Worst-case scenario tools for Verification and Validation

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Outline

- Problem setting: elliptic equations with uncertain input parameters
- Worst-Case Scenario approach: mathematical formulation and some examples
- On the Validation of a WCS model
- Solution strategy based on perturbation techniques: application to uncertainty in coeffs, forcing terms and boundary conds
- Verification issues
- Conclusions



Model problem – linear elliptic equation

$$egin{cases} -\operatorname{div}(\operatorname{A}
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abla u+\sigma u=f & \operatorname{in} D\ u=g & & \operatorname{on}\Gamma_D\ \Phi(u):=(\operatorname{A}
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- model's coefficients $\ \ eta = [A_{ij}, \ b_i, \ \sigma]$
- forcing terms $\mathcal{L} = [f, h]$
- Dirichlet boundary conditions g

$$\implies u = u(eta, \mathcal{L}, g)$$



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Solution All the parameters $\eta = (\beta, \mathcal{L}, g)$ are supposed to be uncertain.



We characterize uncertainty in terms of sets A_{η} of admissible parameters (can be *infinite dimensional!*).



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Other parameter sets could be considered as well, with e.g. smoother perturbations. Computations get more involved.



Goal of the analysis

Section: We focus on a specific feature of the solution: Quantity of interest

local average of the solution

Examples :

local average of the flux

boundary flux

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$$Q=\int_{\omega\subset D}u$$

 $Q=\int_{\omega\subset D}A
abla u\cdot e_i$
 $Q=\int_{\Gamma_D}\Phi(u)$



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Examples :
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 $\begin{array}{ll} \mbox{General form for the Q.o.l.} & Q(\eta, u, \Phi) = Q_1(\eta, u) + Q_2(\Phi). \\ \mbox{notation:} & \psi(\eta) = Q(\eta, u(\eta), \Phi(\eta)) \end{array}$



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Worst scenario analysis- compute $Q_0 = \psi(\eta_0)$ (nominal value)- estimate $\Delta Q = \sup_{\eta \in \mathcal{A}_{\eta}} |\psi(\eta) - \psi(\eta_0)|$



Example: groundwater flow problem



- $\Gamma = \Gamma_{up} \cup \Gamma_{dw}$: upper and lower surf.
- Σ : lateral surf.
- β : permeability



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Mathematical Model

 $\left\{ egin{aligned} \mathrm{div}(oldsymbol{eta}
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Mathematical Model



9 Q.o.l. extraction rate from the well: $Q(p) = \int_{well} eta
abla p \cdot n$

Incertainty in permeability and bottom pressure.









depth H = 100 ft

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depth H = 20 ft





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- **I** input: nominal value + uncertainty band $(\eta_0, \varepsilon(x))$
- **output:** uncertainty interval $\mathcal{I}Q = [Q_0 \pm \Delta Q]$



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Model update based on N validation data Q_i^v , $i = 1, \ldots, N$.

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Idea: interpret it as a uniform random variable $Q^v \sim \mathcal{U}(\mathcal{I}Q^v)$. This allows us to write a likelihood

$$L(\eta_0,\varepsilon|Q_i^v) = \begin{cases} \frac{1}{|\mathcal{I}Q^v(\eta_0,\varepsilon)|^N} & \text{if all } Q_i^v \in \mathcal{I}Q^v(\eta_0,\varepsilon) \\ 0 & \text{otherwise} \end{cases}$$

and perform a Bayesian update of the input data (η_0, ε) .



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and perform a Bayesian update of the input data (η_0, ε) . Take for instance maximum likelihood estimator

$$(\eta_0^{up}, \varepsilon^{up}) = \arg \max \ L(\eta_0, \varepsilon | Q_i^v) \pi_{prior}(\eta_0, \varepsilon)$$



Distance in the prediction (validation metric):

In the prediction level we measure the distance between the original model and the updated one: distance among intervals

original model up updated model


Validation of a worst-case scenario model

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Distance = $|\mathcal{I}Q^p \setminus \mathcal{I}Q^{up}|$



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Distance = $|\mathcal{I}Q^p \setminus \mathcal{I}Q^{up}|$

Production Criterion: for a given tolerance tol > 0

model rejected if $|\mathcal{I}Q^p \setminus \mathcal{I}Q^{up}| > tol$



Solution Technique

The computation of the Worst-Case Scenario bound

$$\Delta Q = \sup_{\eta \in \mathcal{A}_\eta} |\psi(\eta) - \psi(\eta_0)|$$

is a constrained optimization problem

- non convex in general
- may have many local maxima





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We have followed a simpler approach based on perturbation techniques



Perturbation method

Taylor expansion of $\psi(\eta)$ around η_0 : $\exists \theta \in (0,1)$ s.t.

$$\psi(\eta)-\psi(\eta_0)=< D_\eta\psi(\eta_0), \delta\eta>+rac{1}{2}D_\eta^2\psi(\eta_0+ heta\delta\eta)(\delta\eta,\delta\eta).$$

(here $D_{\eta}\psi$, $D_{\eta}^{2}\psi$ are Fréchet derivatives of $\psi(\eta)$).



