High Thermal Conductivity Graphite Foam Reinforced Polymer Composites

by

J. Klett*, L. Klett, J. Strizak, M. Williams, A. McMillian Oak Ridge National Laboratory (423) 574-5220, klettjw@ornl.gov <u>www.ms.ornl.gov/cimtech/cimtech.html</u>

> Juan Valencia, Tom Creeden Concurrent Technologies Corporation

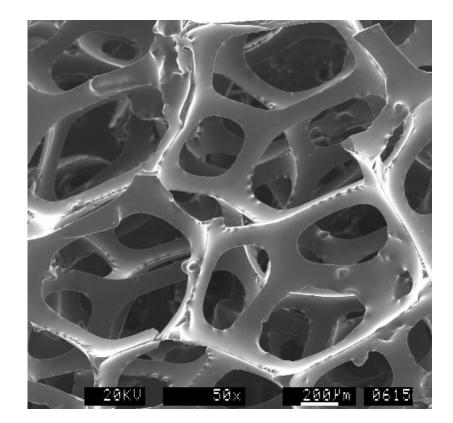
Keywords: Graphite Foam, Thermal Conductivity, Thermal Management





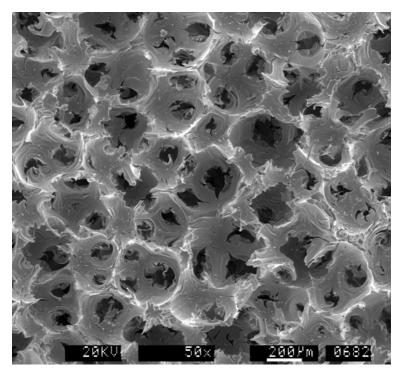
Typical Carbon Foams

- Made from amorphous carbons
- More recently made from pitches and mesophases
- ➤ 5-25% dense
- Thermal insulators
 - o $\kappa < 10 \text{ W/m} \cdot \text{K}$
- Strengths similar to honeycomb materials
- Ability to absorb tremendous amounts of impact energy



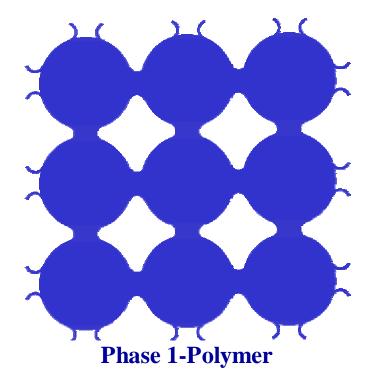
ORNL Mesophase-Derived Graphitic Foam

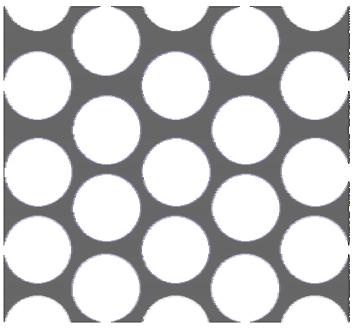
- Graphitic ligaments
 - Graphite-like properties (high κ , E, σ) along ligaments.
- Dimensionally stable, low CTE
- No out-gassing
- Open porosity
- Excellent thermal management material
 - Bulk conductivities greater than 150 W/m·K
 - Natural 3-D reinforcement for composites
 - Should yield composites with conductivities equivalent to aluminum



Unique Structure For a Composite

- Failure mechanisms not understood
- > Thermal effects not understood
- Shrinkage upon cure might damage structure





Phase 2-Foam

Materials Selection

- Selected various polymer candidates
 - o Desired varying properties
 - \rightarrow Polycyanate resin, (RS-14)
 - Low viscosity, high toughness, high temperature stability, low shrinkage during cure
 - \rightarrow Epoxy, (Standard epoxy for mounting samples for polishing)
 - Low viscosity, excellent interfacial bonding to graphites, room temp cure
 - → Polyester, (Bondo Fiberglass automotive grade resin)
 - Cheap (automotive uses), room temp cure, moderate viscosity
 - → Phenolic, (Durite SC-1008, Borden Chemical)
 - Low viscosity, high temperature stability, can convert to carbon
 - → SMJ Carbon (AFRL/PRSM), (proprietary pitch-type deposit)
 - High temperature applications, high thermal conductivity
 - → Aluminum, (MMCC, Aluminum/Silicon alloy pressure cast method)
 - Tough, metallic, high thermal conductivity

