

Fourth CW and High Average Power RF Workshop **Coaxial switch**, high power load and higher harmonic absorber for **PROSCAN**

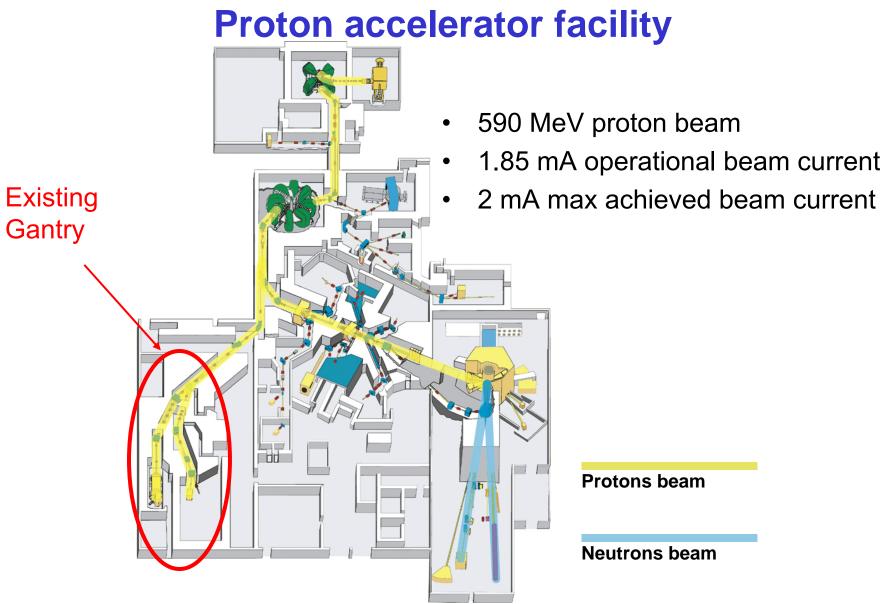
Markus Schneider, RF power amplifier



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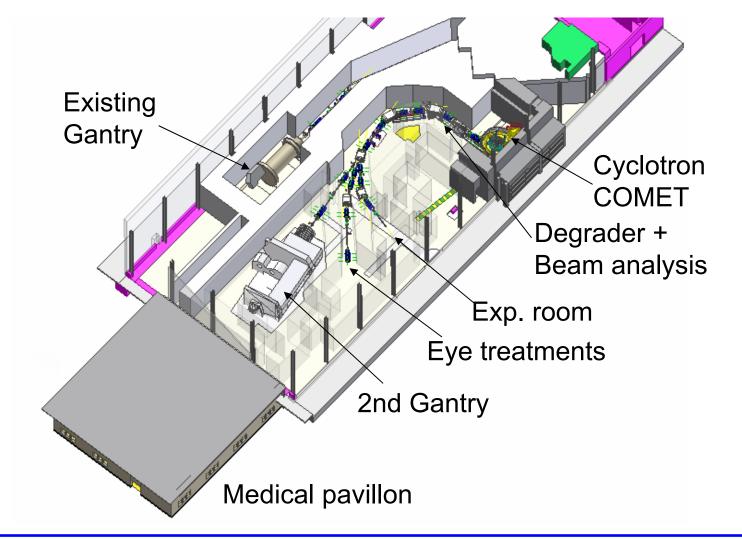
- The PROSCAN Project
- The RF System of PROSCAN
- Coaxial Switch
- 300 kW RF Power Load
- Higher Harmonic Absorber







PROSCAN





PROSCAN



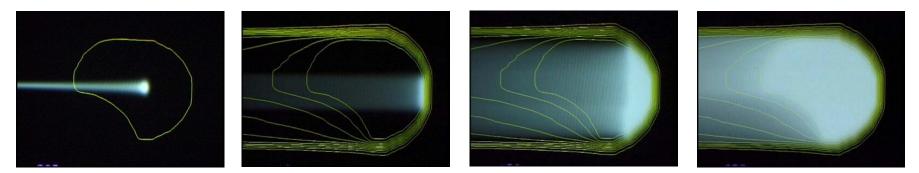


Medical pavillon

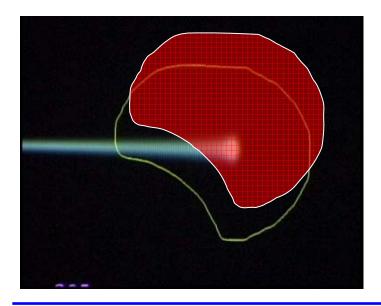
Existing Gantry



Spot scanning technique at PSI



Proton pencil beam scans the tumor in 3 dimensions \rightarrow 3D : lateral + depth



