



FABRICATION & TESTING OF 3M CARBON BLADES

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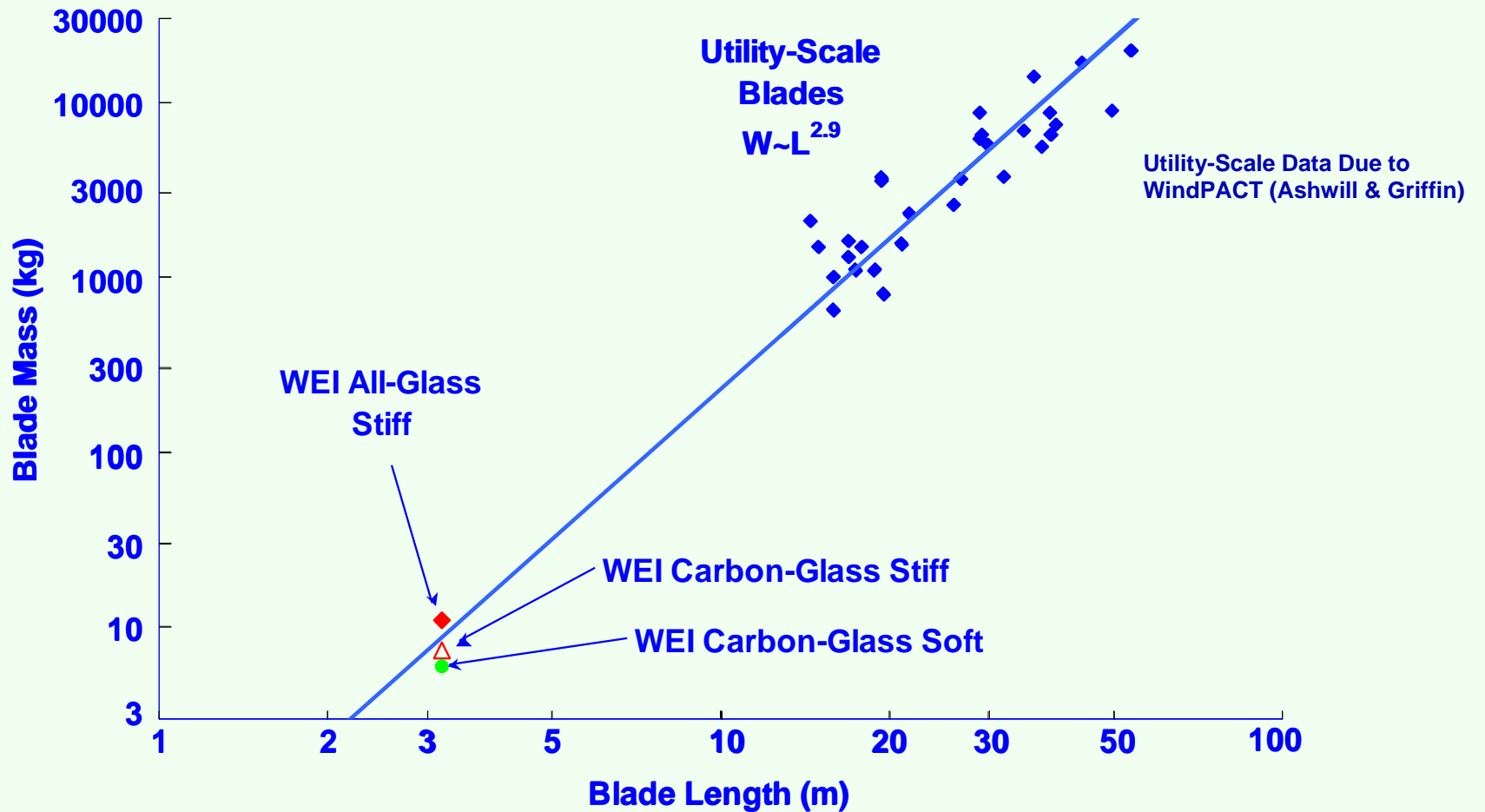
2006 SANDIA BLADE WORKSHOP
APRIL 18-19, 2006
ALBUQUERQUE, NEW MEXICO

ACKNOWLEDGEMENTS

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 - DE-FG02-03ER86175 (SBIR)
 - Dr. Jack Cadogan is technical monitor
 - DE-FG36-03GO13136 (DWT)
 - Drs. Paul Migliore, Jim Green, & Trudy Forsyth, technical monitors
 - Keith Bennett, Administrator
- National Institute for Aviation Research at Wichita State University assisted with fabrication and testing
 - Dr. James Locke was PI at NIAR
 - Dr. Tim Hickey supervised blade testing
 - Sanjay Sharma developed our VARTM process & supervised the shell fabrication
 - Terrence Seet & Michelle Man and others assisted

