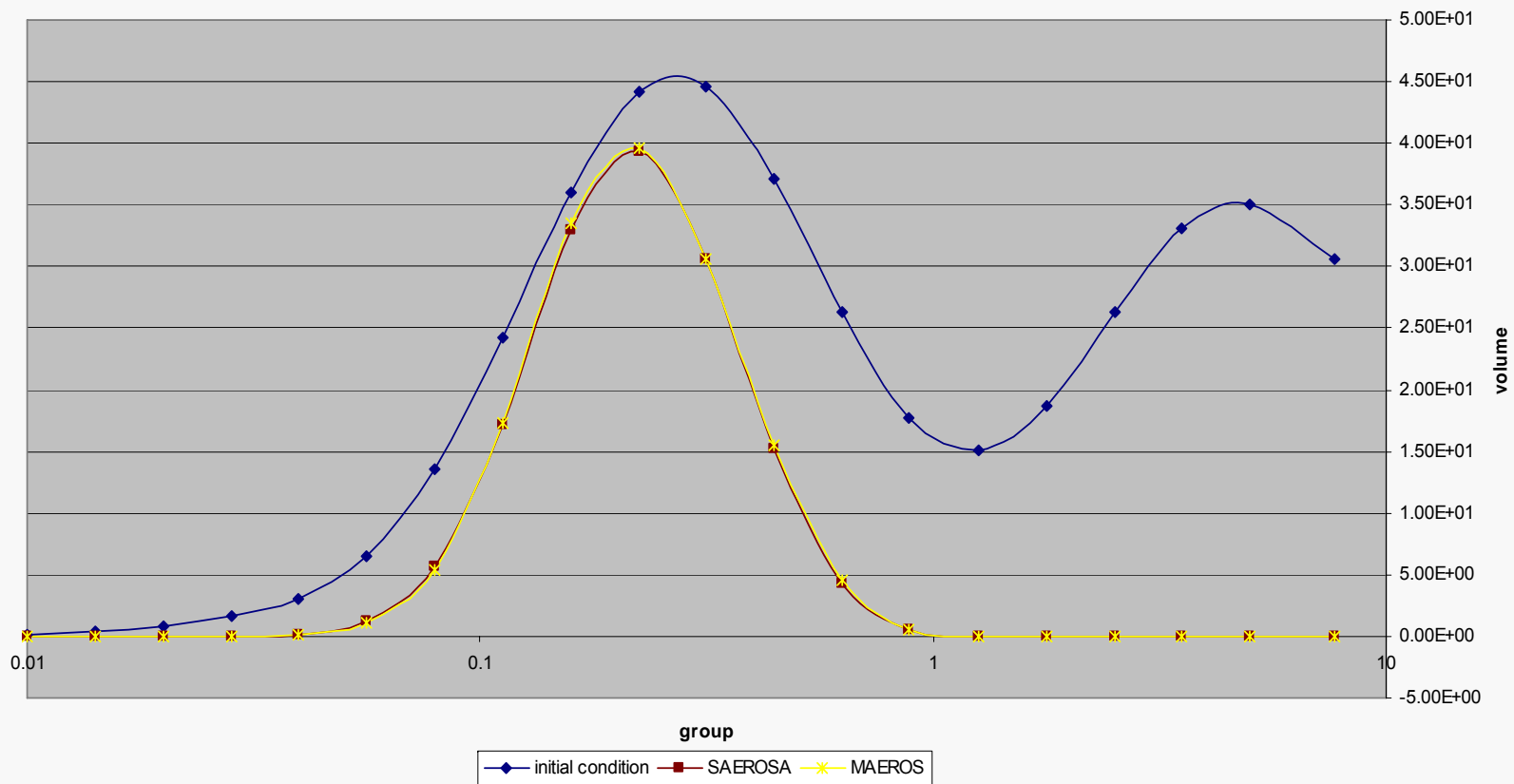
Simulation of atmospheric aerosol coagulation over 24 hrs