Dynamical treatments Danger to underdose and overdose

PROSCAN approach:

Maximum flexibility for research of strategies

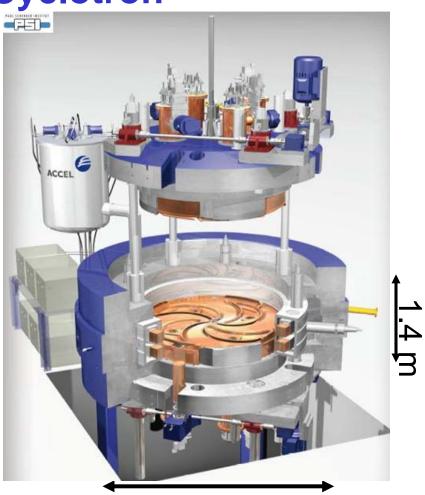
- Multiple scans of tumor
- increase scan speed
- intensity modulation



new cyclotron for proton therapy: 250 MeV, 500 nA superconducting coils basic design: NSCL (H. Blosser)

manufactured by





3.4 m





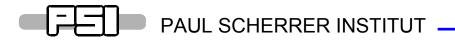
Magnet sectors

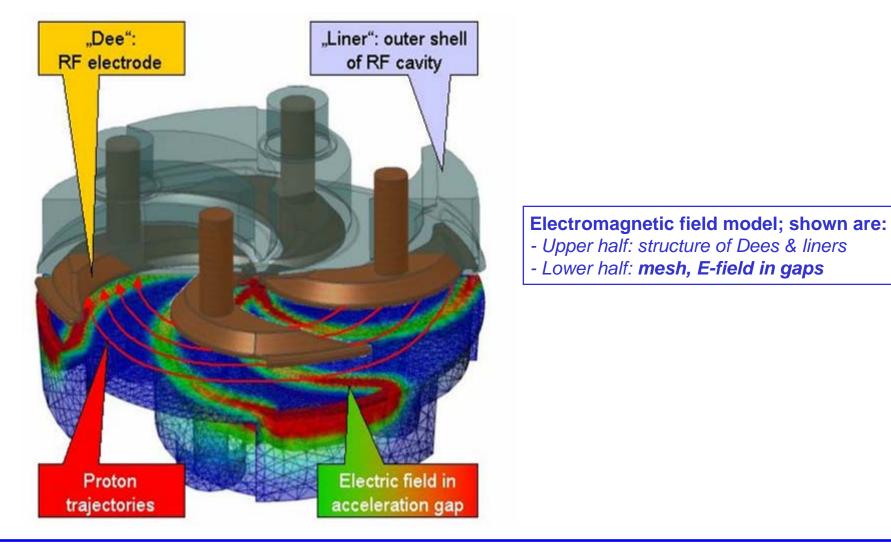
Iron yoke

- Outer diameter 3.1 m
- Height 1.6 m
- weight 90 t

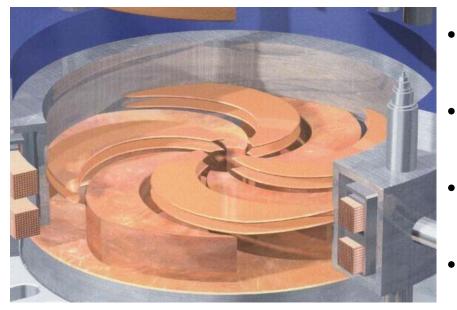
Magnet

- Superconducting coils
- Magnetic Field 2.4 3 T
- Operating current 160 A
- Rated power cryocoolers 40 kW