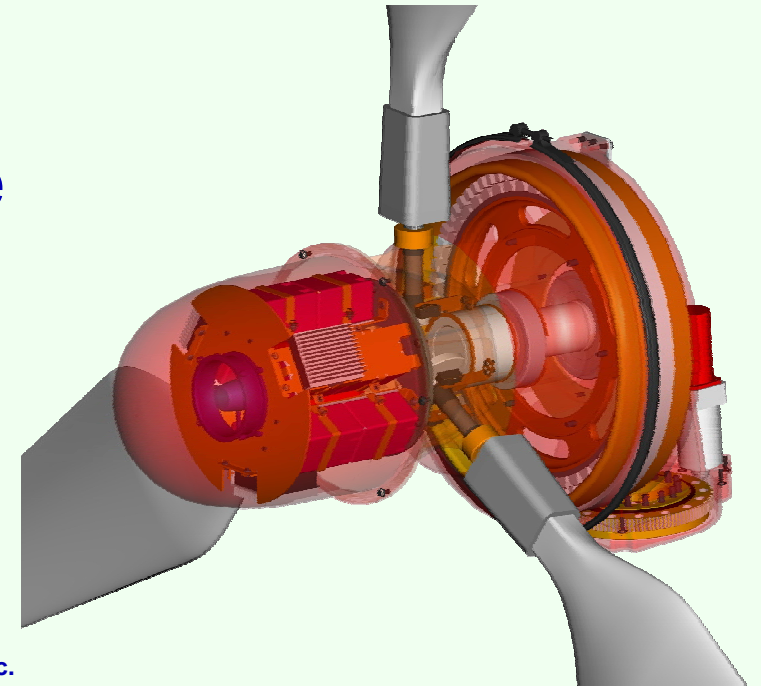


BLADE WEIGHT TRENDS



MOTIVATION FOR THE PROJECT

- Aerodynamically Efficient Blades for Small Turbines
 - Optimized twist & taper
 - High-quality manufacturing → VARTM
- Light-weight designs for pitch-control
 - High-quality structural design
 - Carbon-glass hybrid structure
 - High-quality manufacturing
- Twist-flap coupling



PROJECT ACTIVITIES

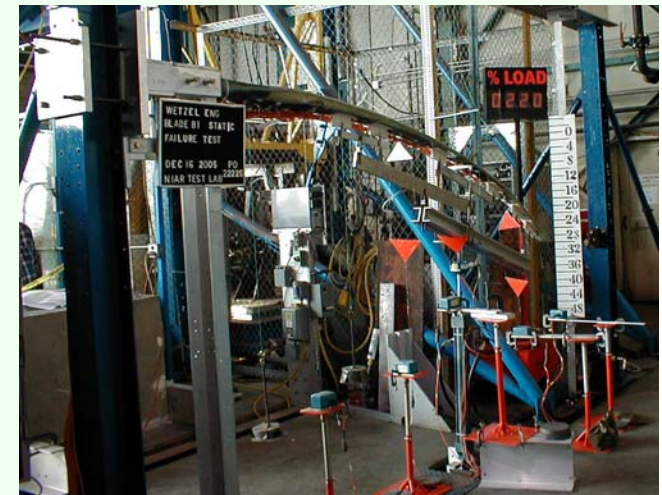
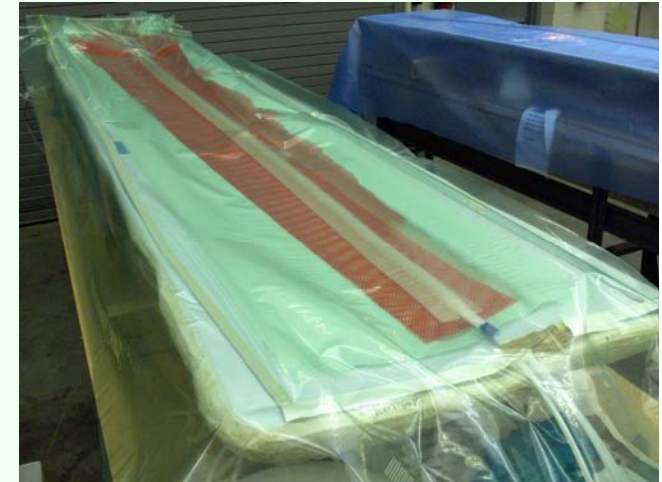
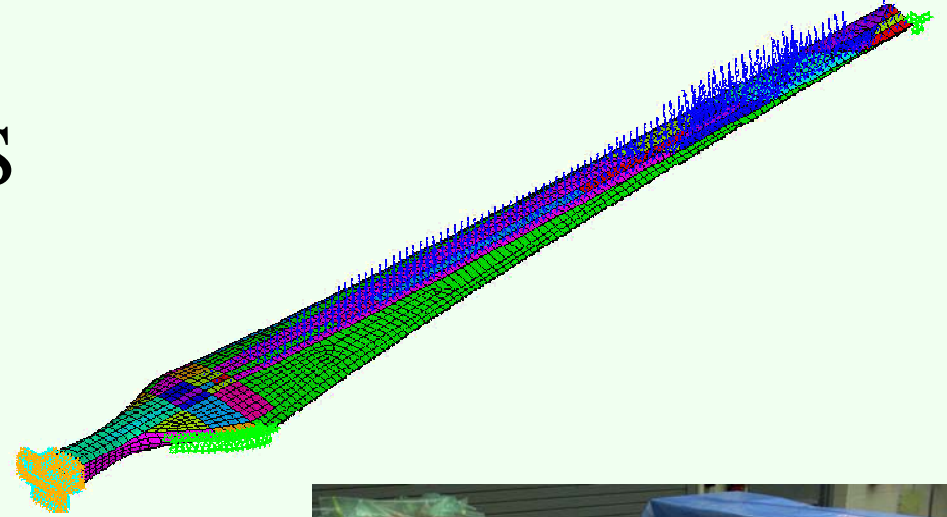
- Blade Design & Analysis

