



U.S. Department of Energy
Office of Civilian Radioactive Waste Management



Drift Stability: Seismic and Thermal

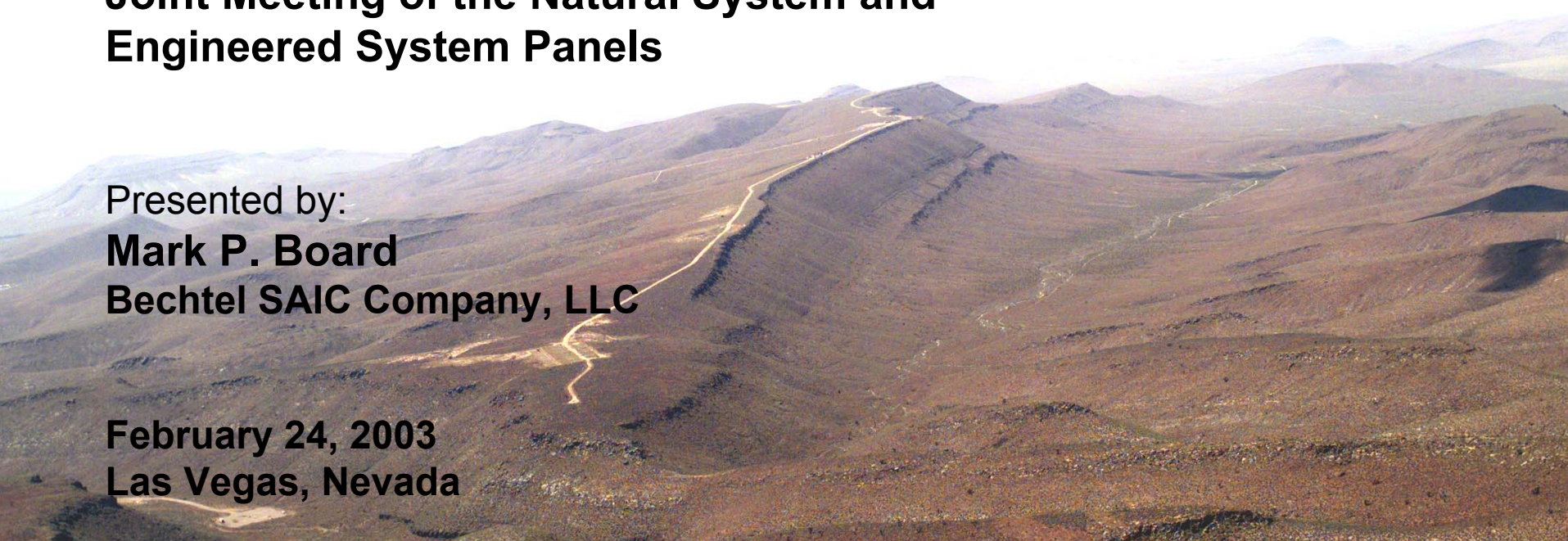
Presented to:

**Nuclear Waste Technical Review Board
Joint Meeting of the Natural System and
Engineered System Panels**

Presented by:

**Mark P. Board
Bechtel SAIC Company, LLC**

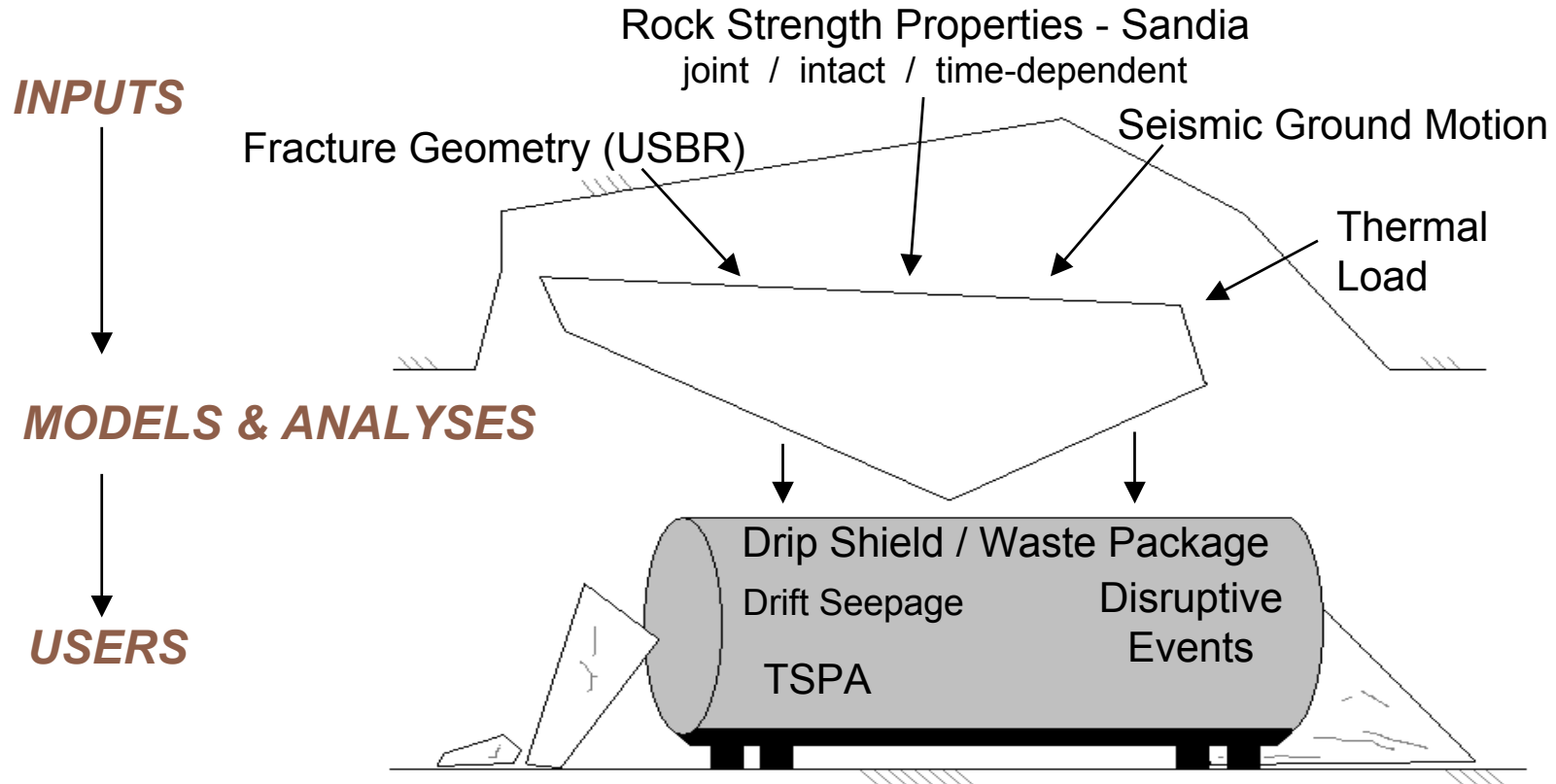
**February 24, 2003
Las Vegas, Nevada**



Objectives of Study

- **Produce a geologically-based estimate of the distribution of rockfall for lithophysal and non-lithophysal rocks as a function of ground motion**
 - **Rockfall defined in terms of:**
 - ◆ **Total tons per “unit length” of tunnel**
 - ◆ **Distribution of block sizes/masses**
 - ◆ **History of velocity (energy), position and timing of ejected blocks**
- **Estimate rockfall as a function of variability of geology, rock properties and ground motion**
- **Determine impact of thermal load history and time-related degradation**

Rockfall Modeling and Analysis



Contributors

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Sandia - Larry Costin, Ron Price