Testing

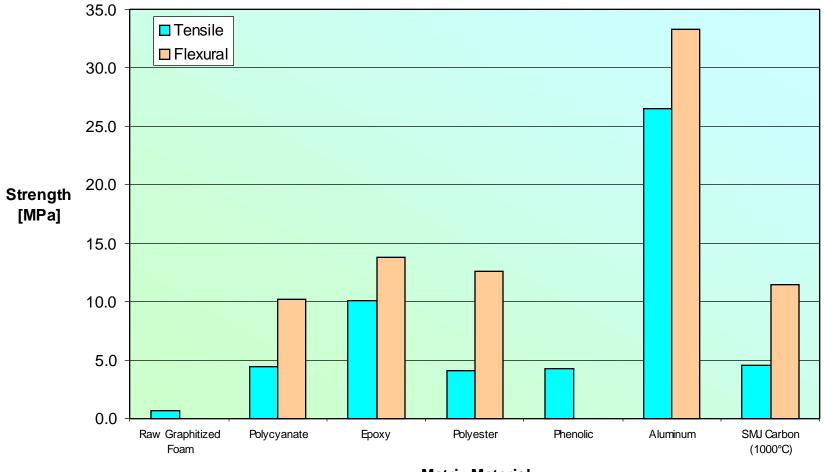
- Mechanical testing
 - o Flexural Strength
 - \rightarrow 4 point bend, specimens 0.2 x 0.5 x 4-in.
 - o Tensile Strength
 - \rightarrow specimens 0.2 x 0.5 x 4-in.
 - Compressive Strength
 - \rightarrow specimens 0.5 x 0.5-in.
- > Analysis
 - Thermal Conductivity
 - \rightarrow specimens 0.5 x 0.5-in.
 - Fracture Surfaces (tensile)
 - → SEM

Flexural and Tensile Strength

			Tensile	Flexural
	Density		Strength	Strength
Matrix	[g/cm ³]	% Dense	MPa (Psi)	MPa (Psi)
Raw Graphitized Foam	0.54		0.69 (100)	
Polycyanate	1.37	88%	4.5 (653)	10.2 (1475)
Ероху	1.31	84%	10.1 (1460)	13.7 (1990)
Polyester	1.33	85%	4.1 (595)	12.6 (1830)
Phenolic	1.00	64%	4.3 (624)	
Aluminum	2.34	89%	26.5 (3850)	33.3 (4830)
SMJ Carbon (1000°C)	1.34	63%	4.6 (660)	11.5 (1660)

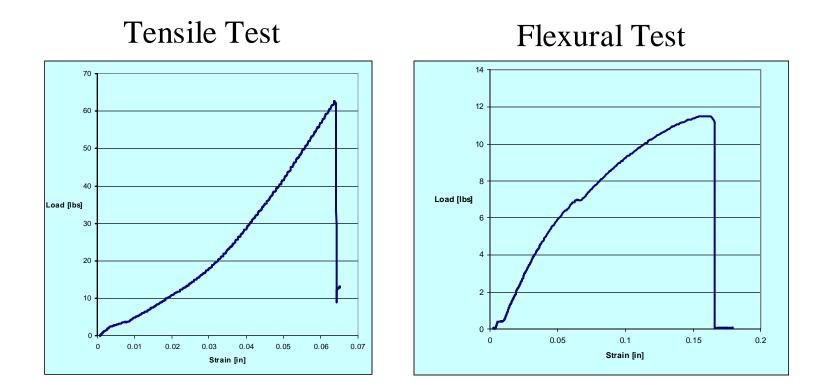
Flexural strength greater than tensile strength indicates weibull effects and therefore strength is flaw limiting (expected).

Flexural and Tensile Strength



Matrix Material

Stress-Strain Behavior



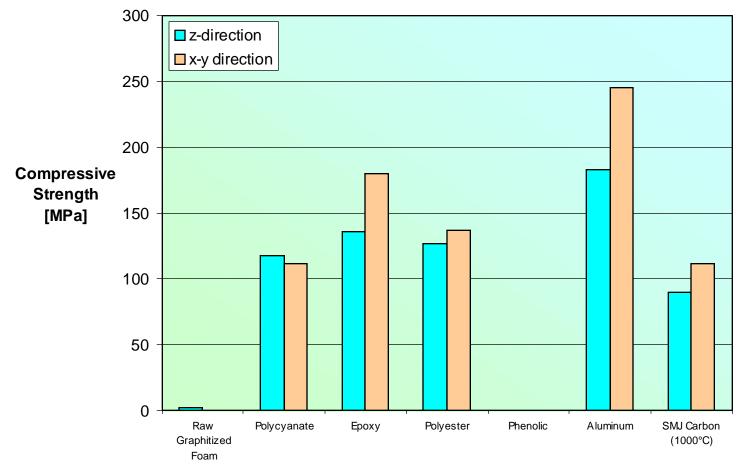
Brittle fracture not usually seen in carbon/polymer composites