- Aerodynamic Design
- Structural Design (ANSYS)

- Blade Fabrication (VARTM)

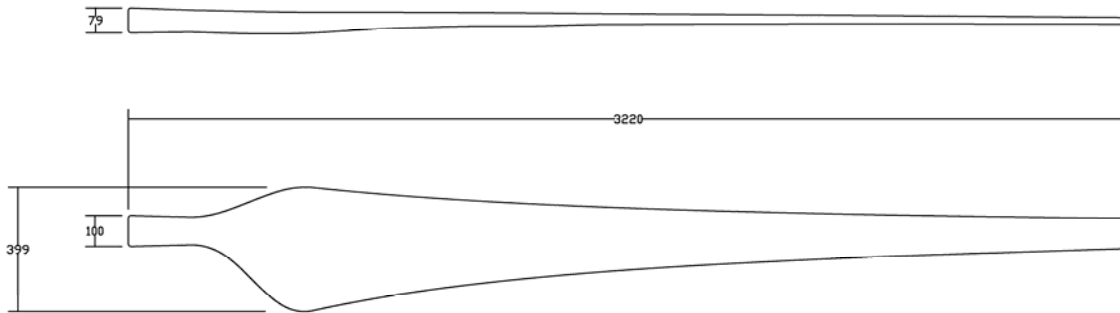
- Blade Testing

- Static (to failure)
- Fatigue (Accelerated Lifetime)

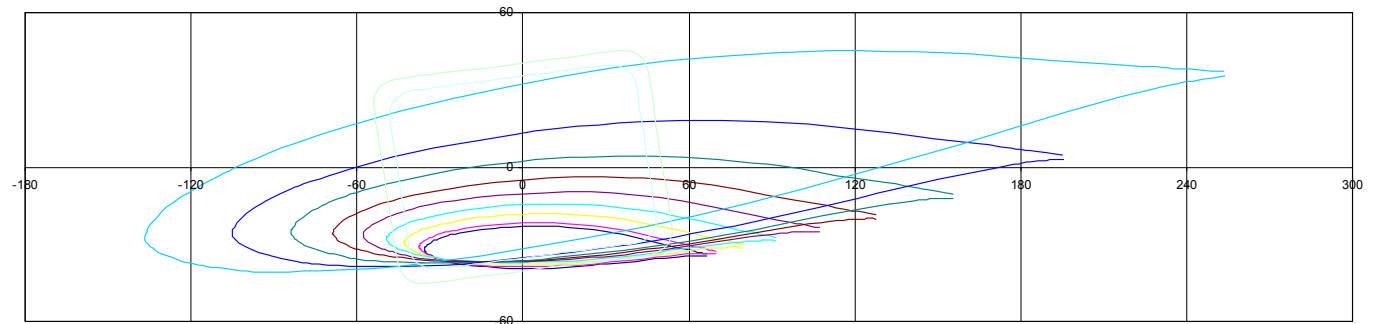


AERODYNAMIC DESIGN

- Maximize energy capture over the entire range of below-rated wind speeds, considering:
 - spanwise distribution of chord length
 - spanwise distribution of twist
 - shaft speed
 - pitch schedule as a function of below-rated wind speed