# Coagulation Benchmark 2

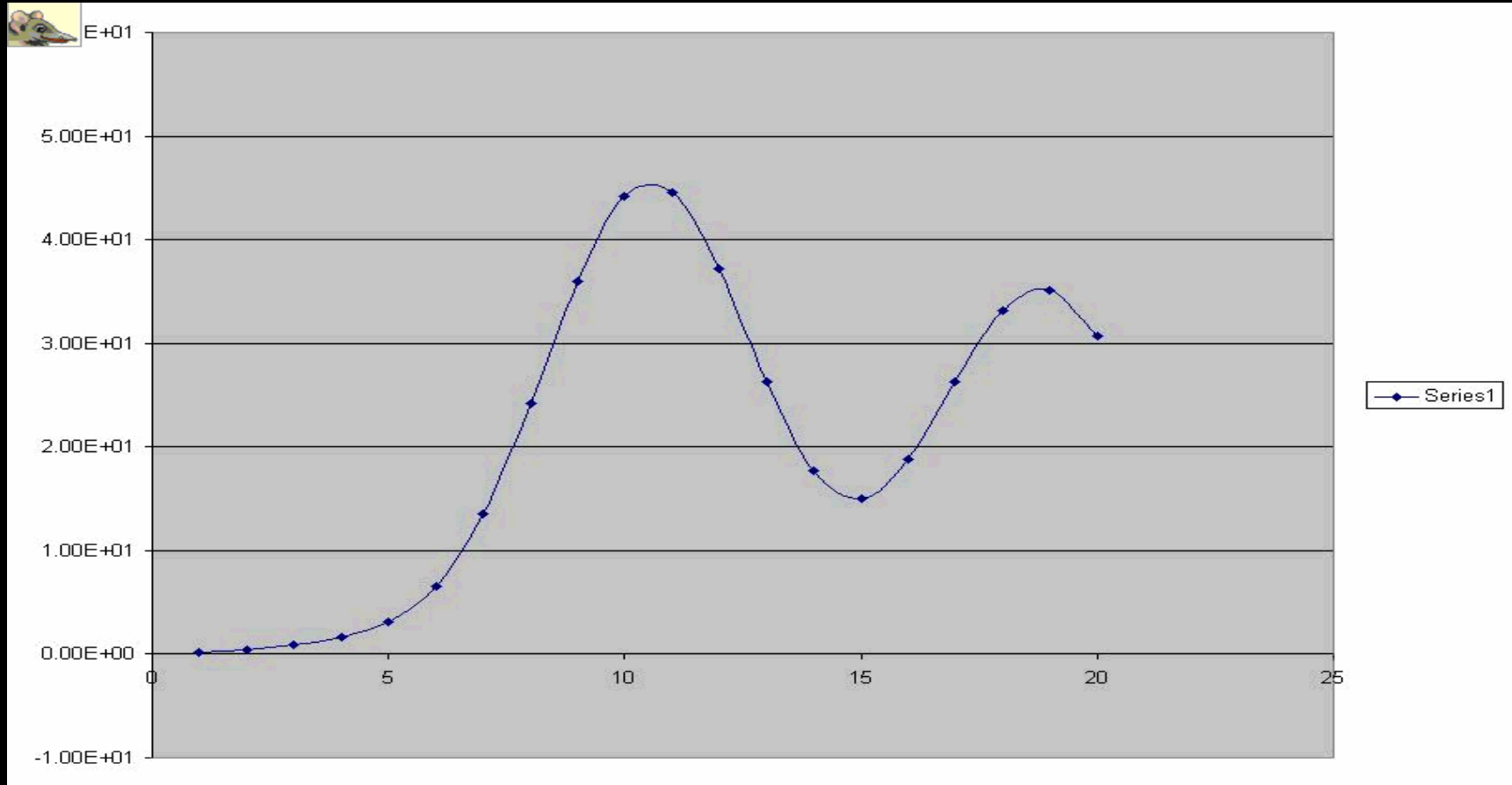
with deposition

coagulation+deposition of atmospheric aerosol



# Visualizing the Time Evolution

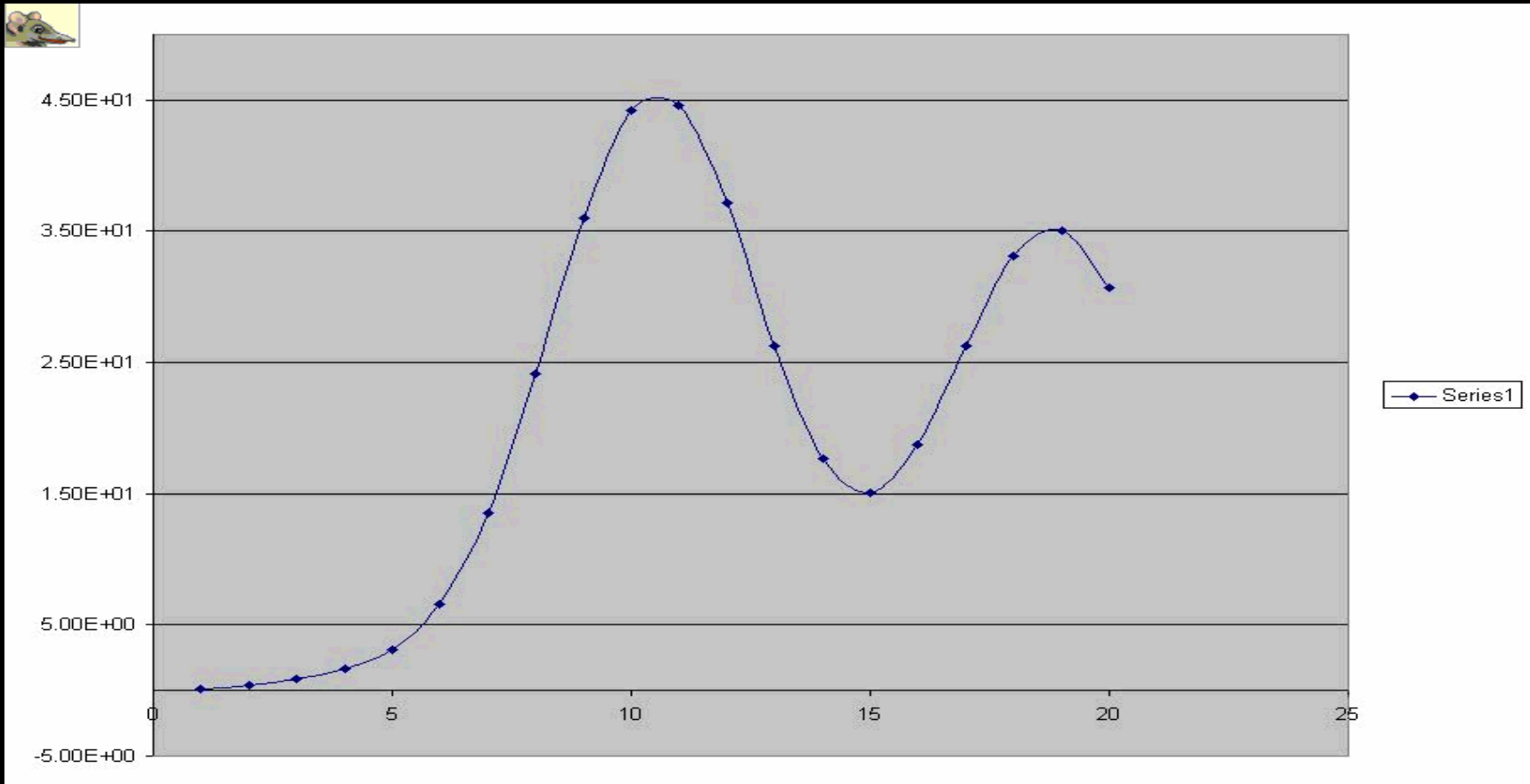
## Coagulation





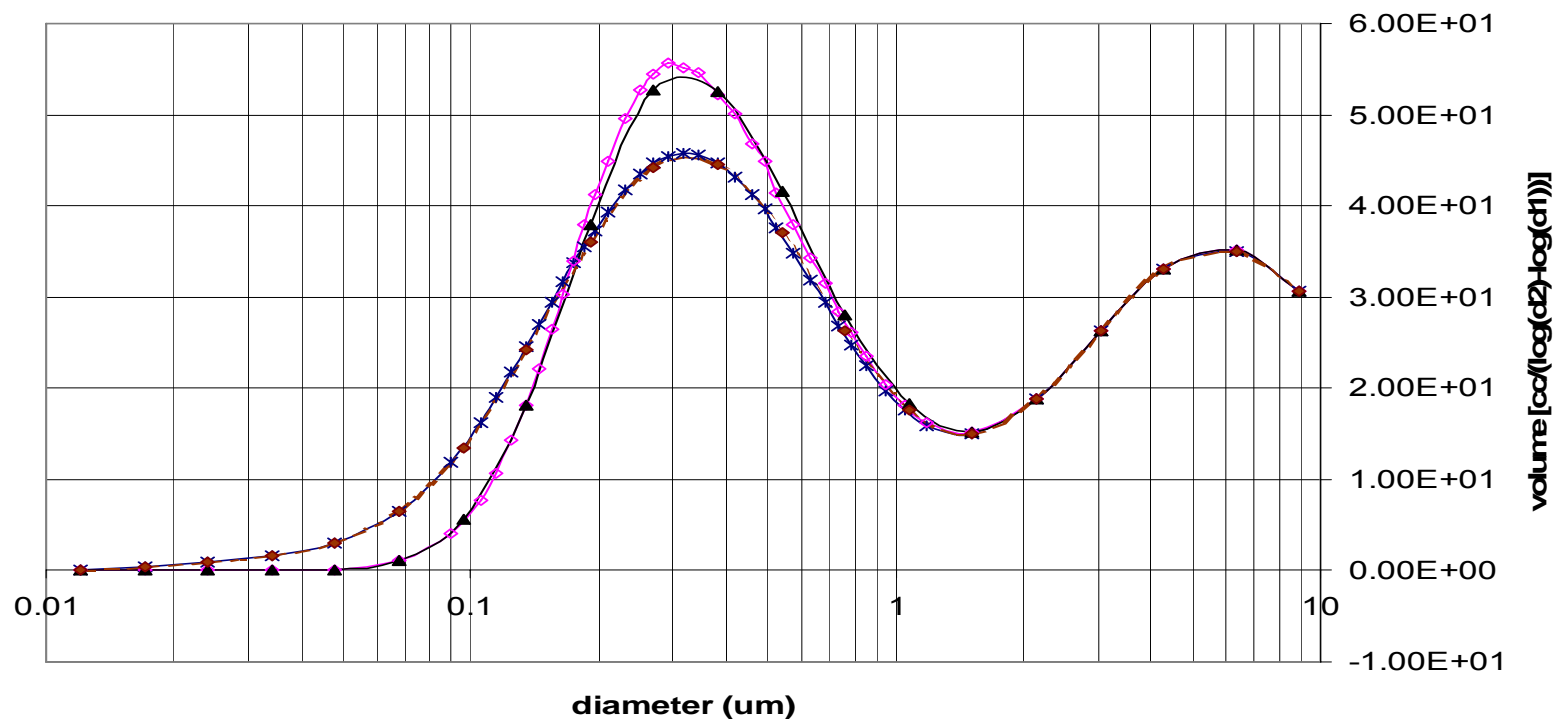
# Visualizing Time Evolution (cont.)