Compressive Strengths

			Compressive Strength		
	Density		z-direction	x-y direction	
Matrix	[g/cm ³]	% Dense	MPa (Psi)	MPa (Psi)	
Raw Graphitized Foam	0.54		2.1 (305)		
Polycyanate	1.37	88%	118 (17,100)	112 (16,200)	
Ероху	1.31	84%	136 (19,800)	180 (26,100)	
Polyester	1.33	85%	127 (18,400)	137 (19,900)	
Phenolic	1.00	64%			
Aluminum	2.34	89%	183 (26,500)	245 (36,500)	
SMJ Carbon (1000°C)	1.34	63%	89 (13,000)	112 (16,200)	

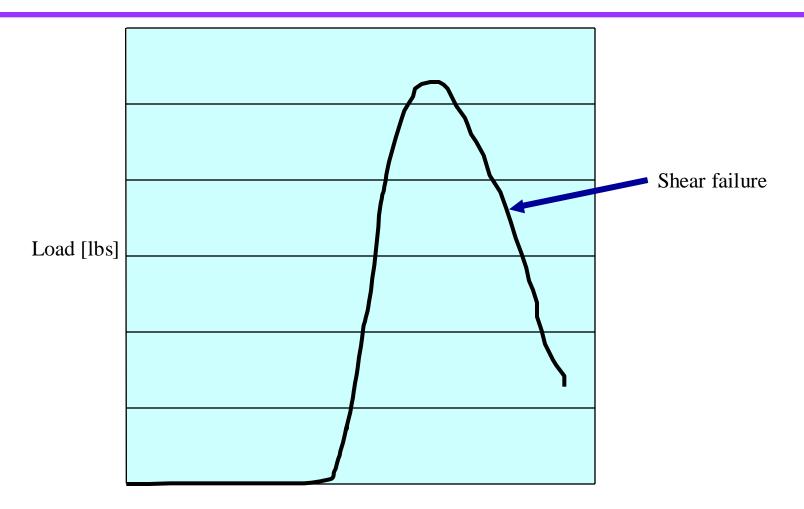
 Compressive strengths are dramatically higher than flexural and tensile strengths (typical carbon/polymer composites do not exhibit this large of a difference)