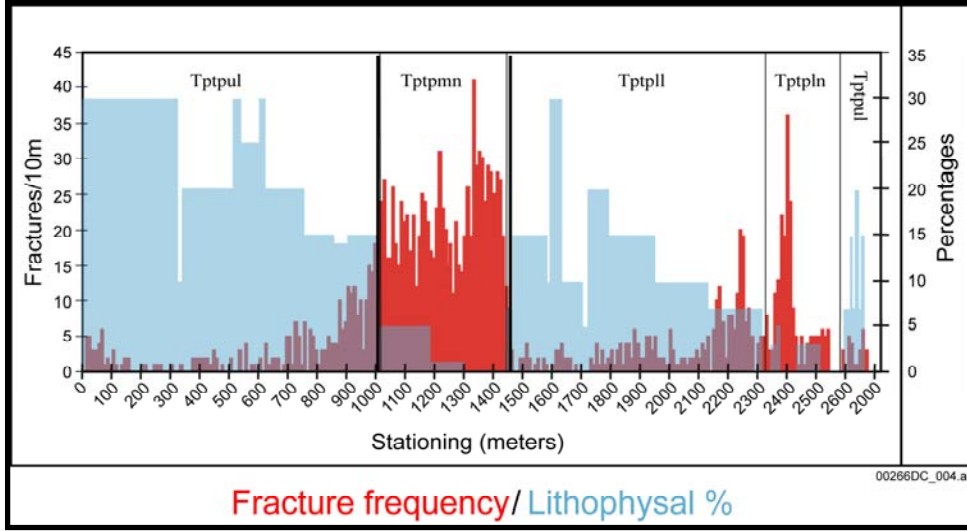
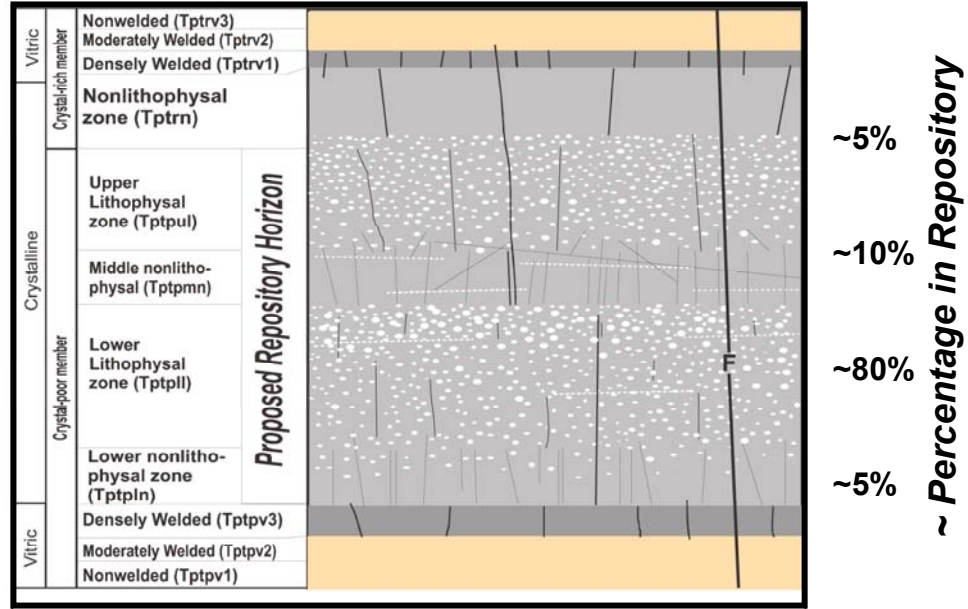
Univ. of Arizona - John Kemeny



Two Distinct Rock Types in Proposed Repository

- Non-Lithophysal and Lithophysal Rock

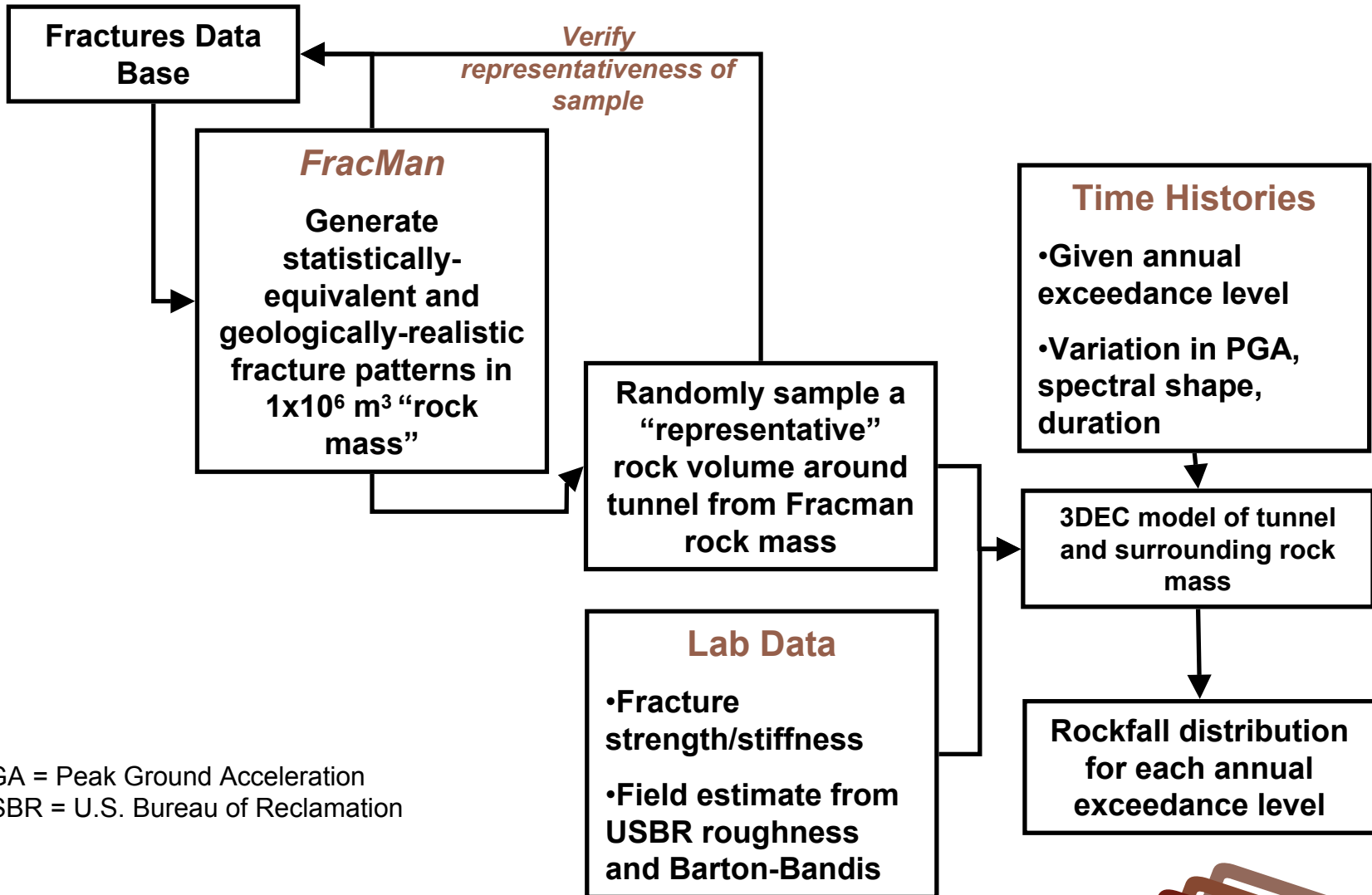
Non-lithophysal is strong, fractured rock, 150 MPa Unconfined Compressive Strength (UCS), Modulus (E)~30GPa, GSI ~ 60 - 70



Lithophysal rock is high lithophysal porosity (10-30%), ~ 7 to 15 MPa UCS, E~1-5 GPa



Modeling Approach for Non-Lithophysal Rocks

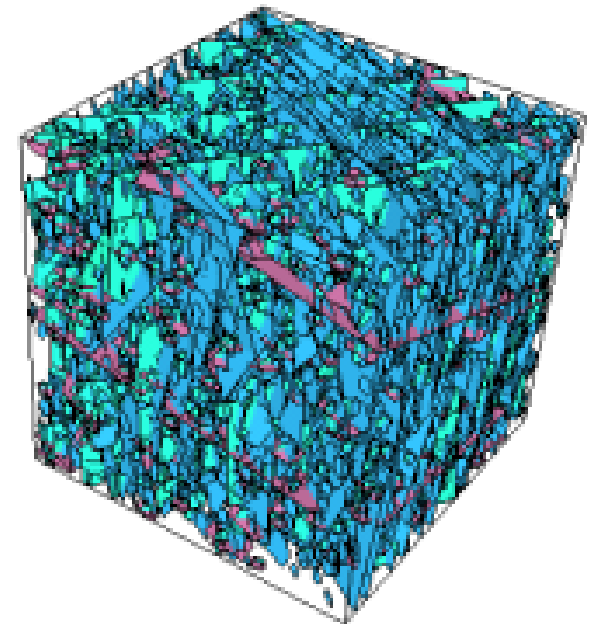
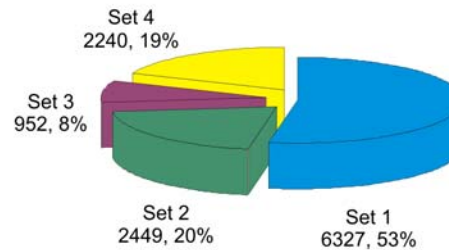
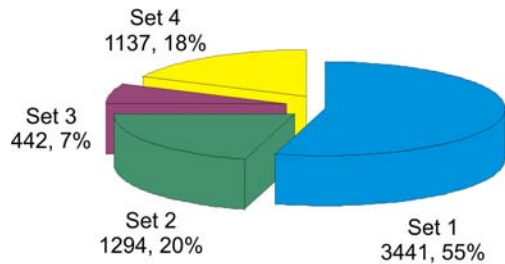
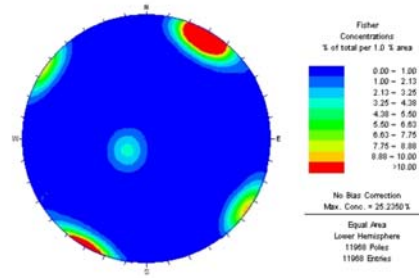
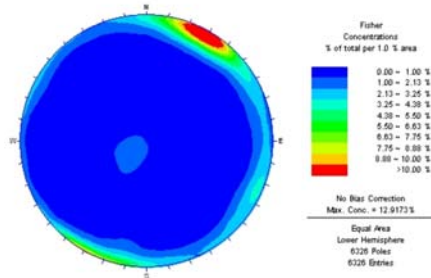