- Frequency 72.8 MHz (2nd harmonic)
- Voltage Source to Puller 80 kV
- Voltage @ extraction radius 130 kV
- RF-Power 120 kW





1. April 2005 first beam extracted

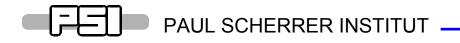
2005 / 2006

- 500 nA Beam current
- Extraction efficiency 80%

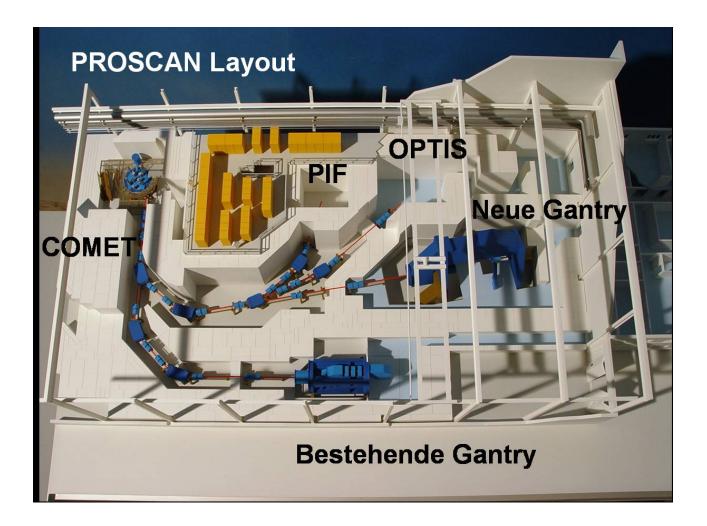
Now connecting Gantry 1 to Cyclotron

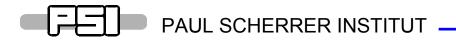
OUTLOOK

- June 2006 first beam to Gantry 1
- In fall 2006 first patient treatment in Gantry 1

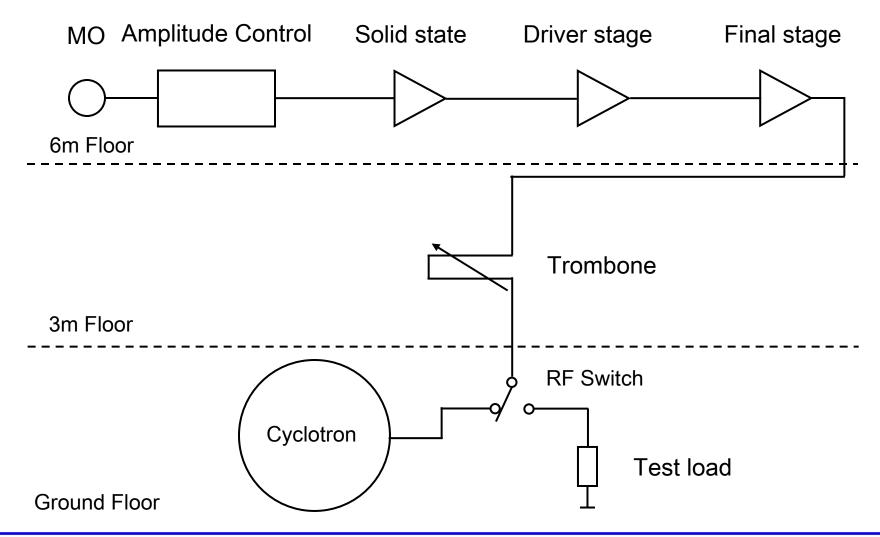


PROSCAN





RF System of PROSCAN



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Fourth CW and High Average Power RF Workshop / May 2006 / M. Schneider





Amplifier for PROSCAN

- 150 kW CW amplifier at 72 MHz
- Designed and manufactured by Bertronix, Munich
- 300 W solid state
- 8 kW driver stage Tetrode TH 561 SC
- 150 kW final stage Tetrode TH 781
- Water cooled tubes from Thales

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6 1/8 " EIA coaxial transmission line 3m floor



- 6 1/8 " EIA transmission line with trombone
- Manufactured by Spinner
- Installed by PSI