**NREL S822 Airfoil (16%)
for All Sections**



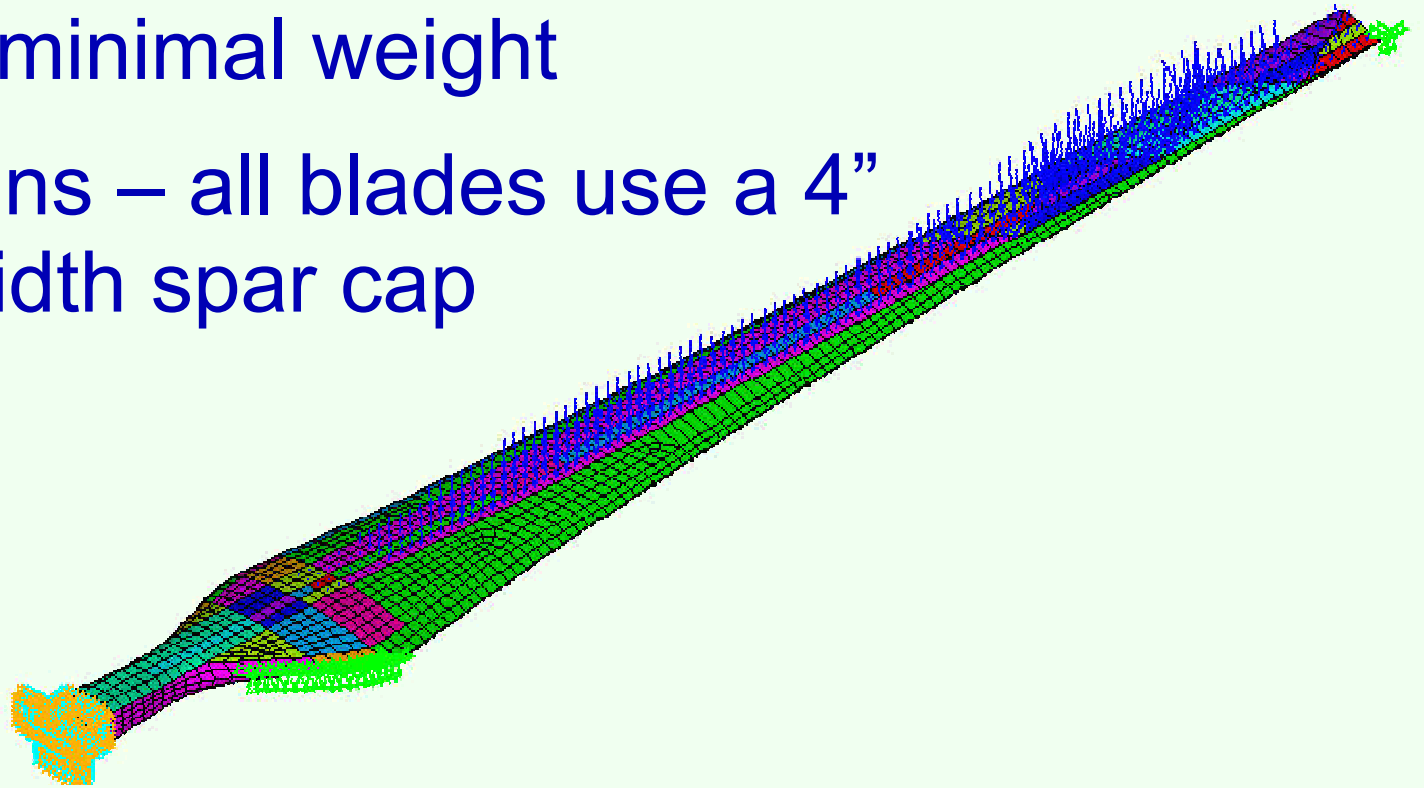
STRUCTURAL DESIGN

Blade	Spar Cap Construction	Skin Fiber Construction	Design Tip Deflection	Designed	Fabricated	Tested
A	100% Glass 0°	100% Glass ±45°	420 mm	Yes	Yes	No
B	100% Carbon 0°	100% Glass ±45°	420 mm	Yes	Yes	Static & Fatigue
C1	92% Carbon off-axis 8% Glass 0/90°	100% Glass ±45°	420 mm	Yes	Yes	Static
C2	Improvement on C1			Yes	In-Progress	Pending
D	92% Carbon of-axis 8% Glass 0/90°	100% Glass off-axis	420 mm	Yes	In-Progress	Pending
E	Carbon/glass hybrid off-axis		420 mm	Yes	In-Progress	Pending
F/H/I1	100% Carbon 0°	100% Glass ±45°	150 mm	Yes	Yes	I1 Static
I2	Improvement on I1			Yes	Yes	Static
G	100% Carbon 0°	100% Carbon ±45°	420 mm	Yes	Yes	Pending