Compressive Strengths



Matrix Material

Stress-Strain Behavior - Compression



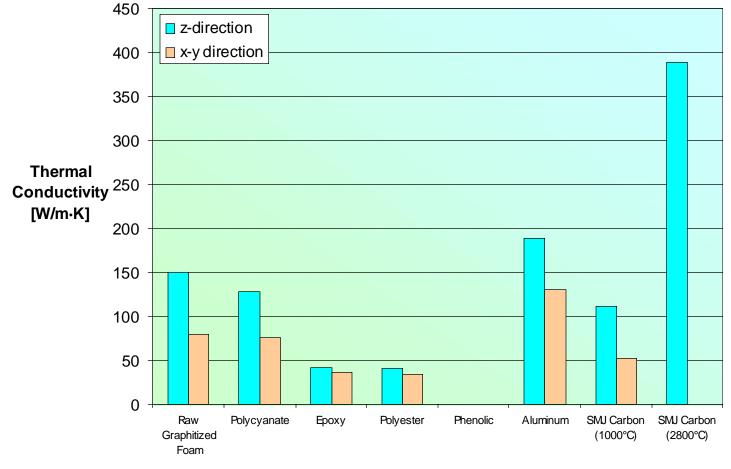


Thermal Conductivity

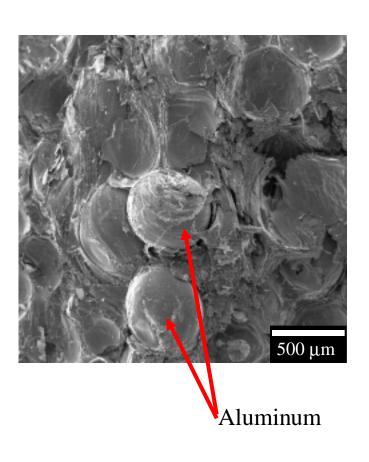
	Density		W/m·K	
Matrix	[g/cm ³]	% Dense	z-direction	x-y direction
Raw Graphitized Foam	0.54		150	80
Polycyanate	1.37	88%	129	76
Ероху	1.31	84%	42	36
Polyester	1.33	85%	40	34
Phenolic	1.00	64%		
Aluminum	2.34	89%	189	130
SMJ Carbon (1000°C)	1.34	63%	112	52
SMJ Carbon (2800°C)	1.29	58%	389	