## Coagulation + Deposition



# Effect of arbitrary sections

On urban aerosol, without deposition

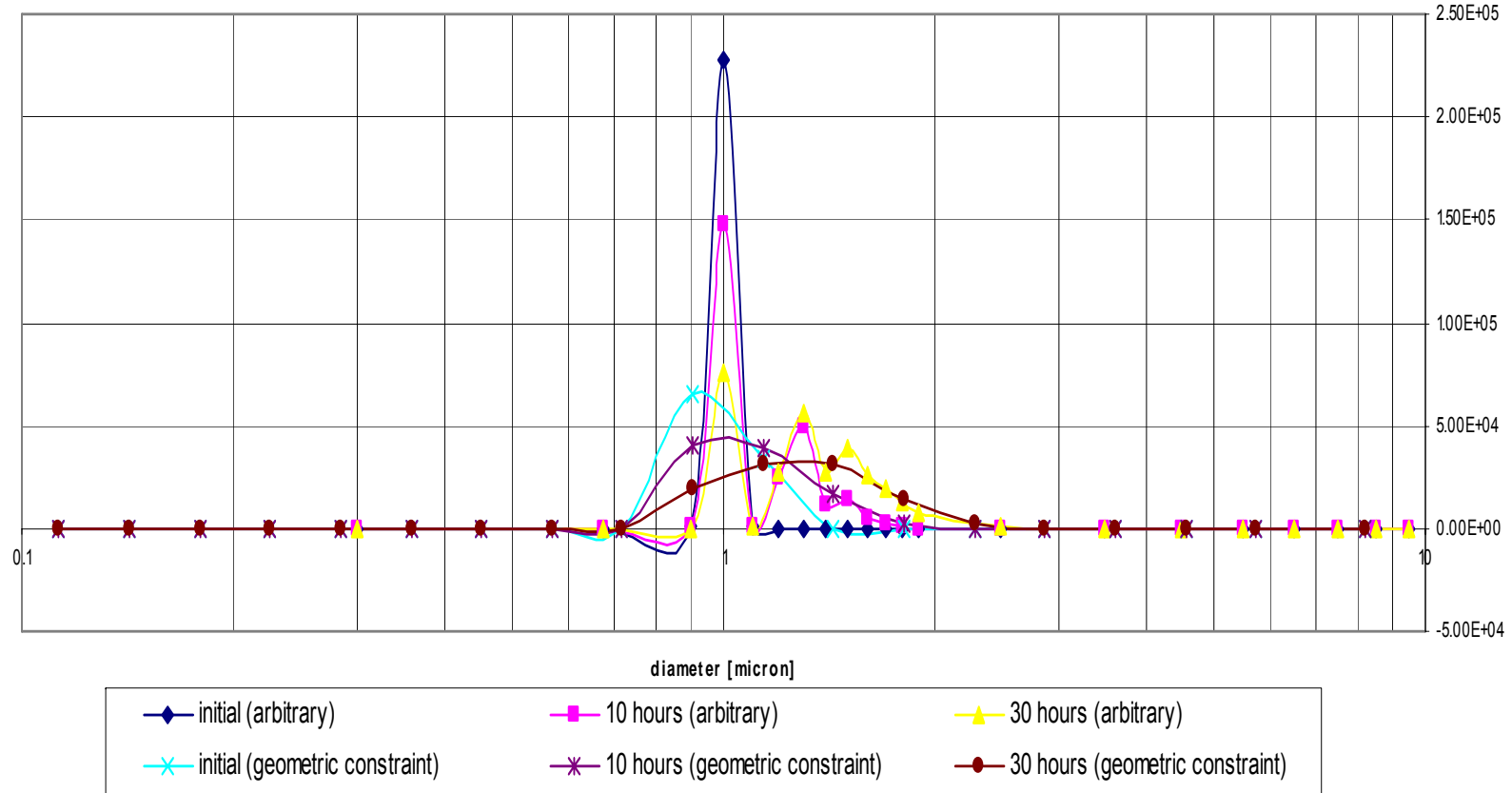


—\*— initial distribution with no geometric constraint(44 groups) —◇— 24hr no geometric constraint (44groups)  
—▲— 24hr with geometric constraint (20groups) —◆— initial distribution with geometric constraint(20groups)

# Effect of arbitrary sections

On near delta function source

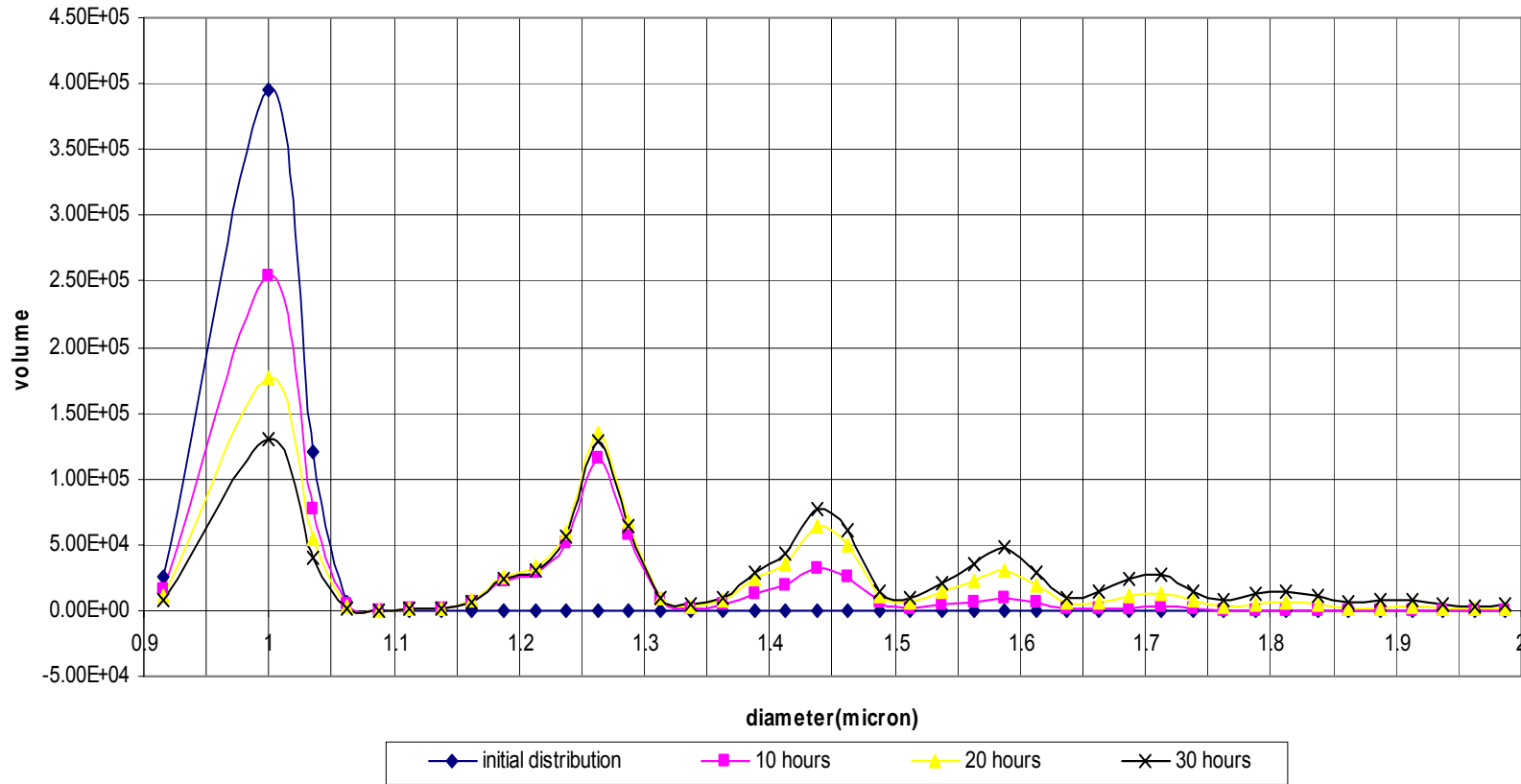
Coagulation of narrow monodisperse particles with  $\text{stdv}=1.02$  at 1micron,  $v=1.0e-8$  cc