- Clamshell Design with Spar Caps Integrated into the Shells
- C- or O-channel shear web bonded between shells in a secondary process

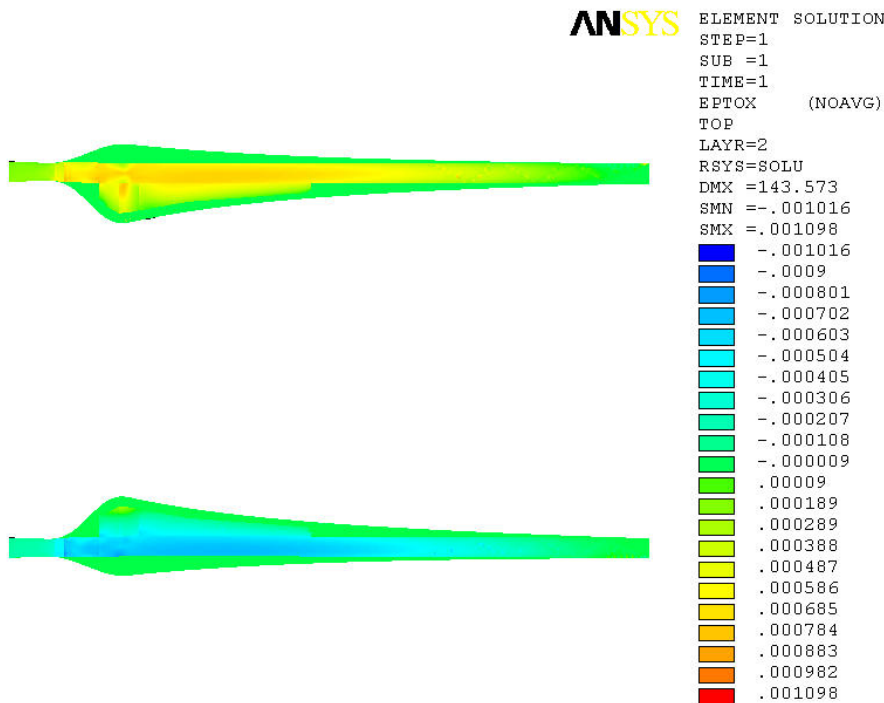
STRUCTURAL DESIGN

- Structural Optimization Pointed to a Spar Cap Tapered in Width & Thickness
- Fabricating Tapered Width was a Nuisance and saved minimal weight
- Final Designs – all blades use a 4” constant-width spar cap

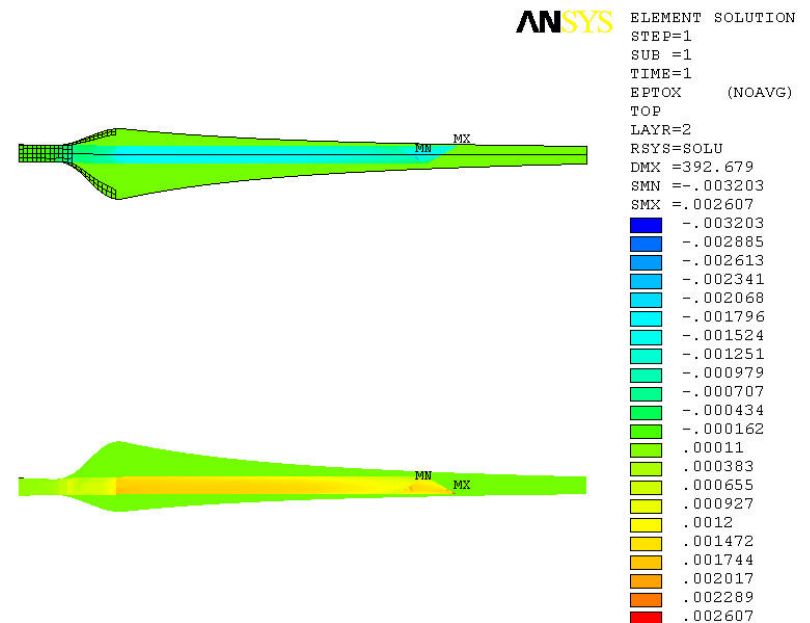


STRUCTURAL DESIGN

- Design Requirements:
 - Carbon fiber strain $< 0.3\%$
 - Soft Blades at margin, stiff blades extra margin
 - 20-year fatigue life \rightarrow all blades \sim infinite life
 - Buckling LF $> 2.1 \rightarrow$ uncoupled blades OK



Blade I, Axial Strain $< 0.11\%$



Blade B, Axial Strain $< 0.32\%$

BLADE FABRICATION

- VARTM shells in Clamshell Tools
- Tools from CNC routed mandrels
- 13 osy Carbon Uni
 - 68k tow Fortafil fiber
 - High fiber volume fraction
 - Low permeability!
- 12 and 17 osy Glass $\pm 45^\circ$
 - PPG Hybon 2022 fibers