PGA = Peak Ground Acceleration
USBR = U.S. Bureau of Reclamation

Fracture Modeling using FracMan

DLS Data

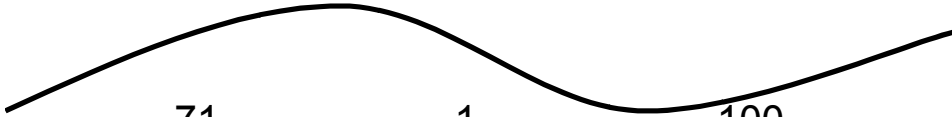
Fracman Data



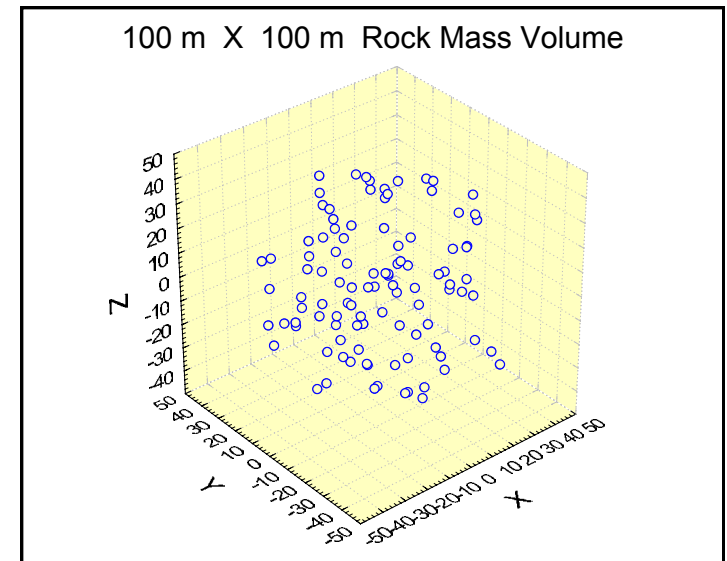
Fracture Data FracMan vs Detailed Line Survey Data					
Orientation of Sets		Trace Length		Spacing	
		FM	DLS	FM	DLS
Set 1	122/84	1.8m	2.3m	0.61m	0.55m
Set 2	195/85	1.5m	1.9m	1.61m	1.48m
Set 3	306/09	2.1m	2.7m	6.8m	4.20m
Set 4	150/90	1.4m	1.7m		

Orientation = Strike/Dip
 FM = Fracture Mapping
 DLS = Detailed Line Survey

Sampling Strategy for Rockfall 3DEC Analyses

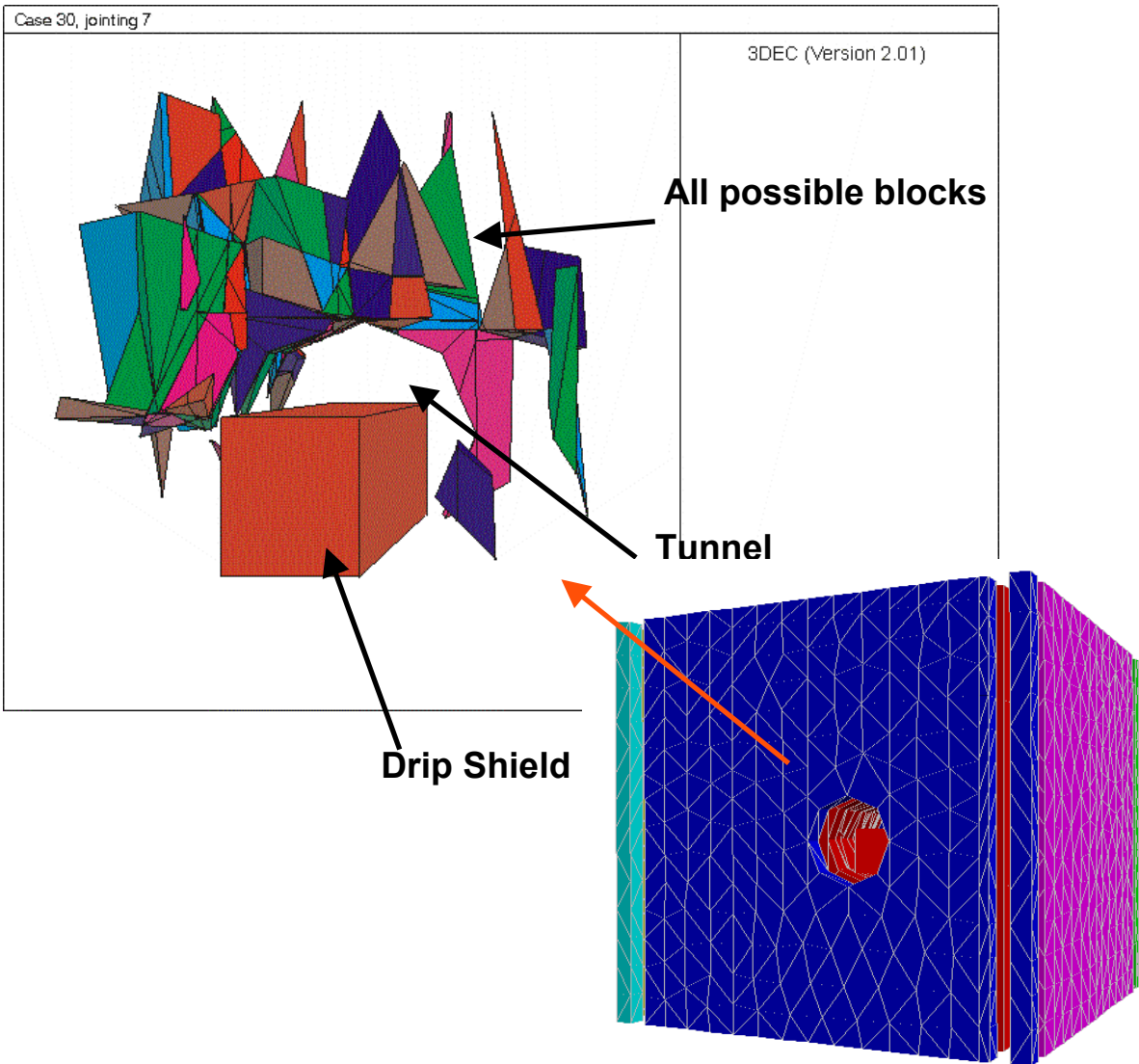
Realization Number	Ground Motion Time History Number	Synthetic Fracture Pattern Number
1	7	22
2	11	21
3	11	30
4	16	27
5	14	26
6	13	10
		
71	1	100
72	16	13
73	2	73
74	11	43
75	7	72
76	11	105

- The complete sample space: 105 fracture patterns x 16 ground motions
- Apply Latin Hypercube random sampling technique to select 76 representative cases



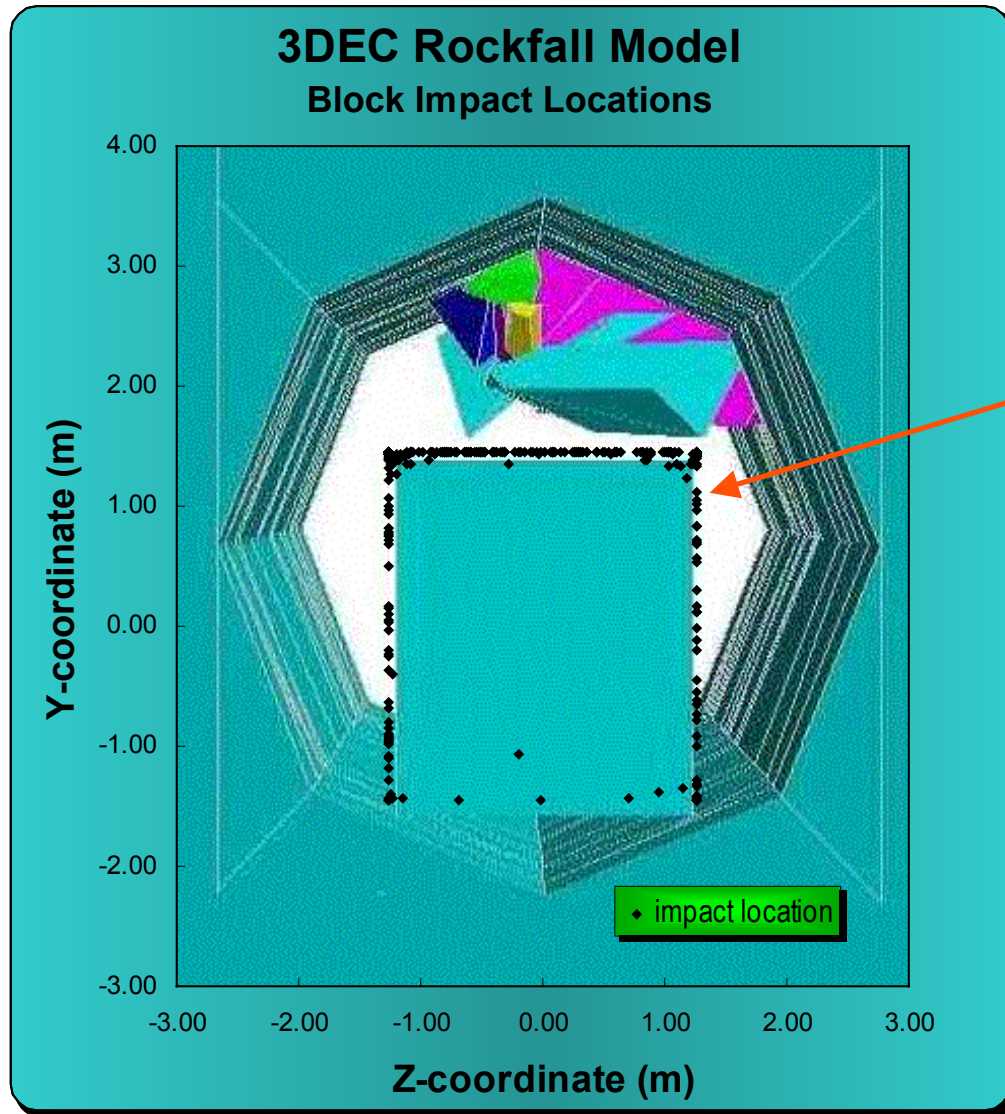
Example 3DEC Model Block Structure

(outside block structure removed)