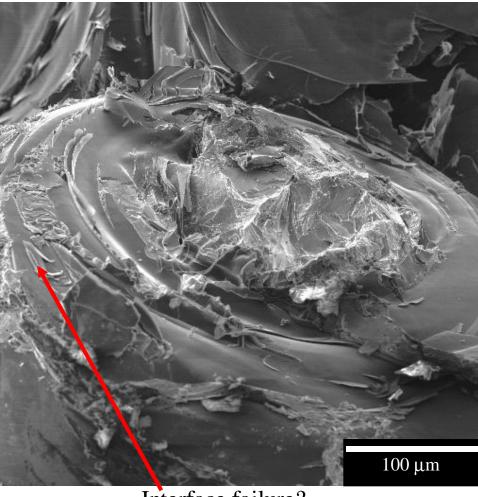
Thermal Conductivity

Thermal Conductivity

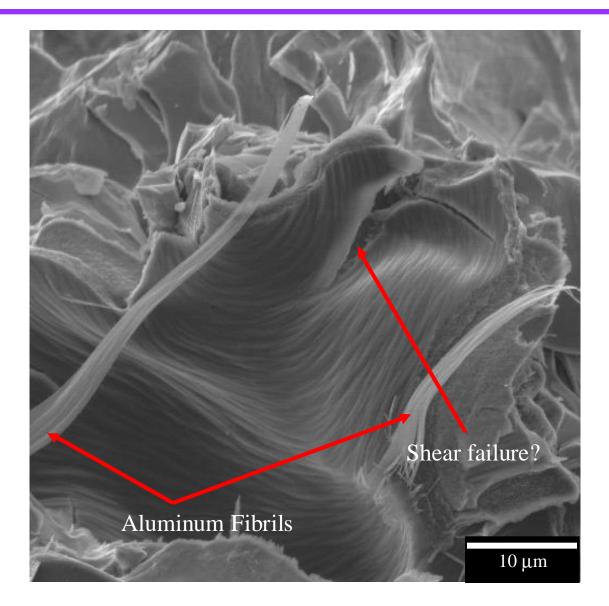


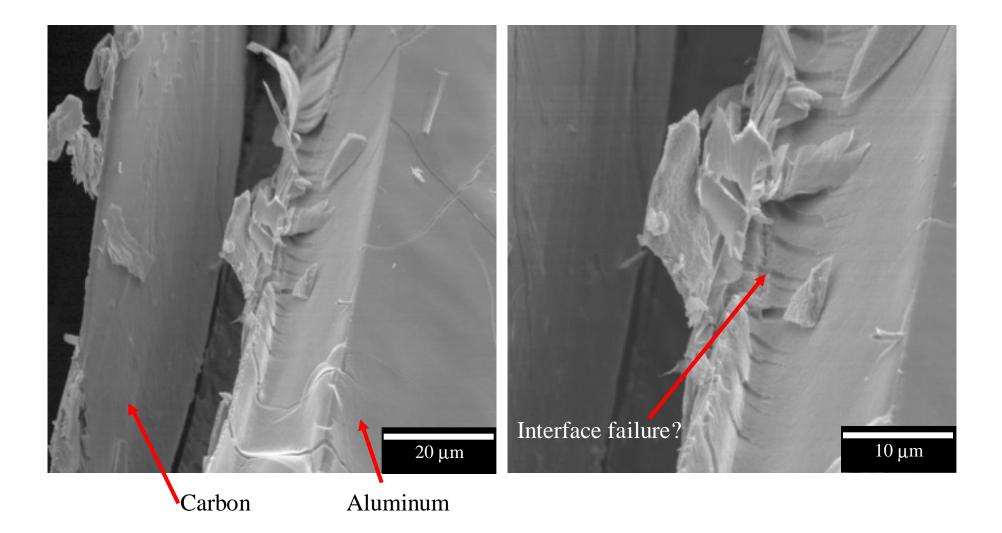
Matrix Material

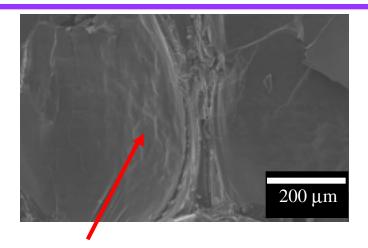




Interface failure?