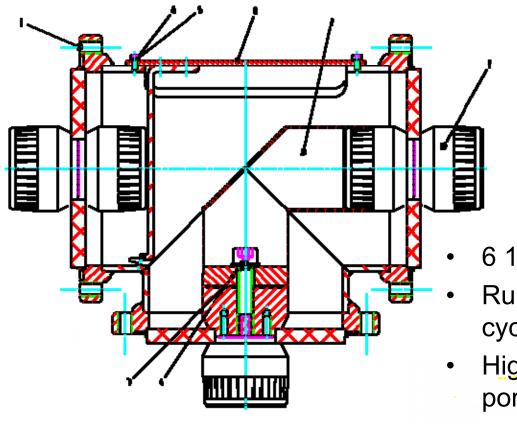
6 1/8 " EIA coaxial transmission line ground floor



- Coaxial Switch
- Absorber
- Transmission line to cyclotron



Coaxial Switch



- 6 1/8 " EIA flange
- Run amplifier on cyclotron or load
- High isolation to disconnected
- port
- Same size as 90° bend ٠



Coaxial Switch



- Coaxial switch in the machine shop
- Outer conductor made of aluminium
- Cover of switching window made of brass
- Inner conductor made of copper and brass
- Finally inner conductor and cover will be silver plated



Measurements of Coaxial Switch

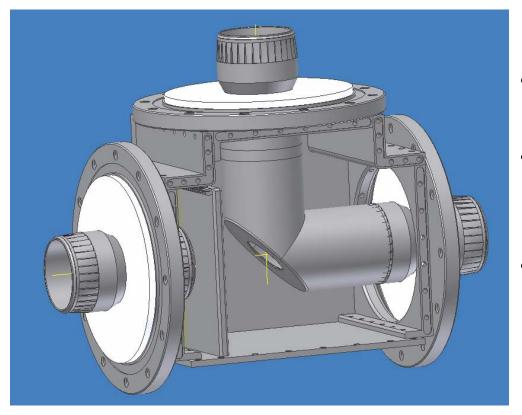


RF Switch with window opened

- Port 1 connected to port 2
- Measured at 72 MHz
- Matching Port 1 40 dB
- Isolation to Port 3 52 dB



New Design of Coaxial Switch



- Better RF shielding
- Higher isolation to disconnected port
- Easier to manufacture

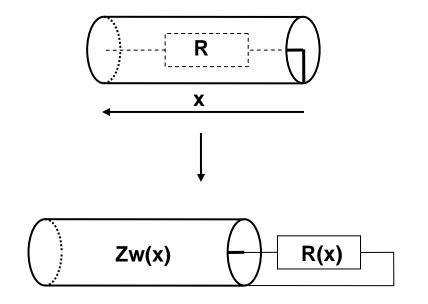


300 kW RF Power Load

- For commissioning, acceptance test and maintenance of the PROSCAN amplifier a high power 50 Ω load was needed.
- The maximal output power of the amplifier was rated at 200 kW. To allow for some margin, the decision was made to build a 300 kW load.
- To handle this power water cooling is needed. A solution of sodium carbonate in water acts as absorbing material and as cooling medium at the same time.
- The operating frequency of the amplifier is 72 MHz.
- Design of a wideband load with VSWR < 1.15
- 6 1/8 " EIA coaxial line connector



300 kW RF Power Load



Simplified electrical schematic of the absorber

- Wideband Load Zw(x) = R(x)
- Coax transmission line
 D = outer Diameter
 d = inner Diameter