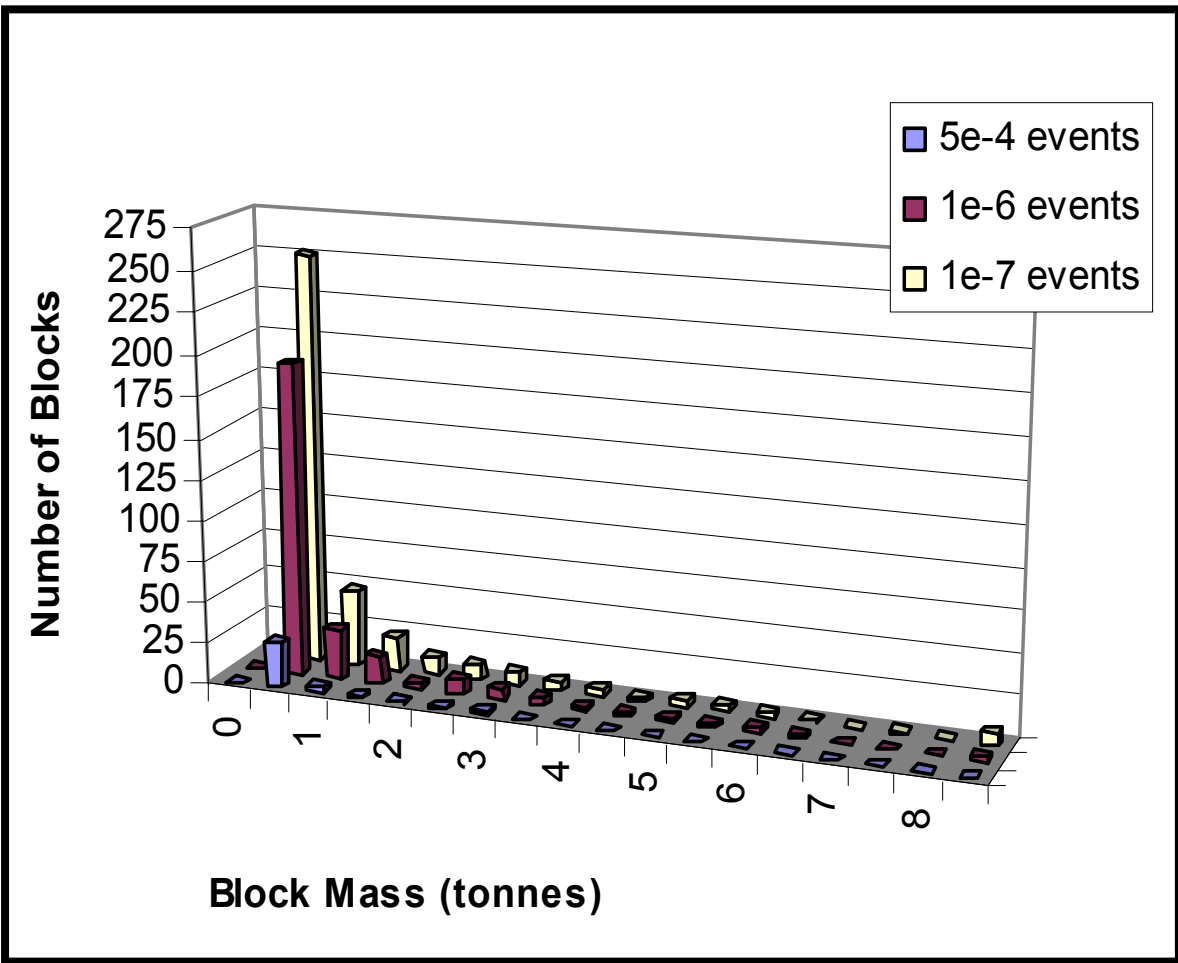
- **Currently examining 100 or more analyses per ground motion**
- **FracMan input of fractures**
- **Partially-penetrating cracks in larger blocks modeled**
- **Base case assumes planar, zero dilation joints**
- **Examine range of joint surface properties**
- **Examine impact of thermal load history**

Determine Block Impact Location, Mass and Velocity



Block impact location to drip shield - record mass, velocity, time

Results - Distribution of Rockfall Block Mass for Non-Lithophysal Rock



- Rockfall largely controlled by block geometry and peak particle velocity (ppv)
- Median block size is approximately 0.25 tonne for all cases
- Fracture dilation angle potentially important, friction angle unimportant
- Thermal load decreases rockfall during heating phase



Lithophysae and Fracturing in the Lower Lithophysal Unit



- Lithophysal porosities of 10% to 30%
- Block size controlled by
 - Lithophysae spacing
 - Extensive cooling fracture network
- Block sizes produced are on order of inches when rock is overstressed

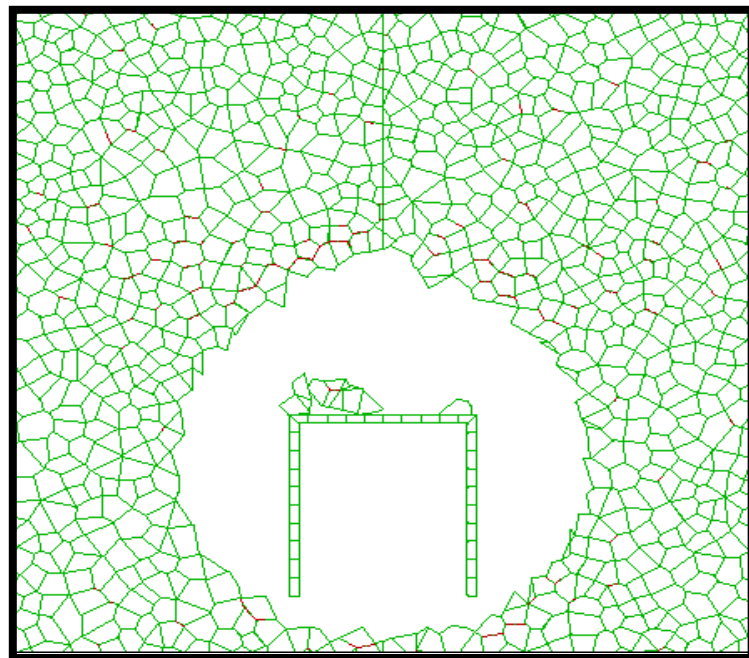
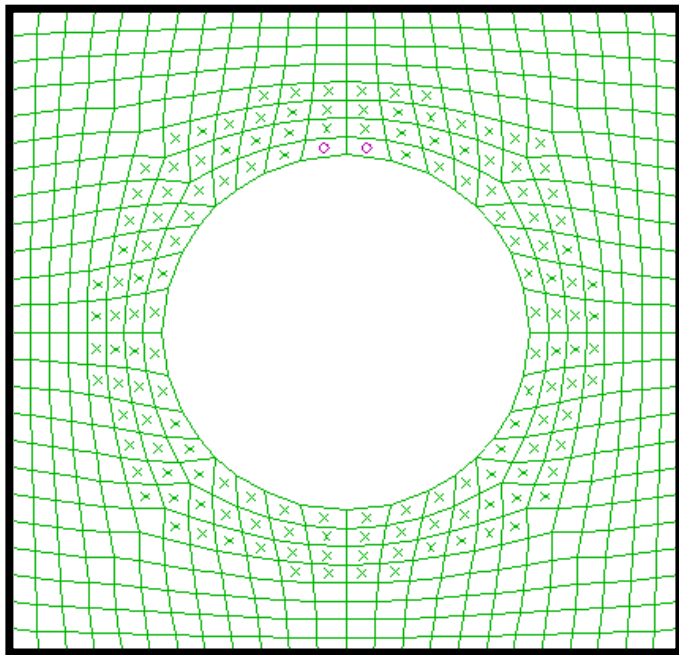
Potential Size of Rock Particles