# Ultra-fine group structure

Near delta function source

Coagulation of mono disperse particles using ultrafine group structure



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# Aerosol transport in confined spaces

## The CAEROT code

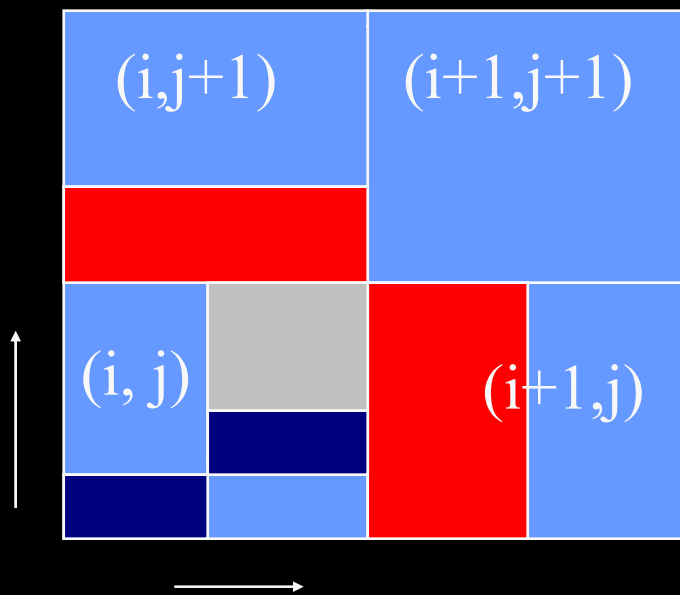
- Inclusion of convective transport and geometry into SAEROSA
  - Spatial discretization
  - Production of velocity field by using external CFD code
  - Advanced nodal method using hybrid Eulerian-Lagrangian treatment
- Time & space-dependent source and sink
- Code validation against experiments

# Advanced Nodal Method

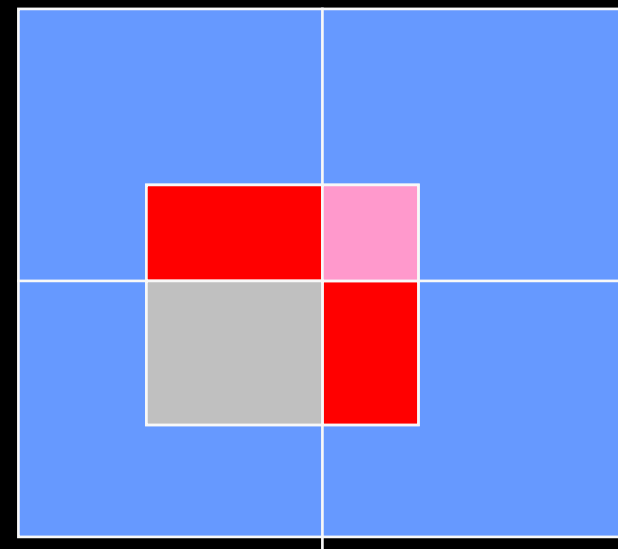
Hybrid Eulerian-Lagrangian

- In 2D case
  - Transport from  $(i,j)$  to  $(i+1,j+1)$  along stream lines
  - Less diffusive, faster convergence