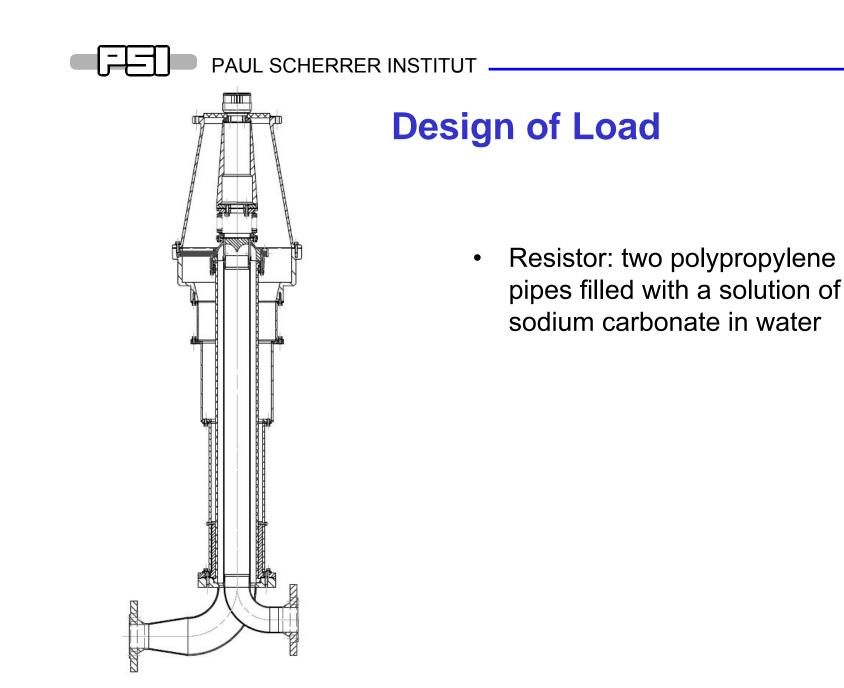
 $Zw(x) \approx 60 \ \Omega \cdot \ln\left(\frac{D(x)}{d}\right)$

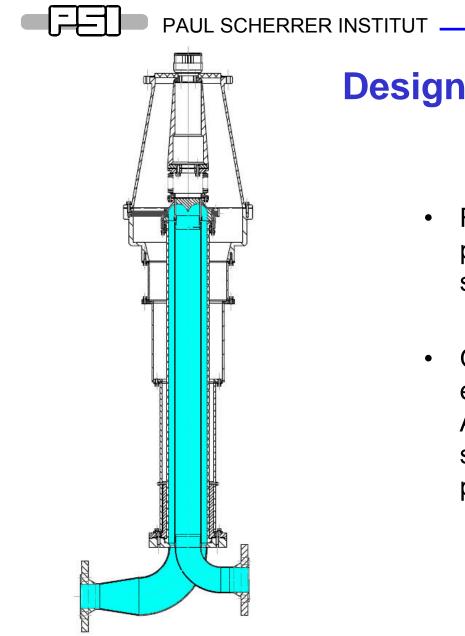
Resistor
 I = length of Resistor

$$R(x) = R_0 \cdot \frac{x}{l} = 50 \ \Omega \cdot \frac{x}{l}$$

• Ideal Absorber outer diameter

$$D(x) = d \cdot e^{\left(\frac{50\,\Omega}{60\,\Omega} \cdot \frac{x}{l}\right)}$$



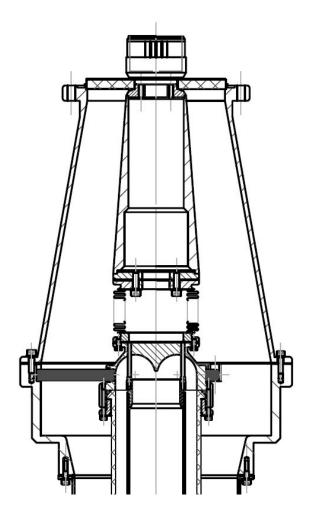


Design of Load

- Resistor: two polypropylene pipes filled with a solution of sodium carbonate in water
- Outer conductor in form of exponential curve.
 Approximated with 5 pieces of silver plated brass or copper pipes.