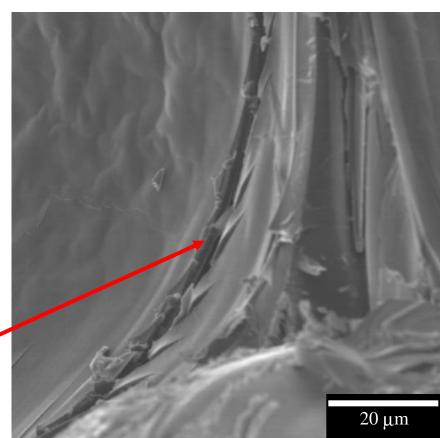


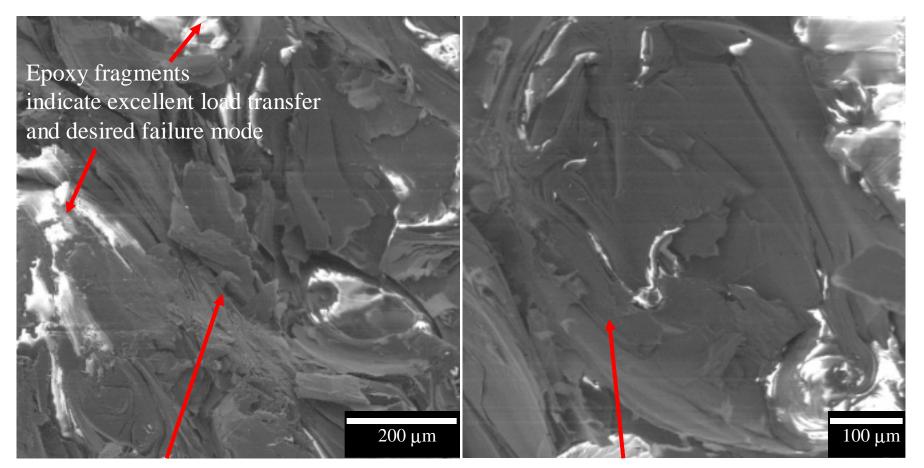




Deformation of cell wall indicates aluminum-carbide formation or good interface

Shear failure of cell wall • indicates good load transfer



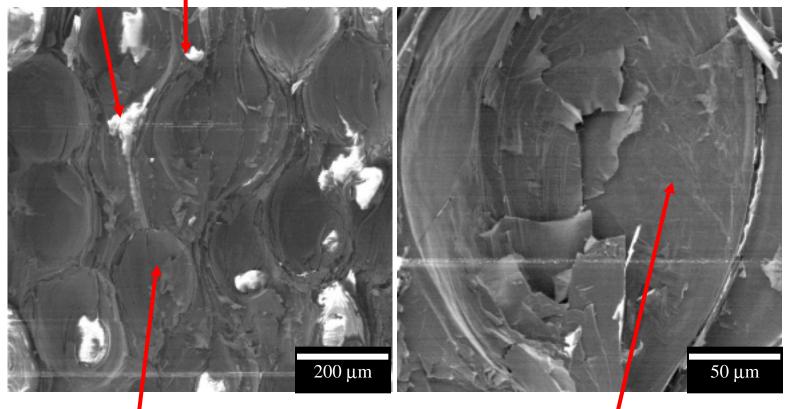


Fracture of cell wall indicates excellent interface

Fracture of cell wall indicates excellent load transfer

Tensile Fracture Surface – Polyester/Foam

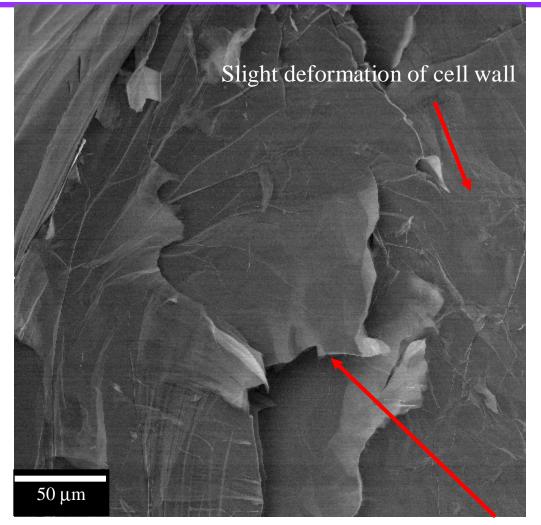
Polyester fragments indicate excellent load transfer



Slight deformation of cell wall indicates excellent interface

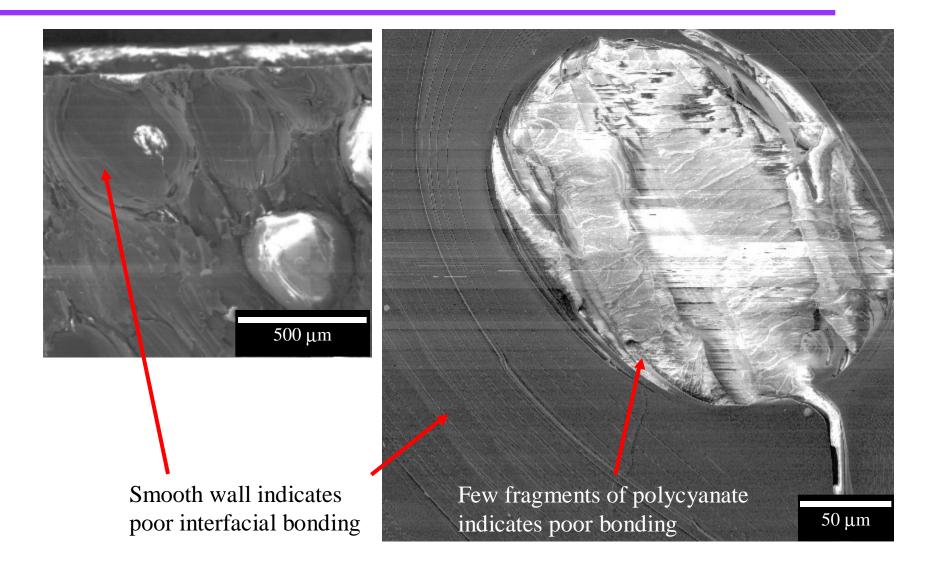
Slight fracture of cell wall indicates good load transfer