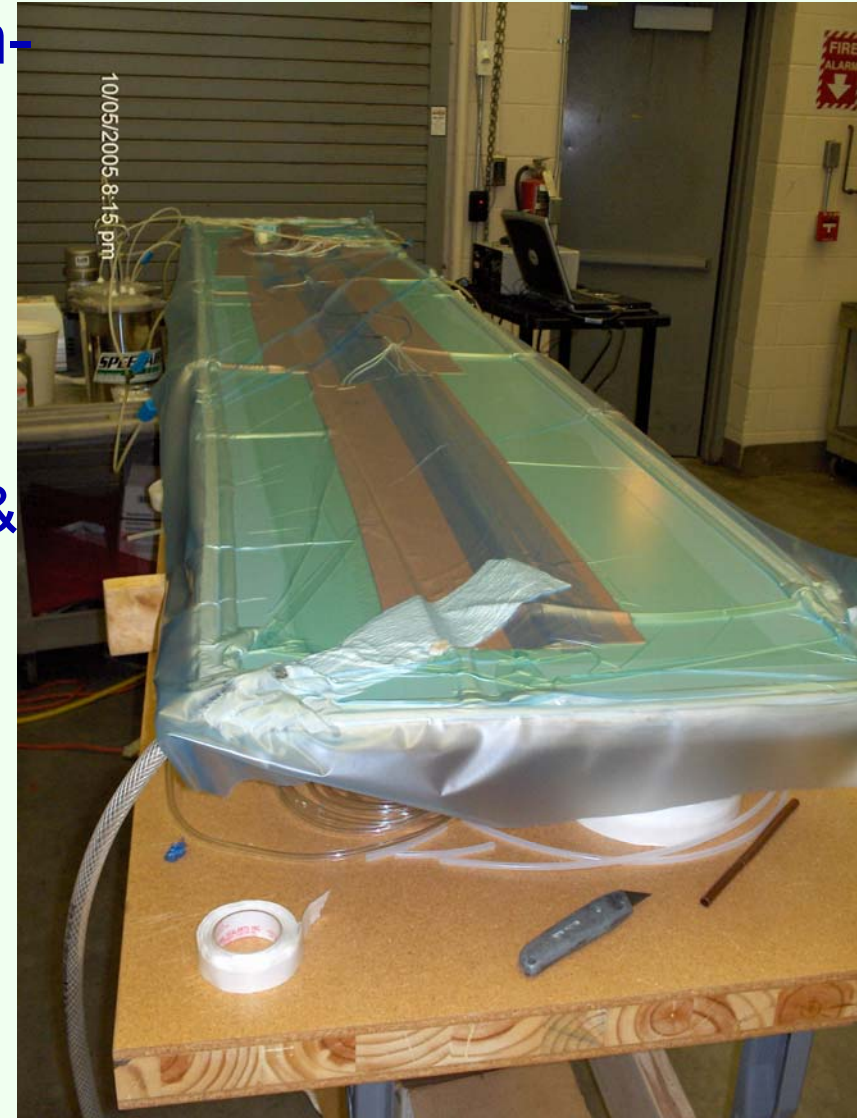


- We had no choice in carbon material at the time we purchased!!



BLADE FABRICATION

- Shells are infused using vacuum-assisted resin transfer molding
 - Full vacuum
 - 0-25 psi back pressure
 - JeffCo 1401-21(18) resin
 - Experimented with number, type, & placement of infusion ports & channels and vacuum ports.
 - Heated with Si rubber heaters during infusion and cure cycle
 - 4-10 minutes to infuse one shell