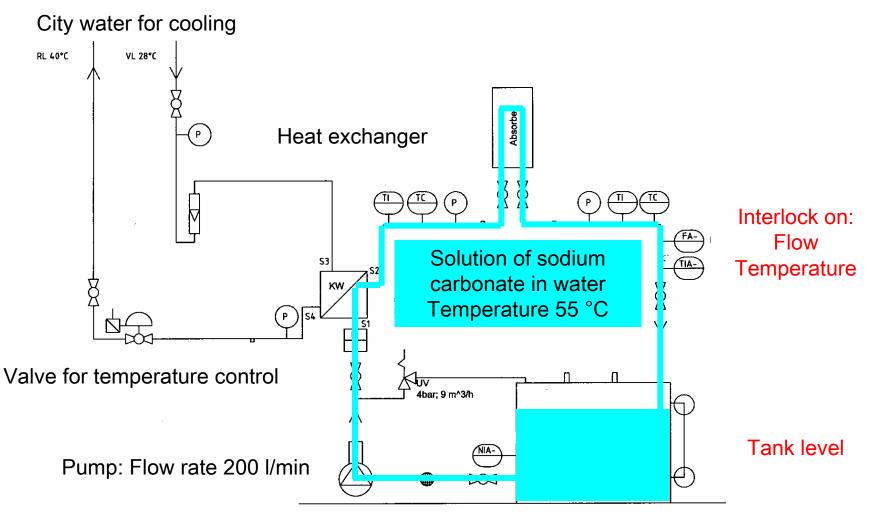
Design of Head of Absorber



- 6 1/8 " EIA coaxial line
- Cone
- Bellows to avoid mechanical forces
- 3 Isolators to center the inner conductor
- Turning head for water



Water Circuit





Control System of Load

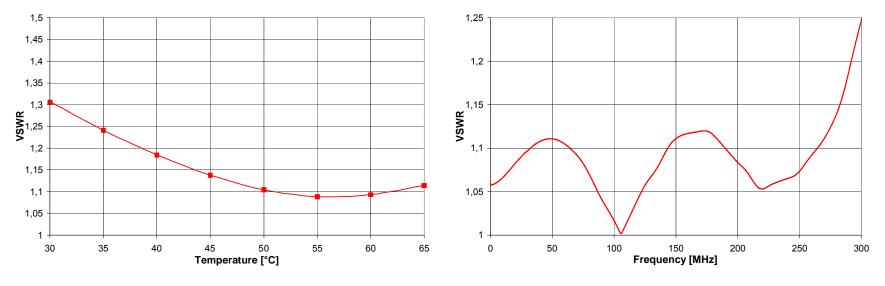


- Temperature of coolant is controlled within 3° C
- PLC for Interlock handling
- Calorimetric calculation of dissipated power

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Measurement of 300 kW RF Power Load

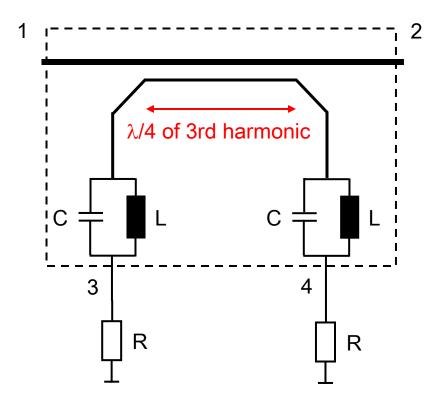


Measurement of the VSWR versus the temperature at 72 MHz Measurement of the VSWR in function of the frequency

During commissioning, acceptance tests and troubleshooting of the amplifier in 2005 / 2006, up to 150 kW of RF power were dissipated in the load without any problems.



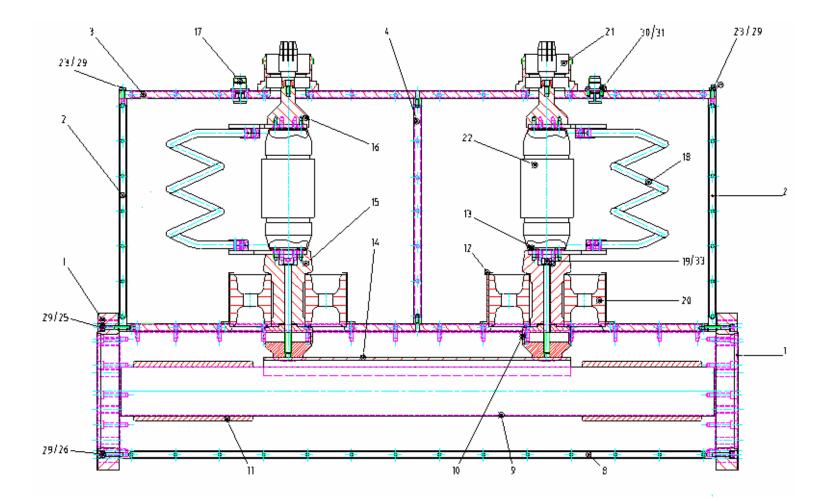
Higher Harmonic Absorber



- 3 dB directional coupler at λ/4 of third harmonic frequency
- Stop band filter for fundamental frequency
- 50 Ω Load