Finite difference

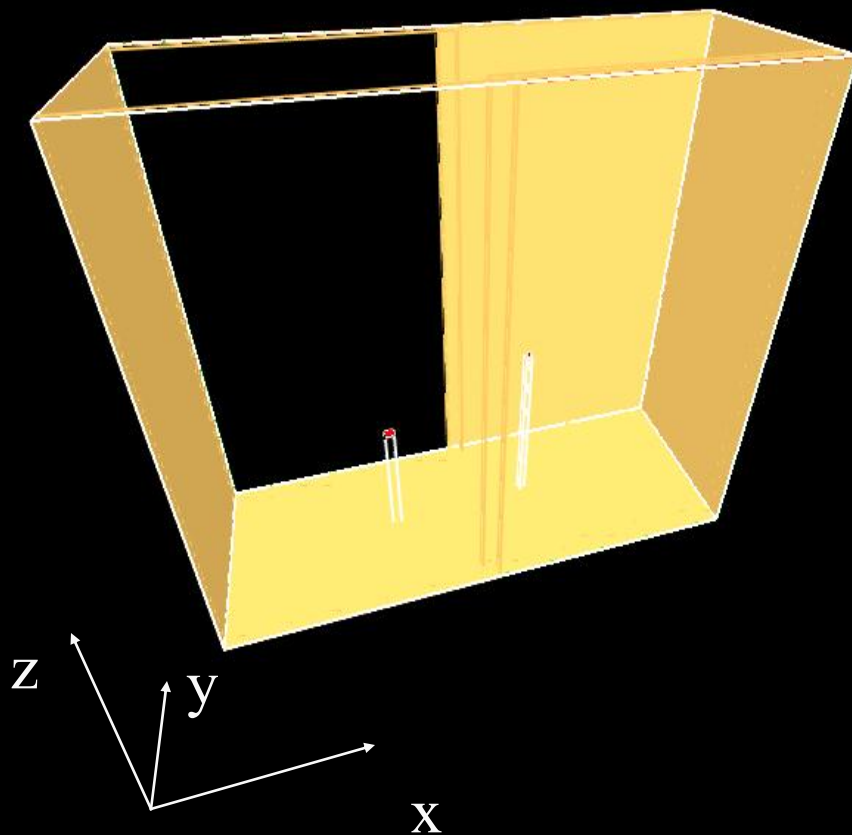


Stream tube model



# Validation Experiments in an Environment Chamber

NIST Smokeview 3.0 Nov 18 2002

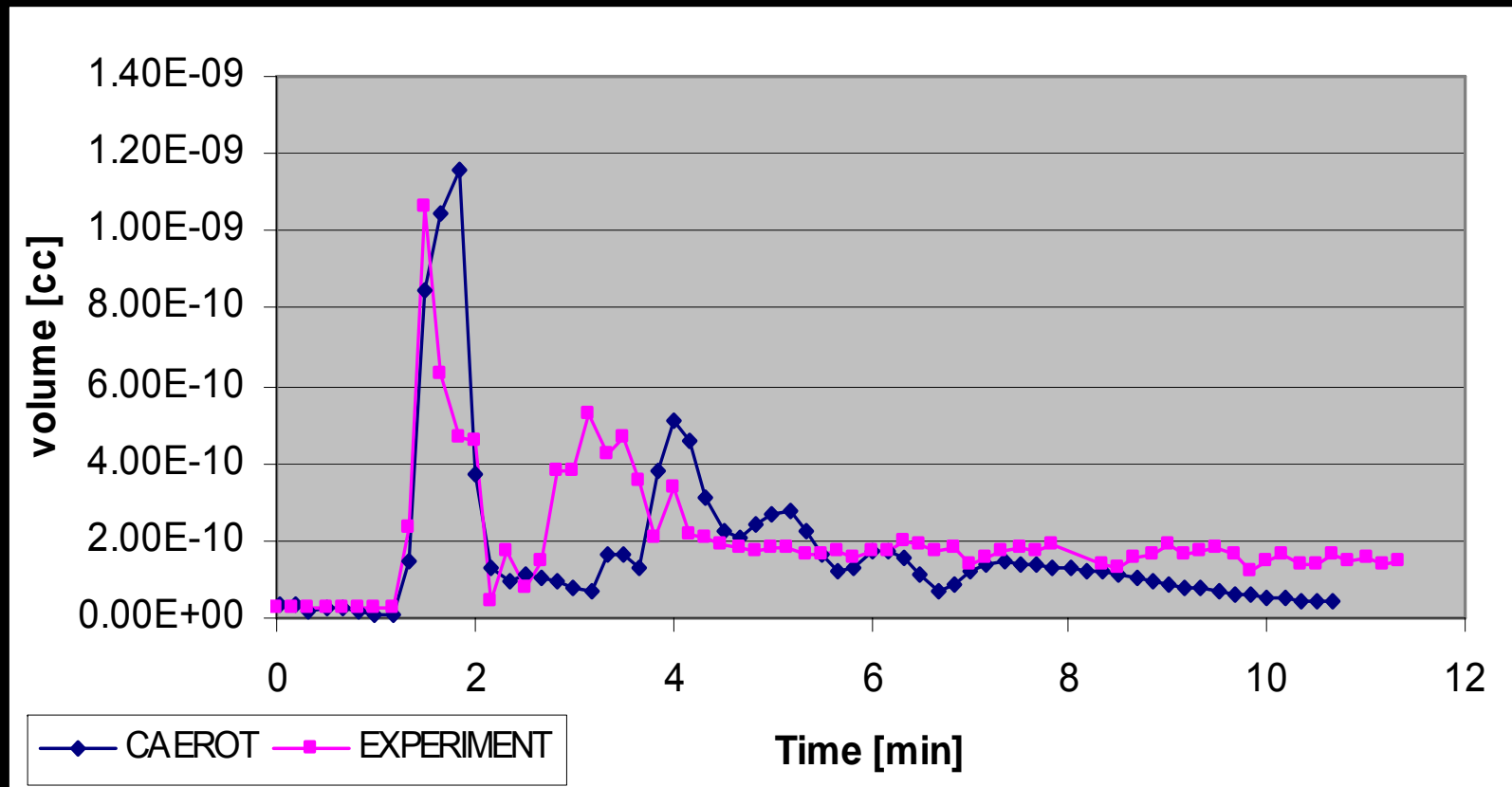


- Size: 180x60x150 cm
- Variable release and sampling locations
- Antistatic tubing
- Release via nebulizer
- NIST traceable particle standard:  $0.502 \mu$
- Multi-channel laser aerosol spectrometer



# Code Validation

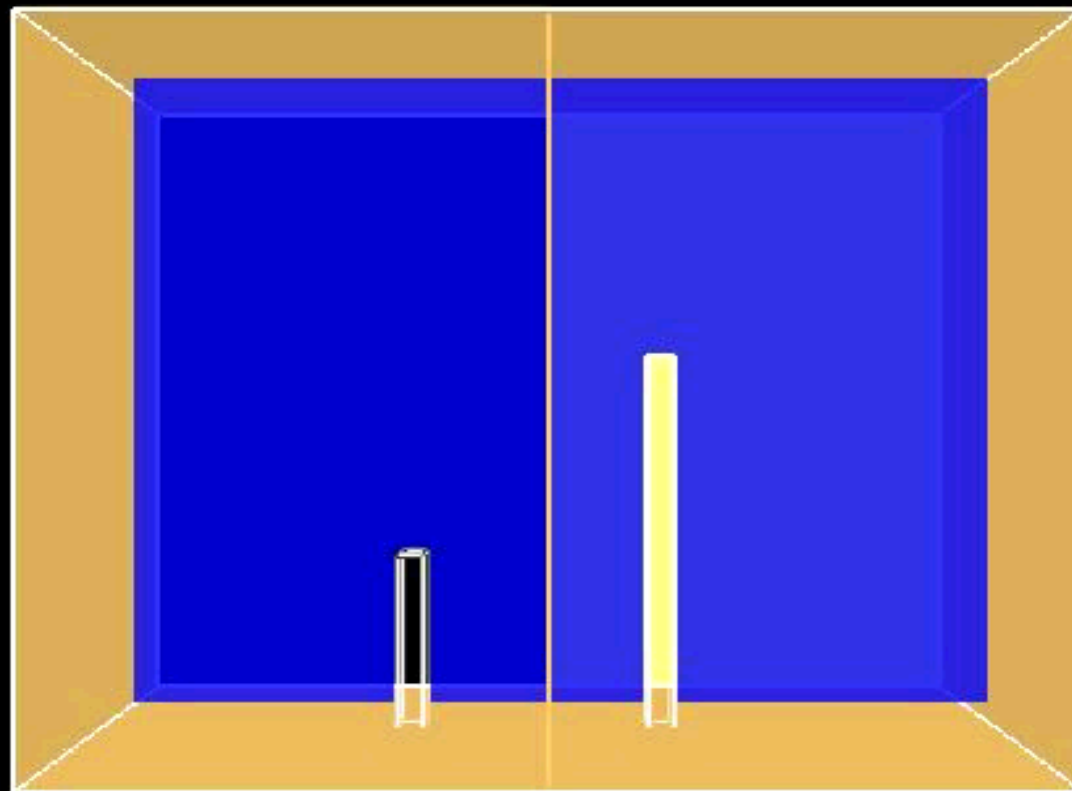
## CAEROT prediction vs experiment



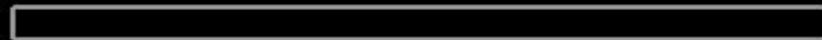
# Visualization (total aerosol concentration)