Modeling Approach

Continuum

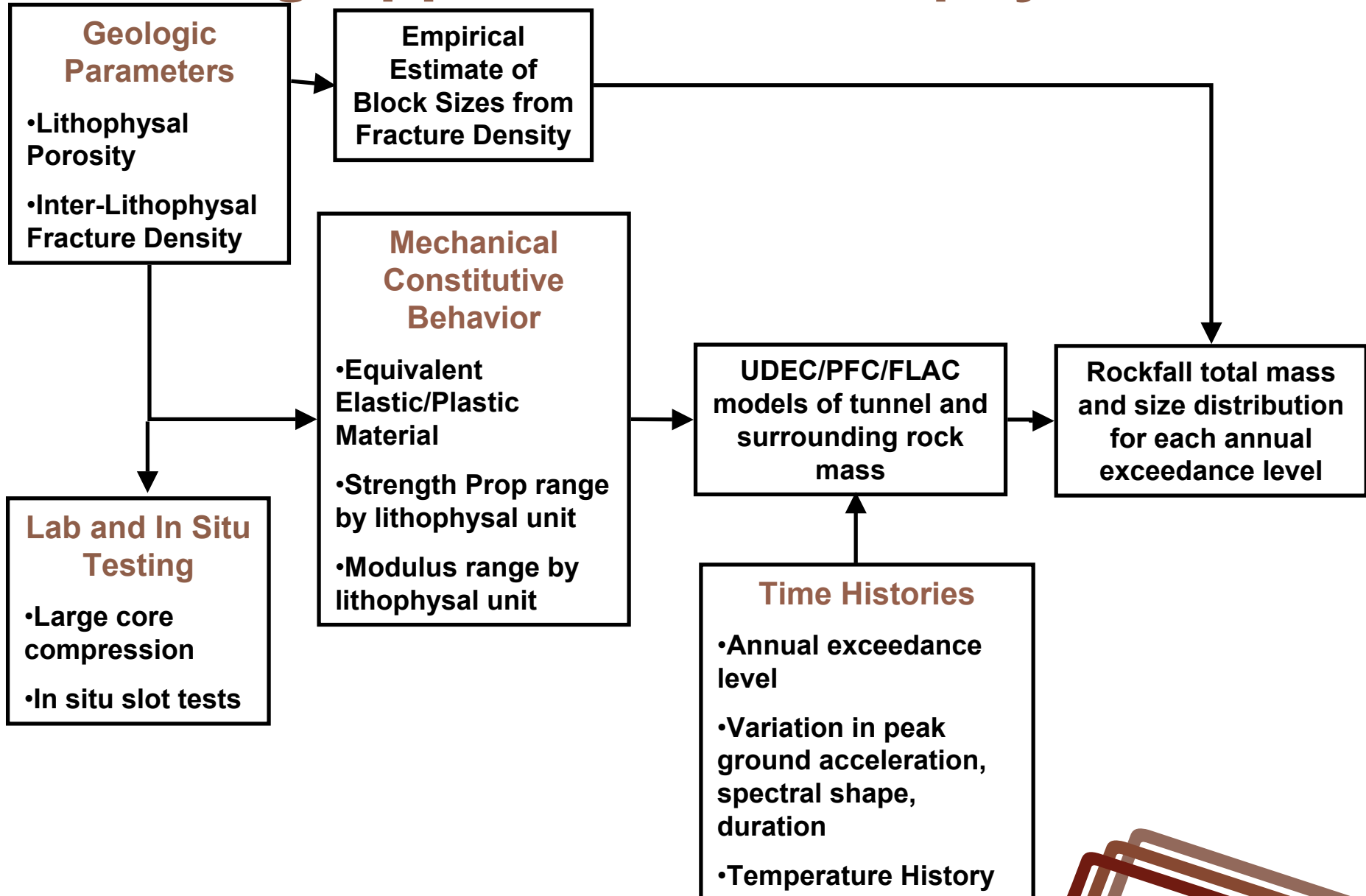
versus

Discontinuum



- Randomly-shaped “Voronoi” blocks in UDEC model do not represent actual internal structure of the lithophysal rock mass
- Blocks are computational tool used to represent damage in the model and formation of loose blocks
- Model has to be calibrated to ensure that its “macro” behavior is the same as behavior of the lithophysal rock mass