Tensile Fracture Surface – Polyester/Foam

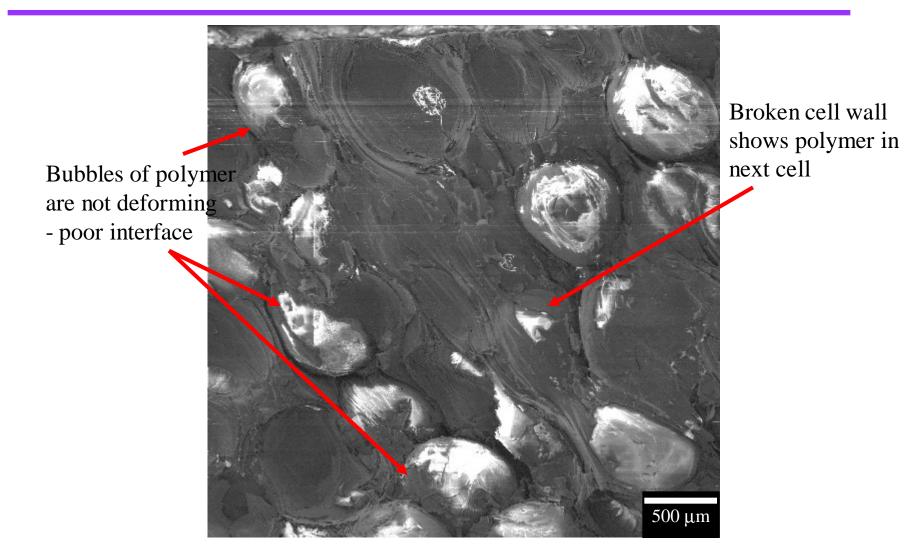


Shear failure of cell wall indicates excellent load transfer

Tensile Fracture Surface – Polycyanate/Foam

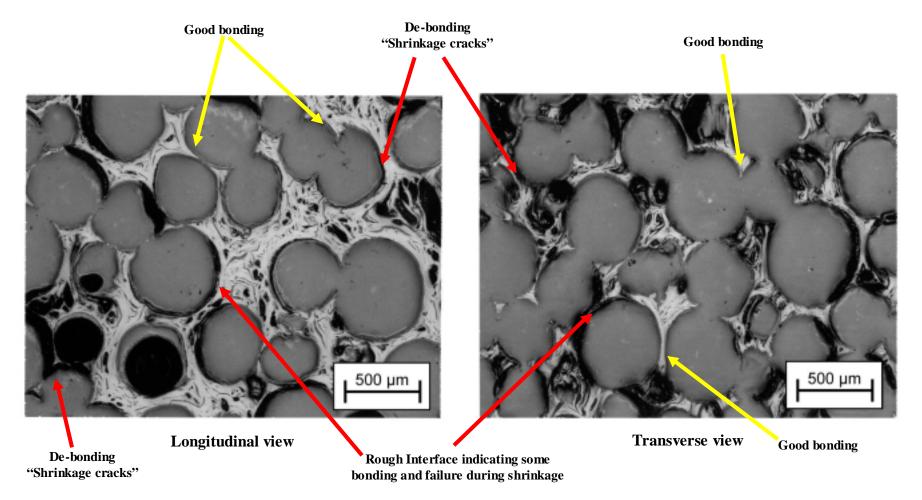


Tensile Fracture Surface – Polycyanate/Foam



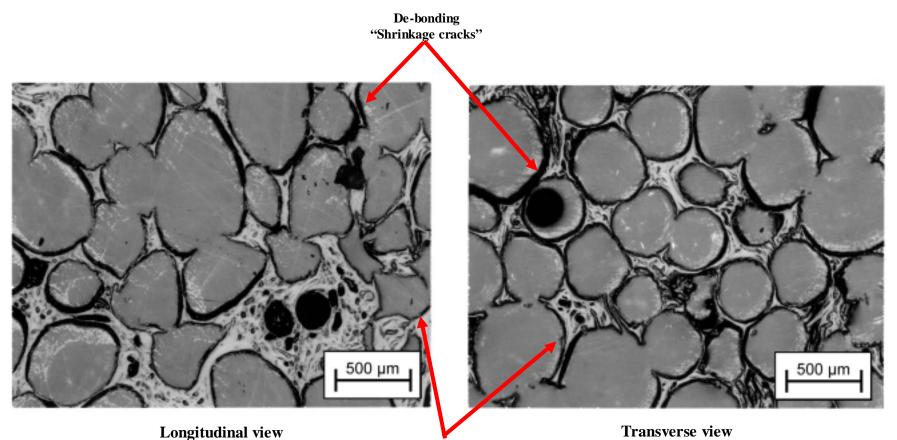
Optical Analysis – Epoxy/Foam

Mostly good bonding with some de-bonding present



Optical Analysis – Polyester/Foam

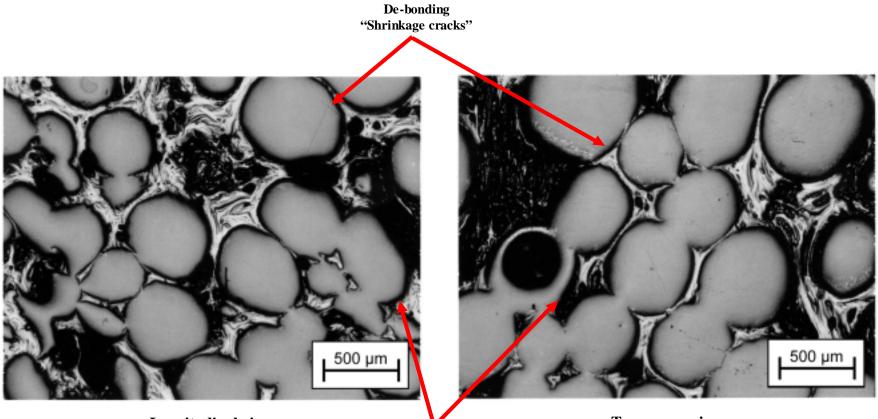
> Mostly poor bonding with very little adhesion to foam