NIST Smokeview 3.0 - Nov 18 2002



Frame: 0  
Time: 60.0

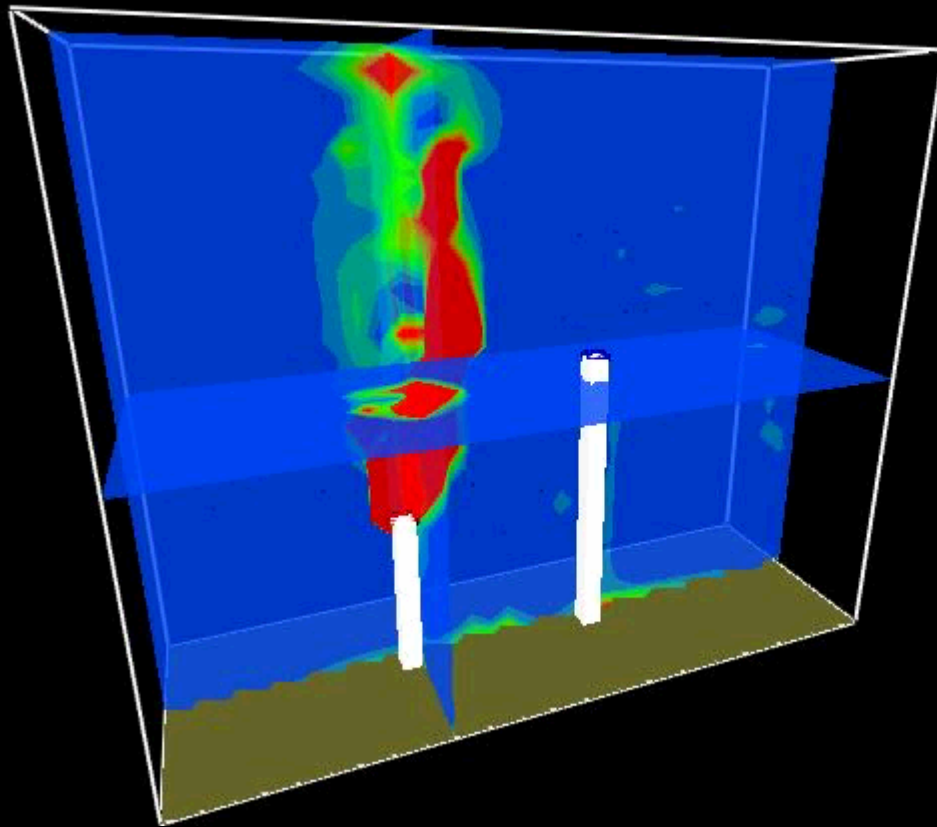


Frame rate: 2.7

# Aerosol Concentration Distribution



CAEROT 5x5 node simulation  
0.5 - 1.0 micron aerosol evolution



Plot3d  
0.5-1.0,  
cc/node  
\*10<sup>-9</sup>



Particles in  
0.5 to 1.0  $\mu$ ,  
at t=100 s

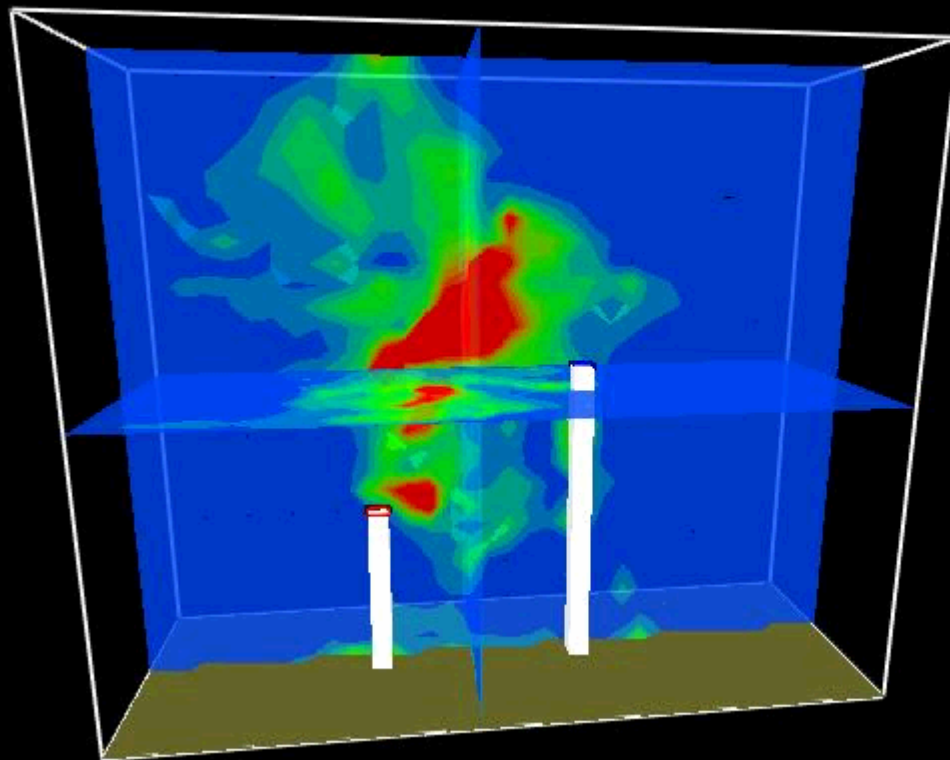
Source:  
60-120 s

xv: 14  
x7: 6  
vz: 12

# Aerosol Distribution



CAEROT 5x5 node simulation  
0.5 - 1.0 micron aerosol evolution



Plot3d  
0.5-1.0μ  
cc/node  
\*10<sup>-9</sup>

2.50  
2.25  
2.00  
1.75  
1.50  
1.25  
1.00  
0.75  
0.50  
0.25  
0.00

Particles in  
0.5 to 1.0 μ,  
at t=150 s

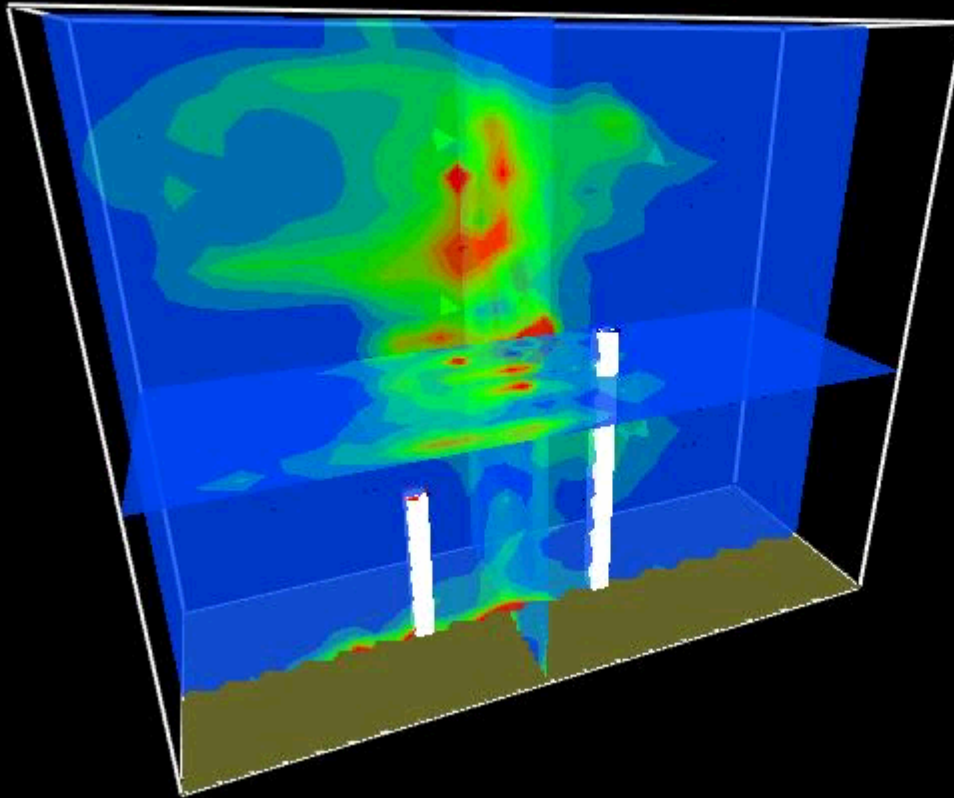
30 s after  
nebulizer  
stopped

xv: 14  
x7: 6  
v7: 16

# Aerosol Distribution



CAEROT 5x5 node simulation  
0.5 - 1.0 micron aerosol evolution



Plot3d  
0.5-1.0  
cc/node  
\*10<sup>-9</sup>

1.50  
1.35  
1.20  
1.05  
0.90  
0.75  
0.60  
0.45  
0.30  
0.15  
0.00

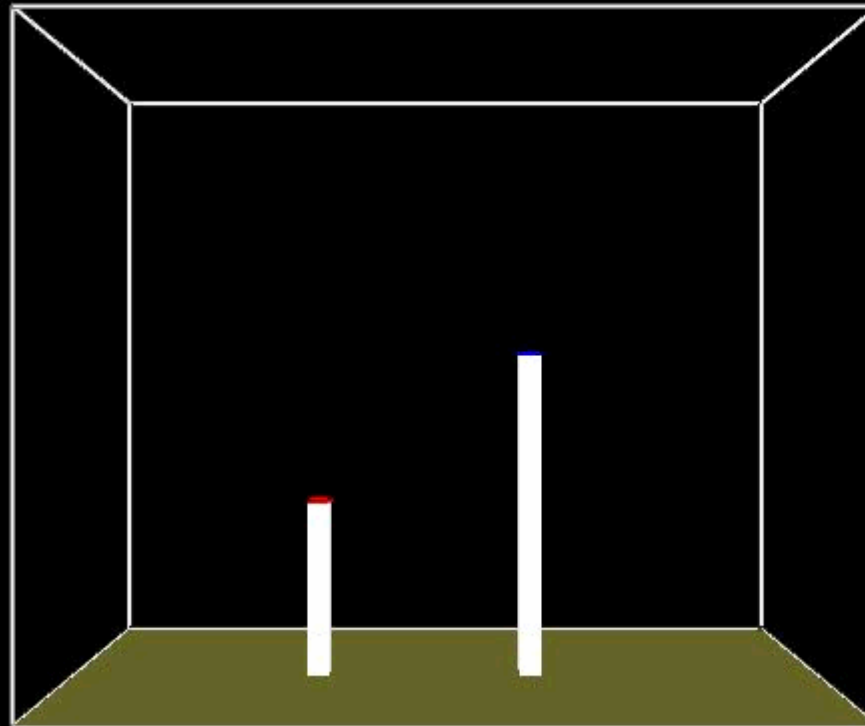
Particles in  
0.5 to 1.0  $\mu$ ,  
at t=200 s

xv: 1.3  
x7: 5  
v7: 1.6

# Aerosol Distribution –3D



CAEROT 5x5 node simulation  
0.5 - 1.0 micron aerosol evolution



Plot3d  
0.5-1.0  
cc/node  
\*10^-10

10.00  
9.00  
8.00  
7.00  
6.00  
5.00  
4.00  
3.00  
2.00  
1.00  
0.00



# Conclusions for the code development

- SAEROSA is stand-alone for well-mixed cases.
- CAEROT has good agreement with experiments.