Modeling Approach for Lithophysal Rocks

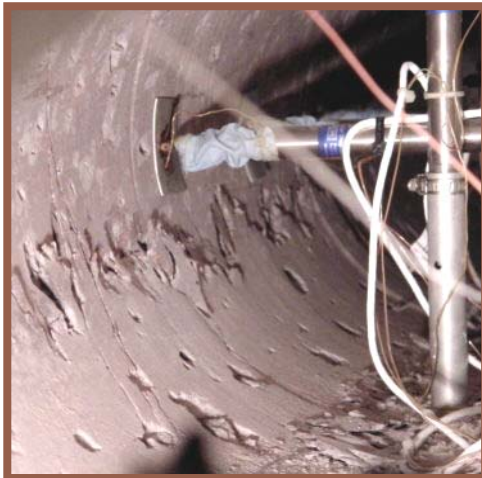


Testing

Mechanical and Physical Properties



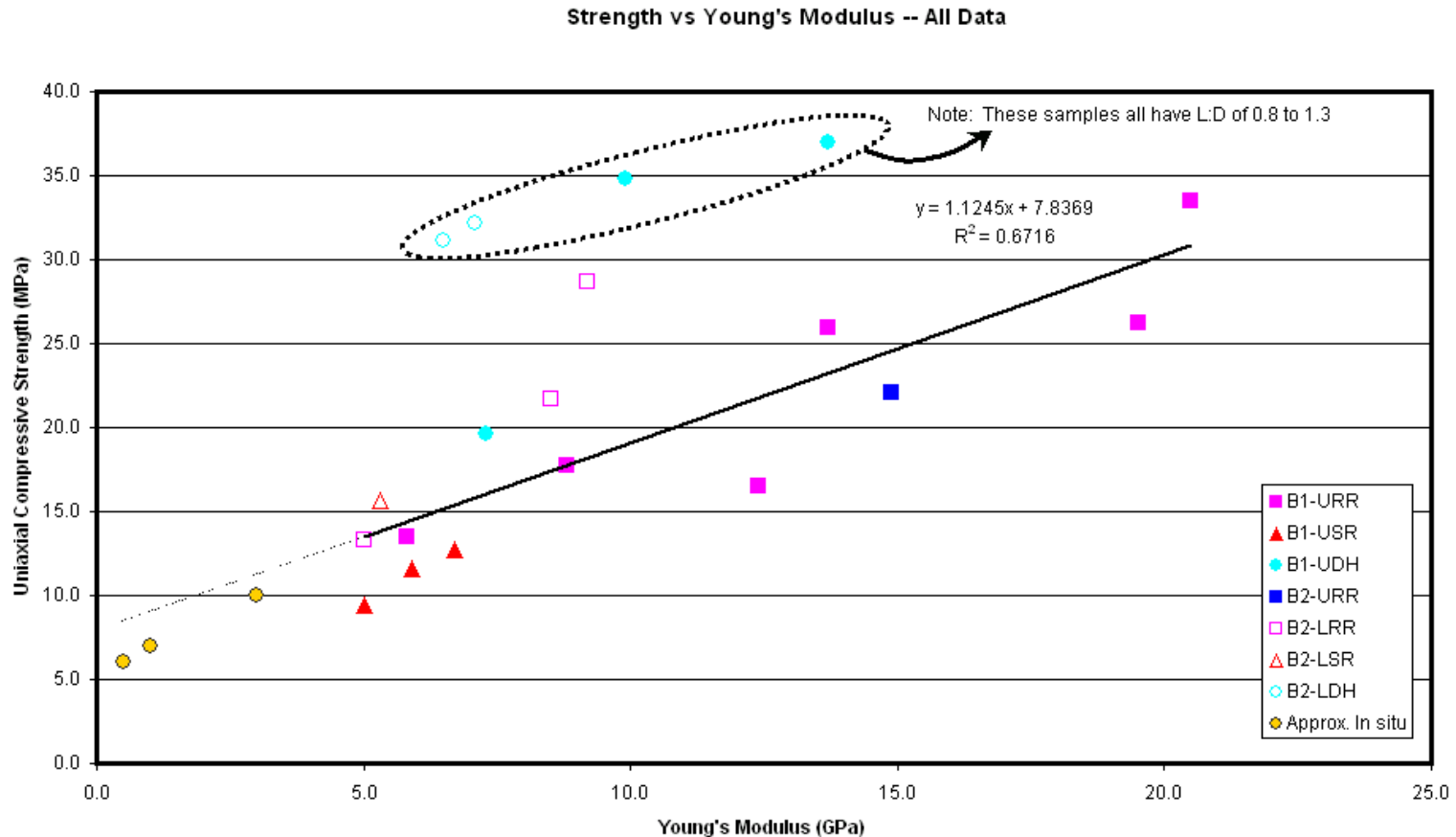
*In Situ Slot
Compression
Testing*



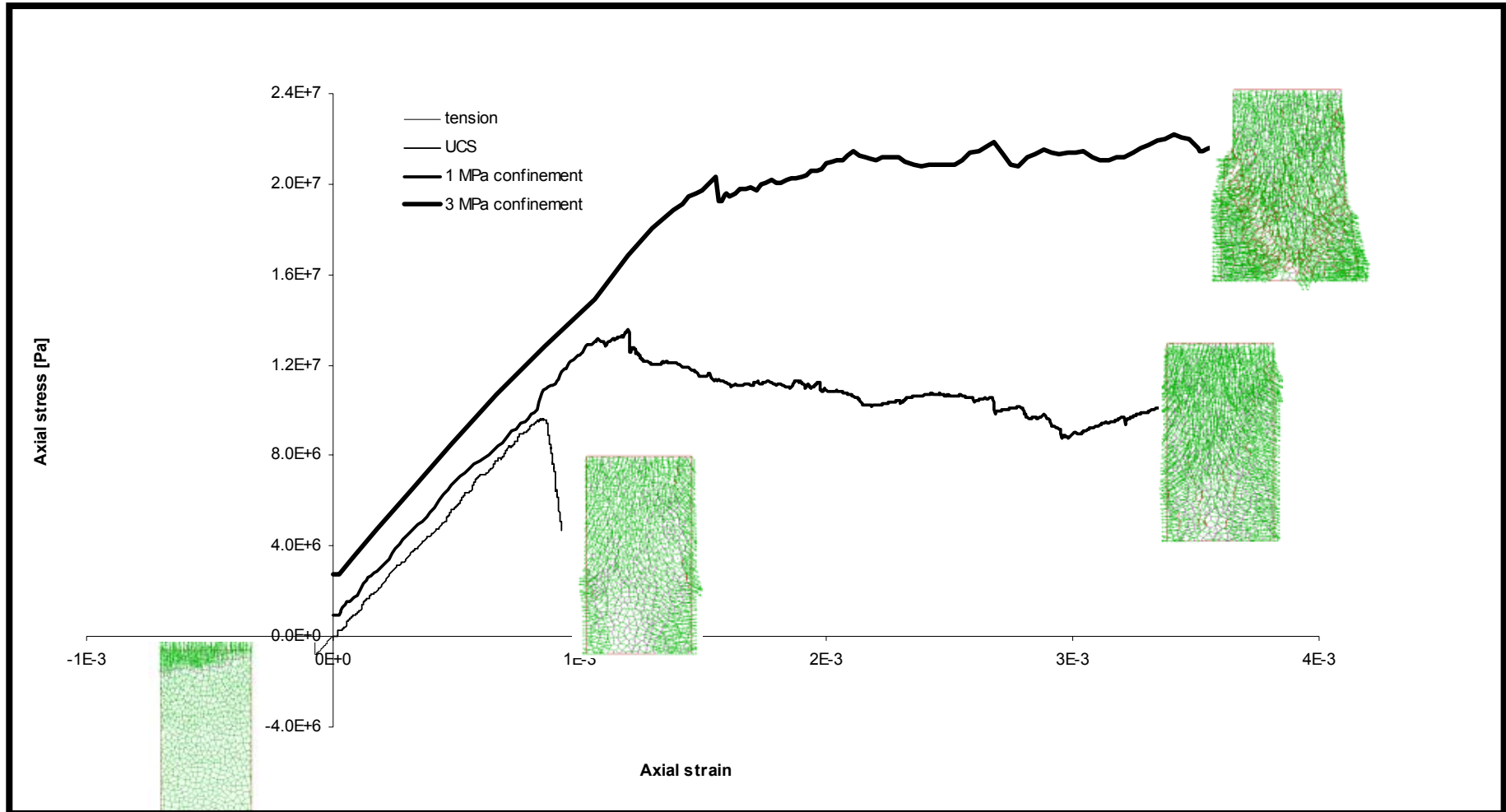
*Laboratory Testing
of 12-inch Cores*



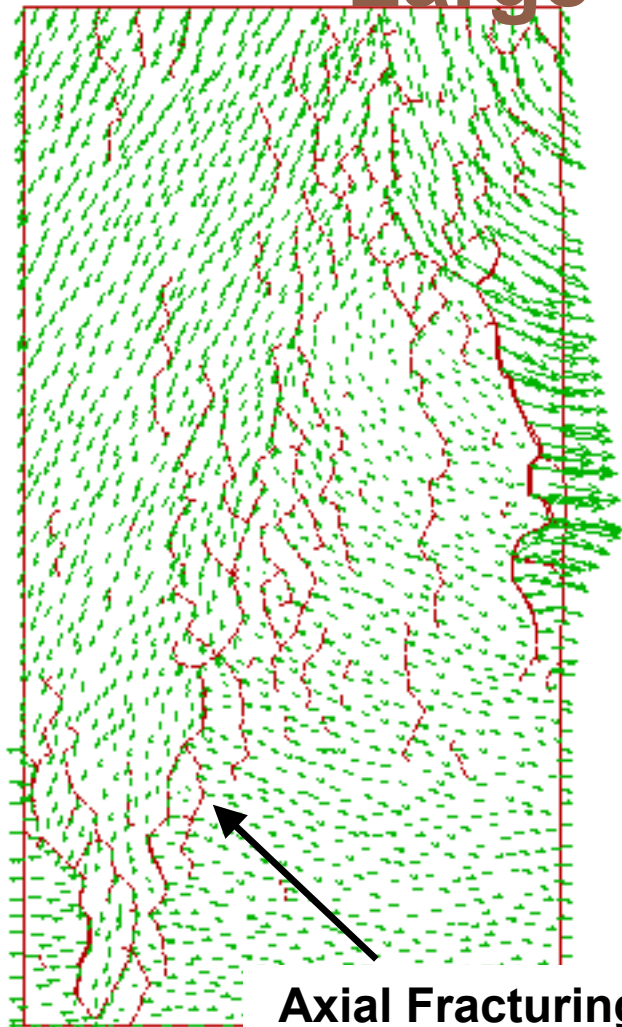
Summary of Compression Data on Large Lithophysal Core Samples and In Situ Tests



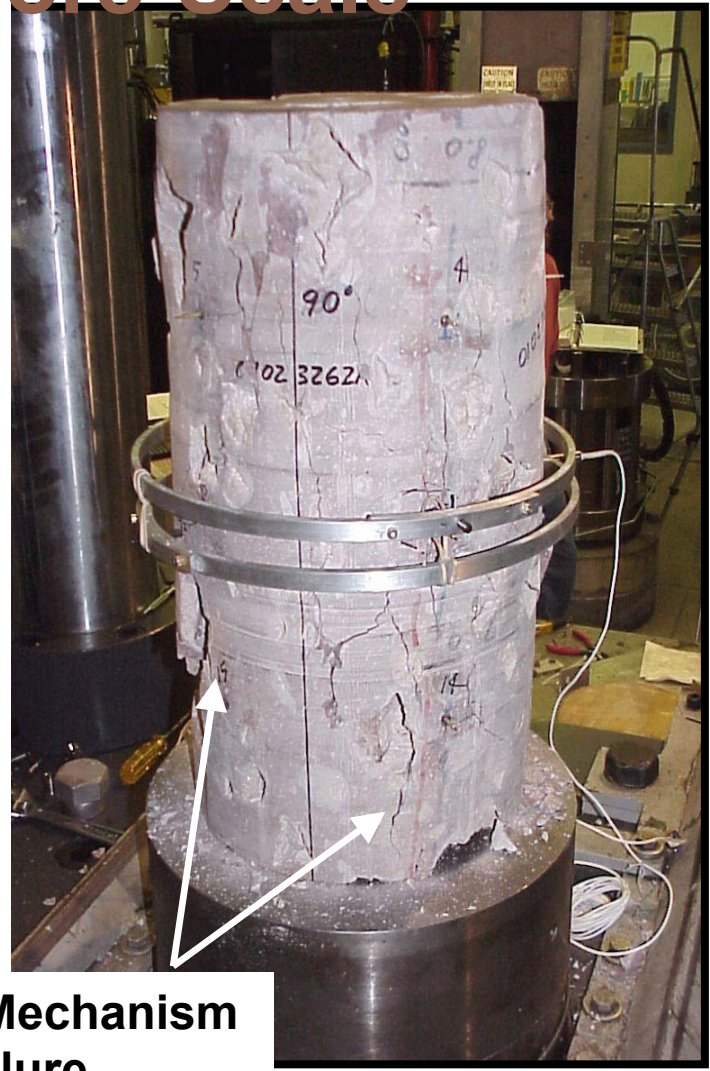
Example of UDEC Model Calibration



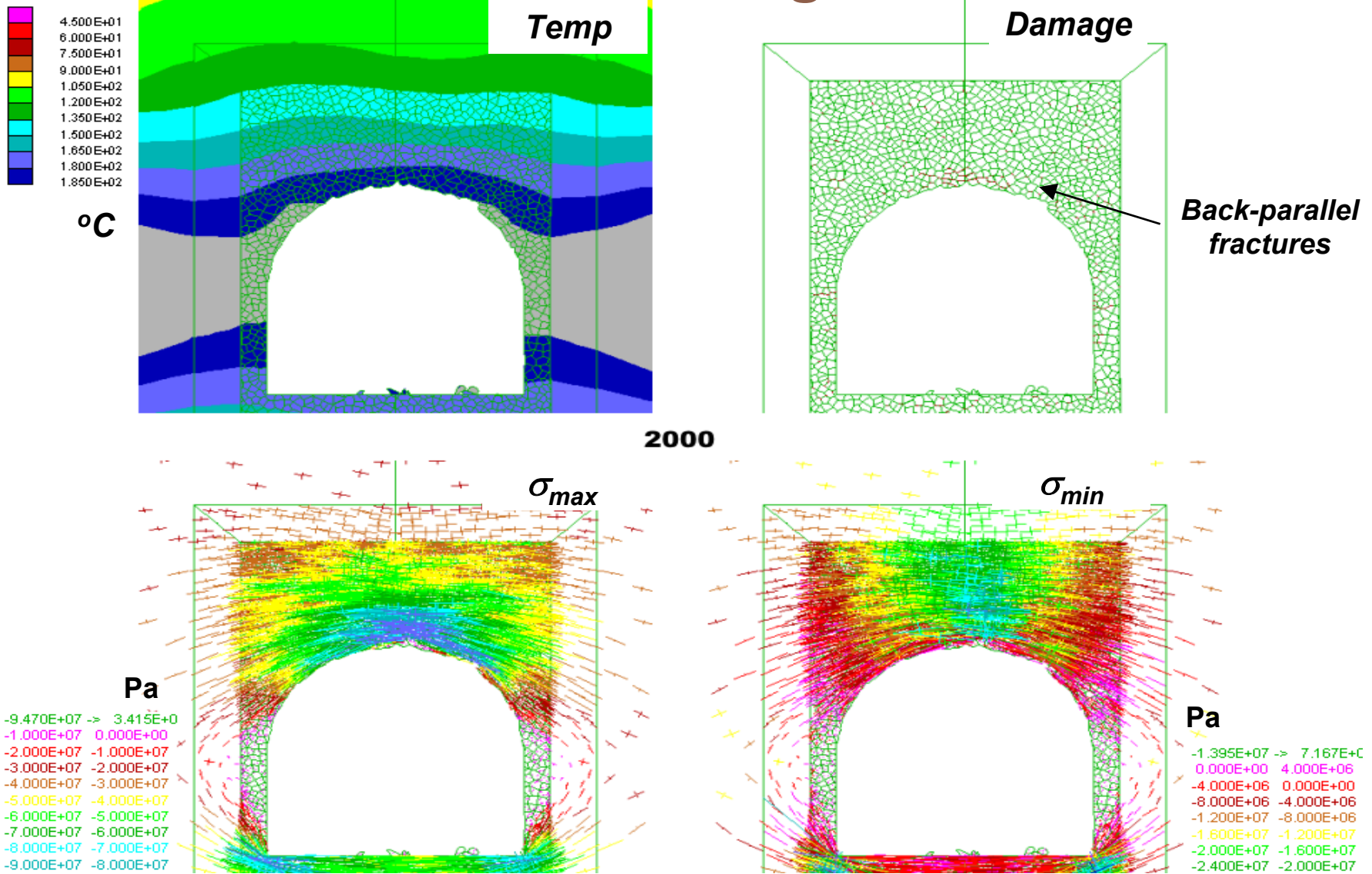
Comparison of Model Failure Mechanism at Large Core-Scale