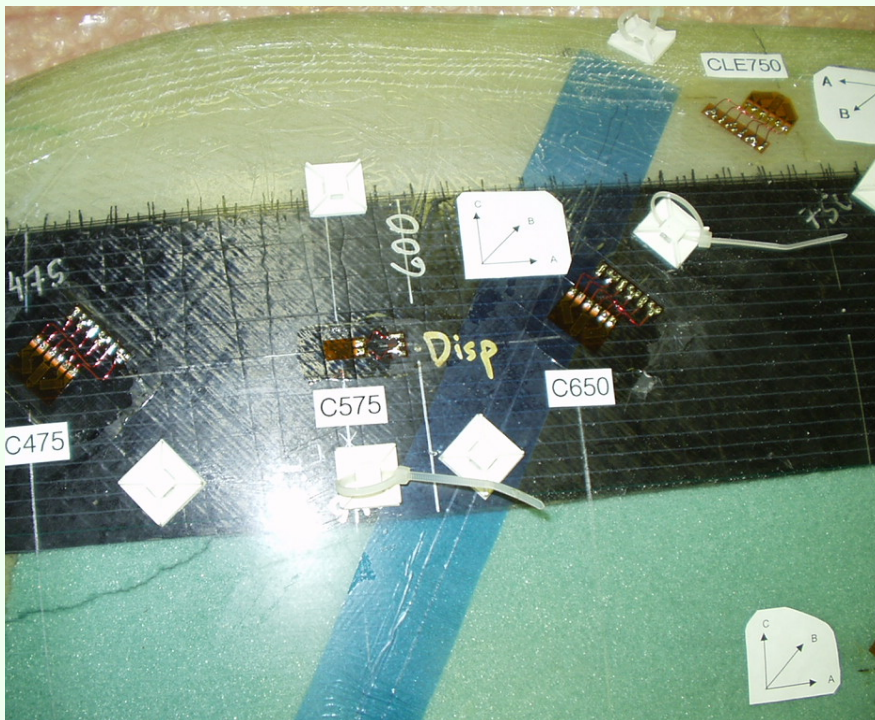
BLADE FABRICATION

- Cured shells were demolded & trimmed
- Shear webs were fabricated using wet layup
- Shells and webs were bonded in a secondary process
- Finished blades were post-cured at 200F for 8 hours in an oven
- Blades were instrumented for testing



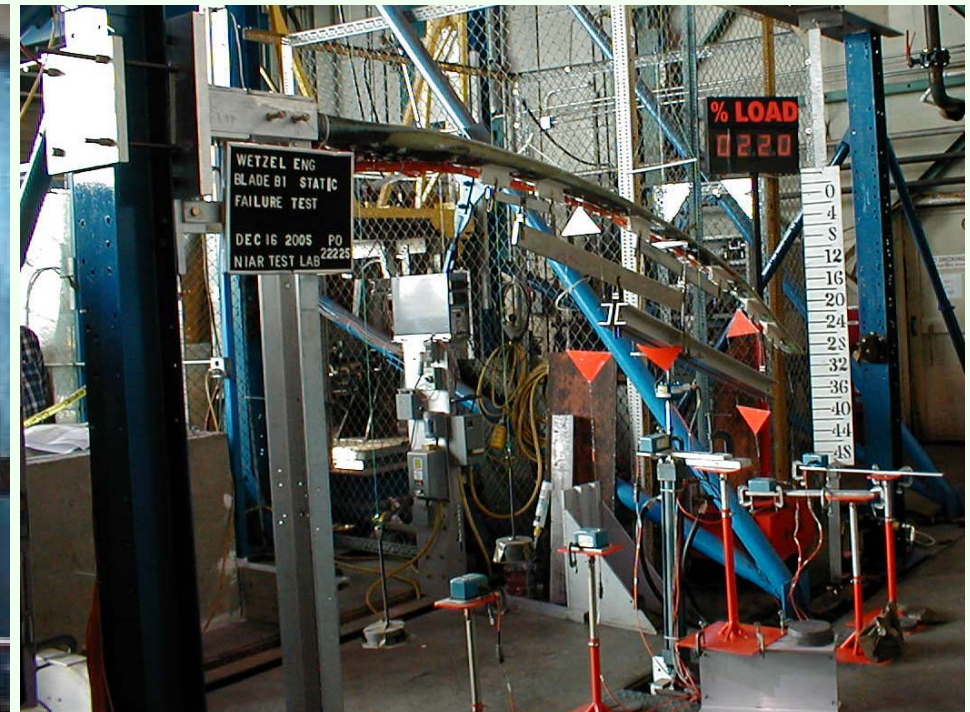
STRUCTURAL TESTING

- NIAR/Raytheon 46000-sf Test Center
- 30-36 channels of strain per blade
- Axial gauges and 3-element rosettes
- 6-point Whiffle Tree Static Load
- Displacement at 6 Spanwise Stations



STRUCTURAL TESTING

Blade	Peak Carbon Fiber Strain at 100% Proof Load		Tip Deflection at 100% Proof Load		Buckling LF		Tip Twist at 100% Proof Load	
	Design	Test	Design	Test	Design (Linear)	Test	Design	Test
I1	0.11%	0.10%	147	191	2.56	2.30	-	-
I2	0.11%	0.10%	147	162	3.10	2.90	-	-
B1	0.32%	0.27%	414	373	2.53	2.26	-	-
C1	0.33%	0.33%	375	318	2.20	1.65	7°	1.5°