Cross Section of Higher Harmonic Absorber





Cross Section of Higher Harmonic Absorber

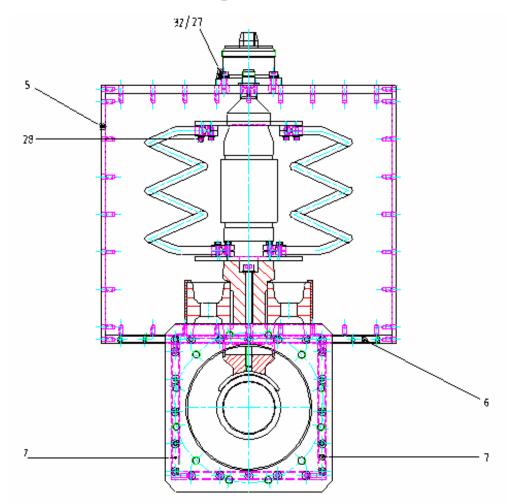


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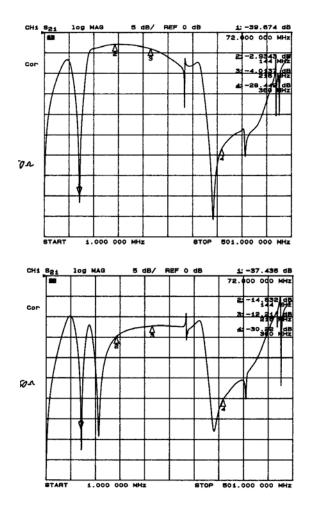


Cross Section of Higher Harmonic Absorber





Measurements of Higher Harmonic Absorber



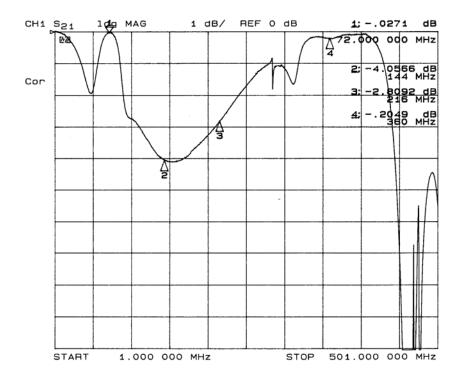
Fundamental:	- 39 dB
2nd harmonic:	- 2.9 dB
3rd harmonic:	- 4.0 dB

Measurement S31

- 37 dB
- 14 dB
- 12 dB



Measurements of Higher Harmonic Absorber



Measurement S	521
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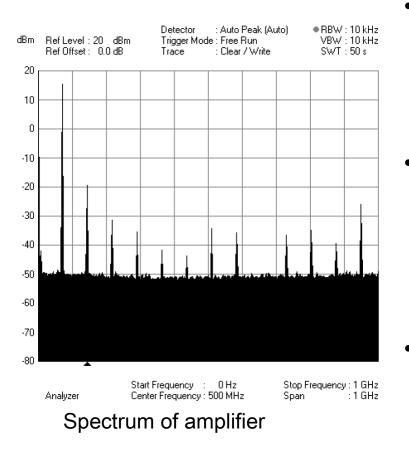
Fundamental: - 0.02 dB

2nd harmonic: - 4 dB

3rd harmonic: - 2.8 dB

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Conclusion



- Higher harmonic absorber works as expected. 2nd and 3rd harmonic are reduce by 3 dB. No influence on fundamental frequency
- Due to the fact, that all harmonics of the amplifier are 30 dB below the fundamental frequency, the higher harmonic absorber is not installed up to now.
- Within 15 minutes the amplifier can be switched form cyclotron to the load. This was done several times during commissioning without of problems.