Axial Fracturing Mechanism of Core Failure

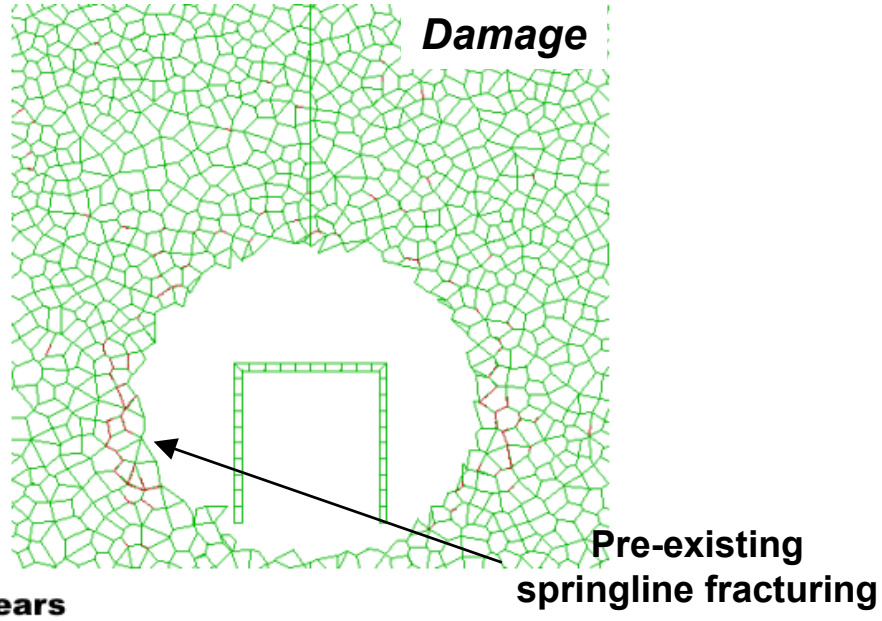
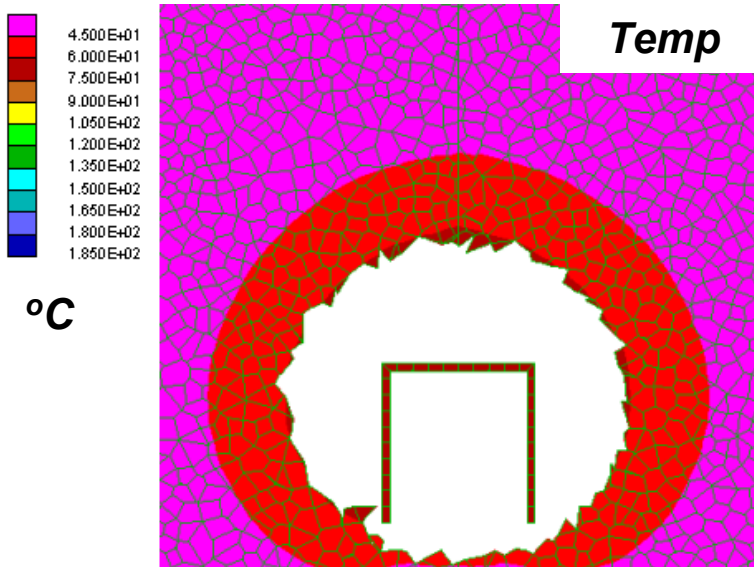


Verification of Model Prediction of Thermal Stress-Induced Roof Slabbing to Drift Scale Test

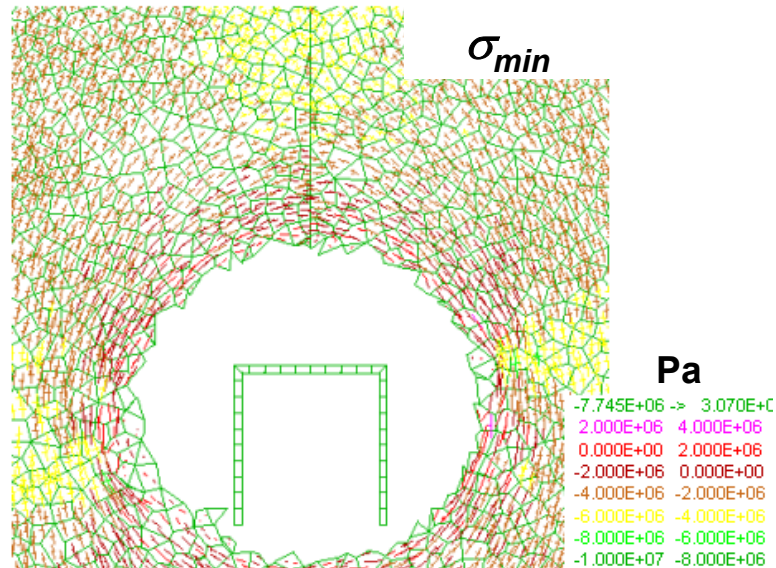
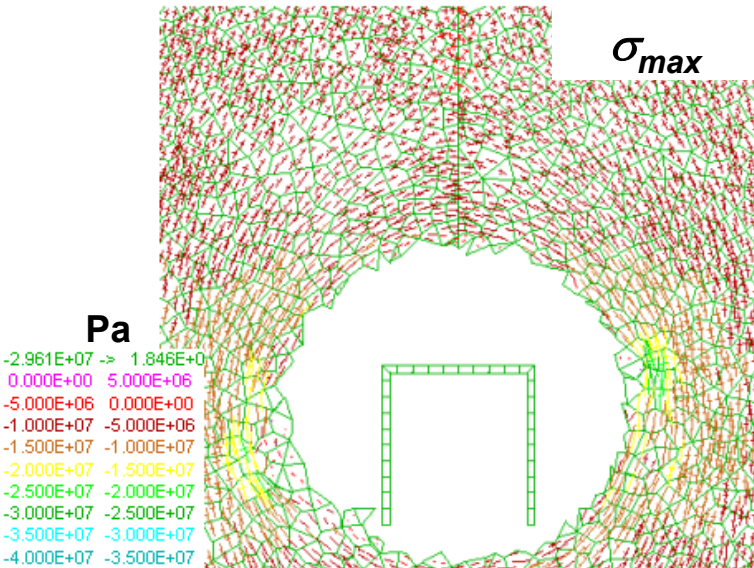


Thermal Drift Degradation Analysis in Lithophysal Rock

- **50 year ventilation**
- **Temperatures imported from NUFT - 1.45 kW/m scenario, peak temperature at drift wall of approx. 135°C reached 20 years (year 70) after closure**
- **Temperatures applied to UDEC lithophysal model in small increments**
- **Allow thermal stressing and fracturing to form naturally with potential gravitationally-induced rockfall**