- Result of simulation is sensitive to velocity field.
  - Low velocities require finer spatial mesh for CAEROT
- Further refinements:
  - Turbulent coagulation
  - Growth (condensation/evaporation)
  - Phoretic effects (thermo-, electro- )
  - Multi-species aerosol
- Availability: Planned through ORNL RSICC library.

# Current/Future Work

- Sensitivity studies
  - Validity with different experiment and different geometries
- Inclusion of obstructions is coded but not validated
- Open boundaries
- Applications:
  - Transport through ducts: design a detector
  - Transport in the lung: better understanding



# Design of an Aerosol Detector

Transport through micro-fabricated channels

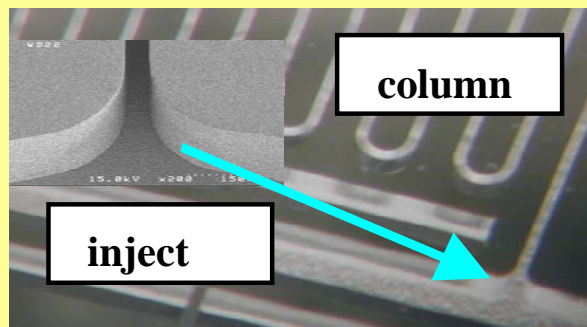
# Rapid Aerosol Detection with Species Identification

- Small size detector
  - Resolves size spectrum
  - Screens organic vs inorganic species
  - Identifies organic molecules
- Rapid response
- Wireless units operated in a network
- Provides near-real-time aerosol phase space information

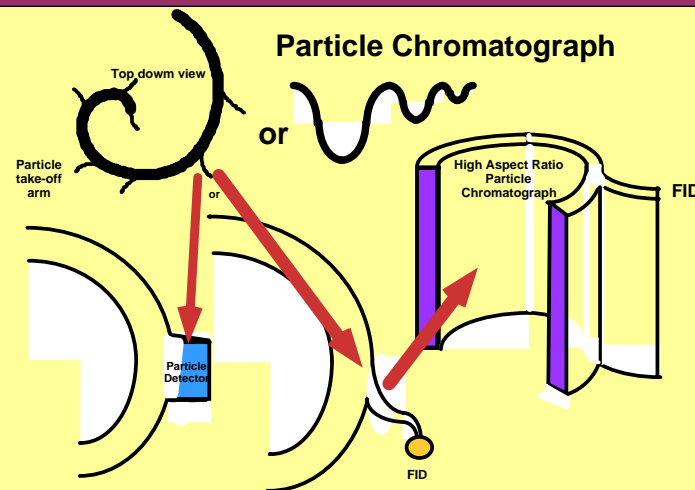
# High Aspect Ratio Particle Chromatograph (HARPC)

- Momentum sorting through a micro-fabricated channel system
- Material identification via flame ionization

QuickTime™ and a Graphics decompressor are needed to see this picture.



Pictures of High Aspect Ratio GC Columns, made with LIGA microfabrication technology, of metal tubes  $50\mu$  wide and  $500\mu$  high, and 2 meters in length.