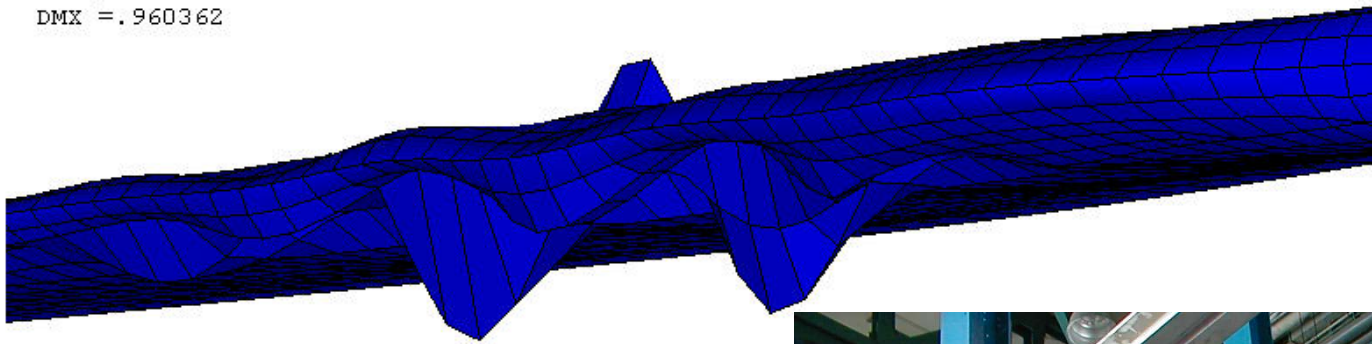


STRUCTURAL TESTING

DISPLACEMENT

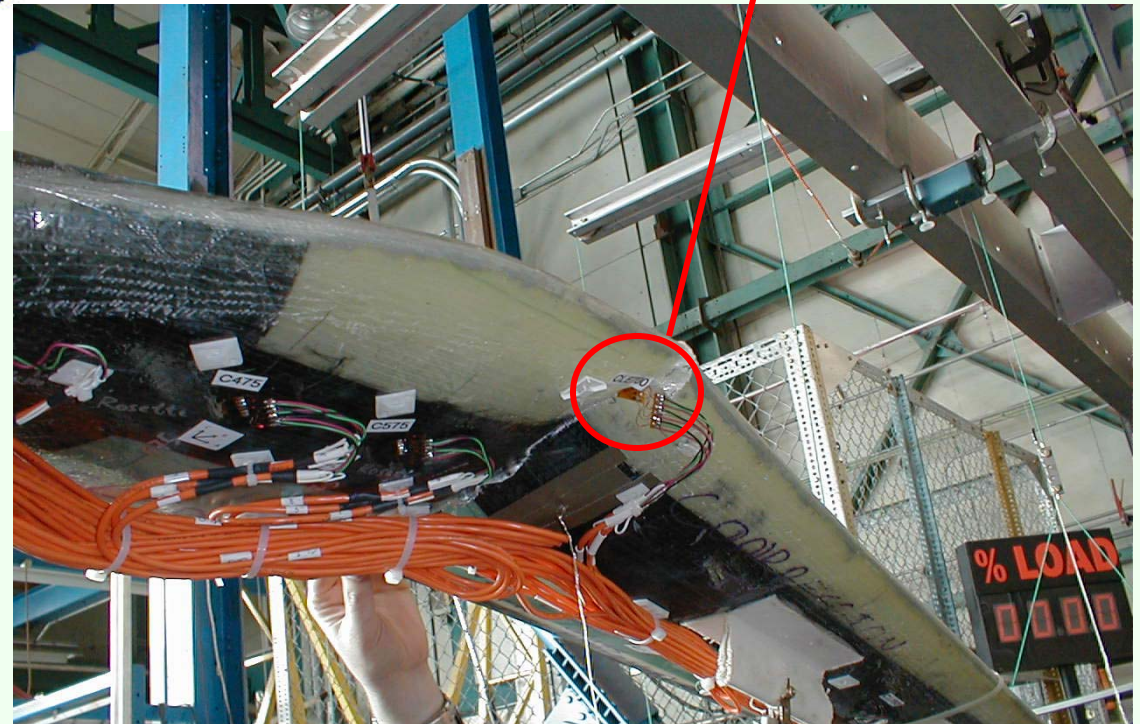
STEP=1
SUB =1
FREQ=2.528
DMX =.960362

ANSYS



Rosette Placed to Capture Buckling

- Buckling Initiated Exactly where predicted in all static tests
- Test Load Factors were close to linear prediction in uncoupled blades



FUTURE PLANS

- Remodeling Blades B, C, & I “as fabricated” to verify against test results
- Completing designs of Blades D & E (twist-bend coupled designs)
- Fabricating & Testing Blades D & E to demonstrate significant twist-bend coupling
- Working with warm vacuum prepreg products that do not require autoclaves