Rough Interface indicating some bonding and failure during shrinkage

Optical Analysis – Polycyanate/Foam

> Mostly poor bonding with very little adhesion to foam



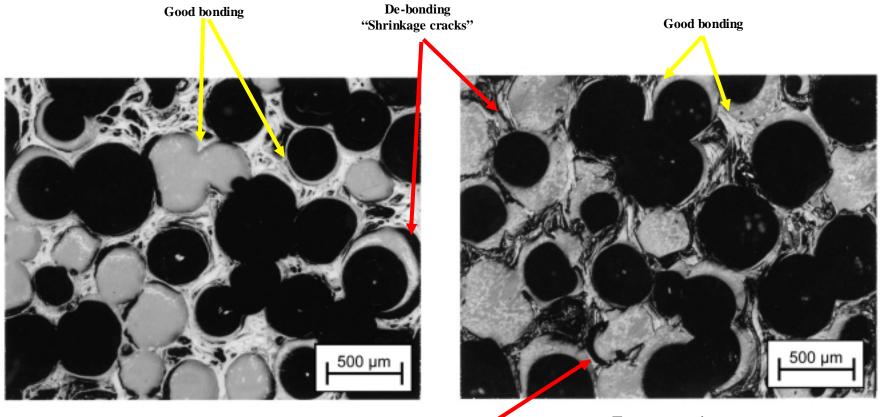
Longitudinal view

Transverse view

Clean Interface indicating little bonding and now failure during shrinkage

Optical Analysis – Phenolic/Foam

> Mostly good bonding with some de-bonding/shrinkage cracks.



Longitudinal view

De-bonding "Shrinkage cracks"

Transverse view

Thermal Stability – Polycyanate/Foam



Foam/Polycyanate after 50 sec

Conclusions - Mechanical

- > Wetting and adhesion is a key factor!
- > Epoxy and phenolic resins seem to exhibit best interfacial bond while polycyanate and polyester exhibit a weak interface.
 - Epoxies typically bond better to carbons
 - Used as a sizing agent with carbon fibers
- Shrinkage during processing (cure or cooling) is causing samples with weak interface to pull away from foam leaving two non-connected continuous phases.
- Unique co-continuous structure may be leading to very dramatic differences in flexural/tensile strengths and compressive strengths.

Conclusions - Thermal

- A lower thermal conductivity in some samples may be due to the damage of cell structure due to the shrinkage of the matrix with good bonding present, thereby damaging structure.
- > It is unsure if the interface is affecting thermal conductivity directly through heat transfer or indirectly through failure mechanisms.
- > Obviously, there are more questions than answers.

Conclusions

- It was noticed that the samples which were densified in a series of cycles (phenolic and SMJ carbon) did not densify as well (64%) as the samples densified in one cycle (polyester, epoxy, polycyanate) (85%).
- > Yet they experienced very similar tensile and flexural strengths.
- The process of only laying down a small layer allows the polymer to shrink around the ligaments rather than pull away as the polymer cures and/or cools.
- Building up these layers to a denser composite may result in better reinforcement of the foams than a "one-shot" densification.

Conclusions

- This was tried with a polyimide (LaRC-SI) which is soluble in a solvent by Engineered Ceramics, Inc.
- The polymer is applied, dried, cured with as many as 8 cycles needed to densify the sample.
- After achieving densifications comparable to the polycyanates the flexural strength was reported to be 80 MPa, compared to 10 MPa for the samples densified in one cycle.
- Perhaps, this is the best method to densify carbon foams for structural reinforcement.

Future

- Study interfacial bonding
 - Sizing agents (epoxies and other polymers)
 - Surface treatments (oxidation)
- > GOAL
 - Show relationship between enhanced interfacial bond and tensile/flexural/compressive properties.
 - Determine if interfacial bond will affect thermal conductivity directly.
 - Develop fundamental understanding of failure mechanisms of this unique co-continuous two-phase system.

Acknowledgements

Research sponsored by the U. S. Department of Energy, Laboratory Directors Research and Development program of the Oak Ridge National Laboratory

and

The National Center for Excellence in Metalworking Technology, operated by Concurrent Technologies Corporation under contract N00140-92-C-BC49 to the U.S. Navy as part of the U.S. Navy manufacturing Science and Technology Program

> Special thanks to Claudia Walls Oak Ridge National Laboratory

> > Chin-Chin Tee University of Tennessee