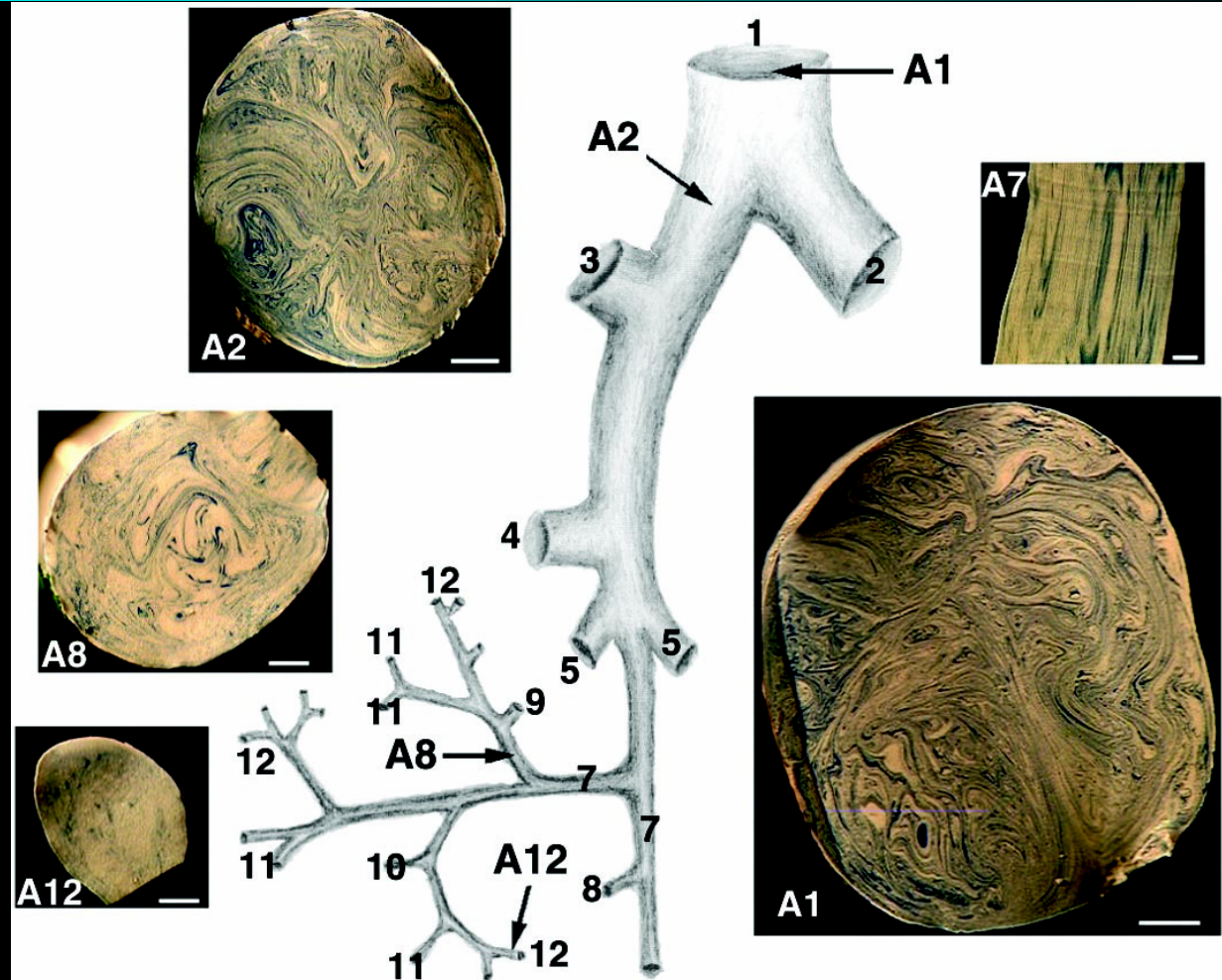
Concept drawing showing possible particle take-off arms for detection of hydrocarbon containing aerosol particles with the "Particle Chromatograph".

# Transport in the lung

Aerosol dynamics in chaotic mixing

# Flow patterns in the airways

- A1: Trachea (bar=500  $\mu$ )
- A2: Main stem bronchus (bar =500  $\mu$ )
- A7: Medium size airway (bar =100  $\mu$ )
- A8: Medium size airway (bar =200  $\mu$ )
- A12: Small airway (bar =100  $\mu$ )



Courtesy of A. Tsuda, Harvard U.

Critical factor in aerosol retention: kinematic interaction between inhaled and residual alveolar gas.

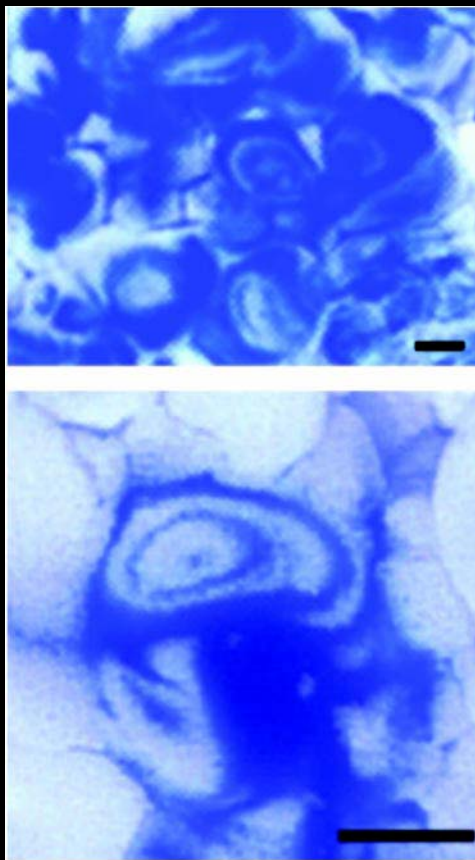
# Air flow in the alveolar region

- Low Re number ( $\sim 1$ )
- Reversible lung wall motion
- Kinematically reversible Stokes flow?
- In reality:
  - Inertial stream-line crossing, sedimentation and diffusion alone do not explain the degree of deposition seen in experiments.
  - Oscillatory Stokes flow can result in chaotic behavior
  - Stagnation saddle points in the alveolar openings
  - Lagrangian simulation shows irreversible stretched and folded flow patterns

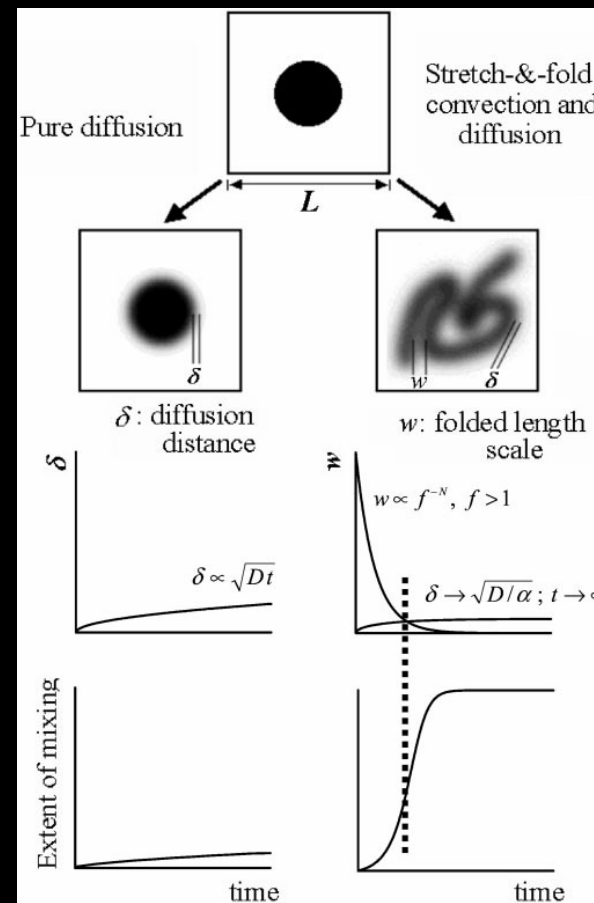
# Stretch and fold patterns

interaction of diffusion and convection

Alveolar recirculation  
(bar = 100  $\mu$ )



Brownian mixing vs stretch & fold convection + diffusion



$\alpha$  = stretching rate  
 $f$  = cycle-by-cycle  
folding factor

When length scales  
of  $w$  and  $\delta$  are  
comparable, an  
entropy “burst”  
occurs characteristic  
to chaotic mixing



Thank You