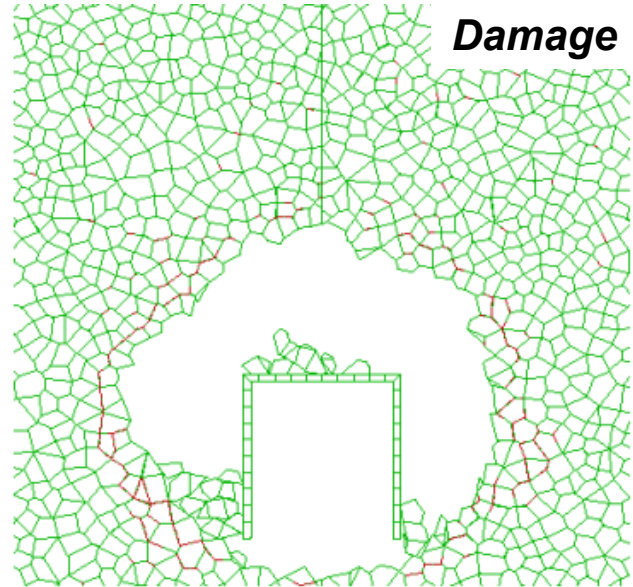
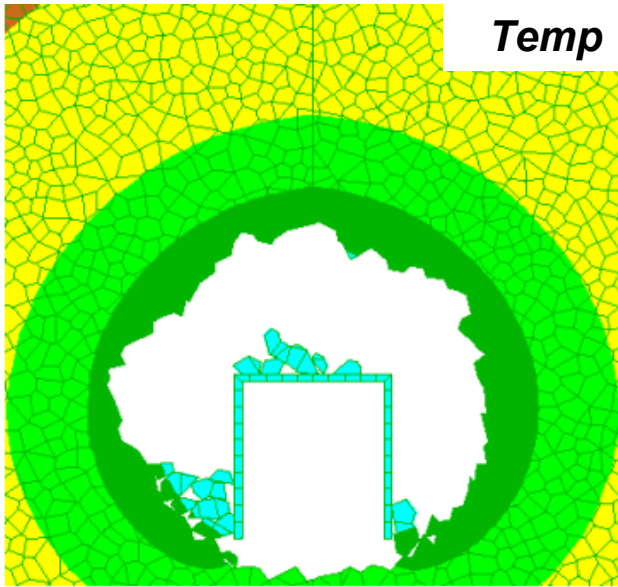
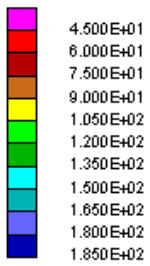


50.2 years

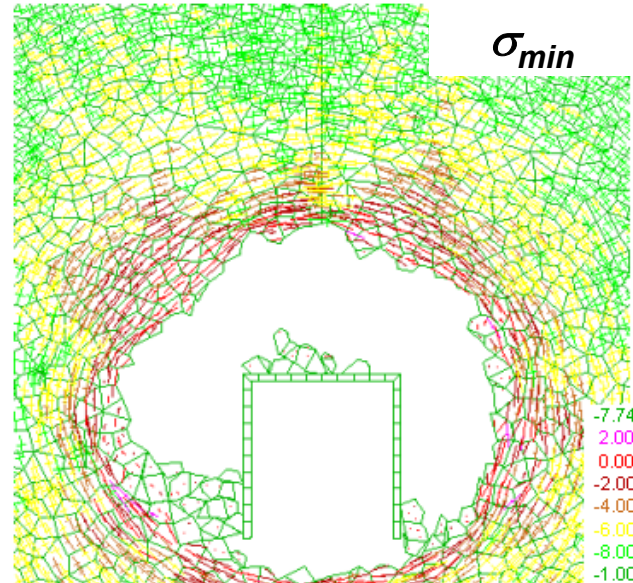
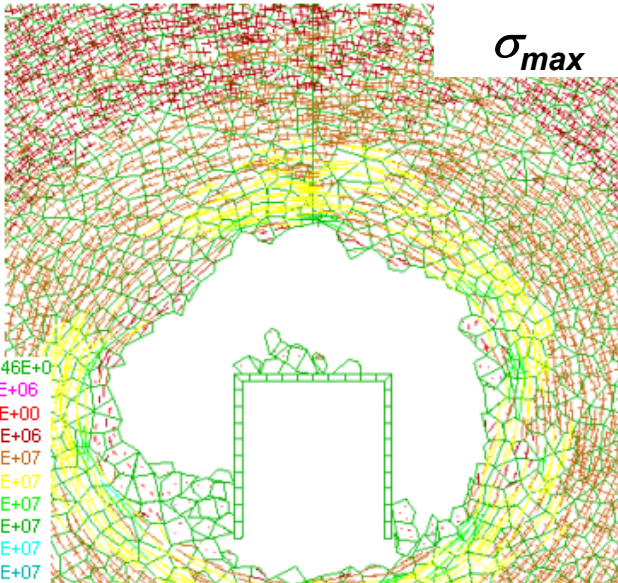


Immediately at end of ventilation





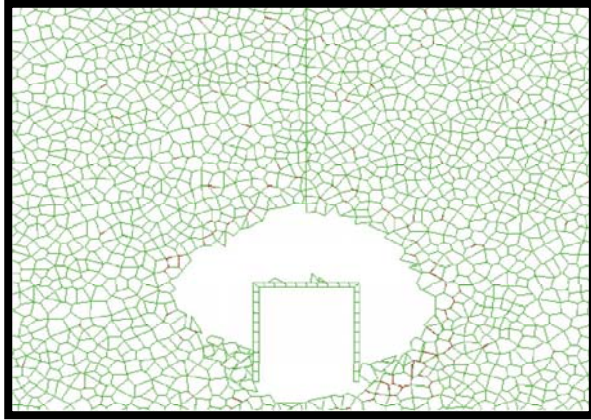
70 years



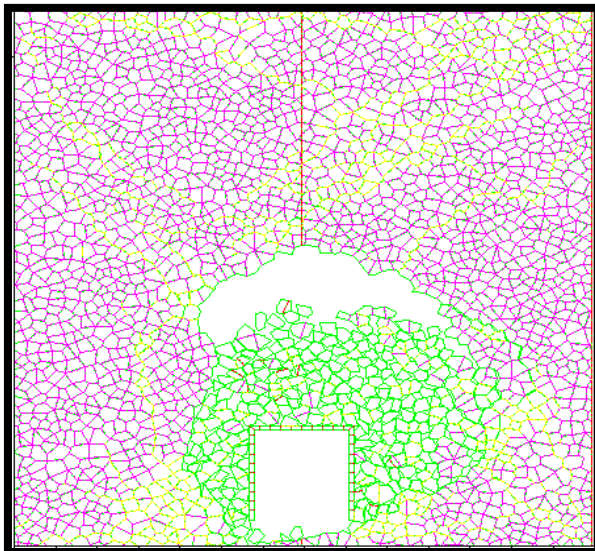
20 years after end of ventilation - peak stress change/damage

Seismic Drift Stability - Lower Lithophysal Unit

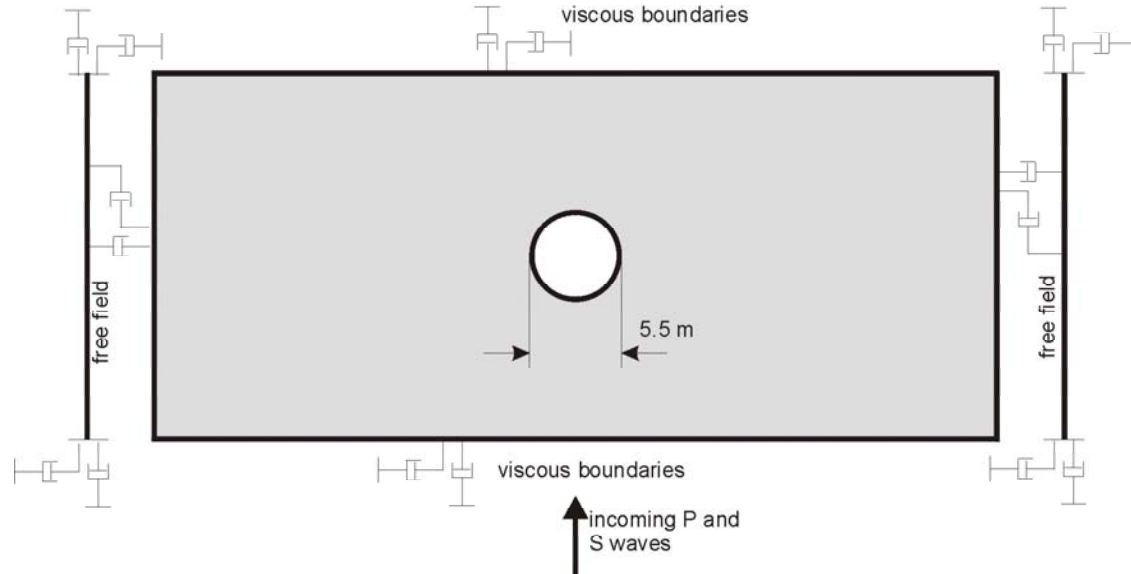
Example Results



5×10^{-4} , unsupported



1×10^{-6} , unsupported



- **Results**
 - 5×10^{-4} - sidewall spalling only
 - 1×10^{-6} and 1×10^{-7} - similar damage - rock failure over drip shield - primary impact is dead weight load on drip shield
- **Damage levels for low prob. events not consistent with observations of no damage in lithophysae in Exploratory Study Facility**

Summary of Drift Degradation Studies

- **Preliminary Conclusions Based on Estimated Ground Motions:**
 - **Non-Lithophysal rock**
 - ◆ Median rock size approx. 0.25 tonne
 - ◆ Relatively small rockfall volume
 - **Lithophysal rock**
 - ◆ Thermal stressing in post-closure results in small displaced volume of rock from springline areas
 - ◆ Pre-closure motion results in loosening of springline for unsupported conditions
 - ◆ Significant damage for 10^{-6} and 10^{-7} motions
 - ◆ Estimated ground motions at 10^{-6} and 10^{-7} not consistent with geological observations of undamaged lithophysae in ESF and Enhanced Characterization of the Repository Block Drift
 - ◆ Time-dependency work currently underway