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Then
$$\Delta Q \leq \sup_{\substack{\delta\eta \in \mathcal{A}_{\eta} - \eta_{0}}} | < D_{\eta}\psi(\eta_{0}), \delta\eta > |$$

$$\operatorname{Linear term} (\Delta Q^{lin})$$

$$+ \frac{1}{2} \sup_{\delta\eta \in \mathcal{A}_{\eta} - \eta_{0}} \sup_{\theta \in (0,1)} |D_{\eta}^{2}\psi(\eta_{0} + \theta\delta\eta)(\delta\eta, \delta\eta)|.$$
Remainder (\mathcal{R})



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Remainder (\mathcal{R})

Solution Remark: Q depends linearly on the boundary conditions g and forcing terms \mathcal{L} . In this case $\mathcal{R} = 0$.



Duality method

We first rewrite the primal problem in the following weak form: find $u \in H^1(D)$ and $\lambda \in H^{-\frac{1}{2}}(\Gamma_D)$ s.t.

$$egin{aligned} B(eta; u, v) &+ \int_{\Gamma_D} \lambda v = \mathcal{L}(v) & orall v \in H^1(D) \ \int_{\Gamma_D} u \mu &= \int_{\Gamma_D} g \mu & orall \mu \in H^{-rac{1}{2}}(\Gamma_D) \end{aligned}$$

where we use a Lagrange multiplier to impose boundary conds. and

$$B(eta; u, v) = \int_D \left[(\mathrm{A}
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A Q.o.I. associated to the normal flux can be written in the form



1

$$Q=Q(\lambda)$$

We also introduce a dual problem: find $\varphi \in H^1(D)$ and $\xi \in H^{-\frac{1}{2}}(\Gamma_D)$ s.t.

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We typically have $\begin{cases} B(\beta; u, v) = \int_D G(\beta; u, v) \, dx & \text{with } G \in L^1(D) \\ Q_1(\beta; v) = \int_D F(\beta; v) \, dx + \int_{\Gamma_N} H(v) \, dS & \text{with } F, H \in L^1 \end{cases}$



Uncertainty in the coefficients $\beta = [\beta_1, \ldots, \beta_m]$

By a duality argument, the Fréchet derivative of ψ wrt β is

$$< D_eta \psi(eta_0), \deltaeta > = \int_D
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We consider the set of coefficients (pointwise uncorr. perturbations):

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Linear worst scenario analysis: [Babuška-N-Tempone, 2005]

a)
$$\Delta Q^{lin} = \sum_{i=1}^{m} \int_{D} \left| \frac{\partial (F-G)}{\partial \beta_{i}} (\beta_{0}; u_{0}, \varphi_{0}) \right| \varepsilon_{i} dx,$$

b) worst perturbation: $\delta \beta_{i}^{*} = \varepsilon_{i} \operatorname{sign} \left(\frac{\partial (F-G)}{\partial \beta_{i}} \right)$



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Other types of perturbation sets could be considered as well. For instance, correlated coefficients or smoother perturbations. In this case the postprocess is more involved but still relatively cheap.



Bounds for the reminder

Not easy in general !



Bounds for the reminder

- $\label{eq:Reminder} \red{eq:Reminder} \ \mathcal{R} \equiv \frac{1}{2} \sup_{\delta\beta \in \mathcal{A} \beta_0} \sup_{\theta \in (0,1)} |D^2_\beta \psi(\beta_0 + \theta \delta\beta)(\delta\beta, \delta\beta)|.$
- **Second order Gâteaux derivative (case** $Q = Q(u(\beta))$)

 $egin{aligned} D^2_eta\psi(eta)(\deltaeta,\deltaeta) &= - \, D^2_eta B(eta;u(eta),arphi(eta))(\deltaeta,\deltaeta) \ &- 2 < D_eta B(eta;D_eta u(eta)(\deltaeta),arphi(eta)),\deltaeta > \end{aligned}$



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For symmetric problems: combine a priori and a posteriori estimates to get a bound of the form

$$\mathcal{R} \leq rac{1}{2} |u_0|_{E,eta_0} |arphi_0|_{E,eta_0} \sup_{eta \in \mathcal{A}_eta} \left\{ \sum_{i,j} C_{ij}(eta) ar{arepsilon}_i ar{arepsilon}_j
ight\}$$

where $\bar{\varepsilon}_i = \sup_{x \in D} \varepsilon_i(x)$: maximum perturbation for the *i*-th coefficient. The constants $C_{ij}(\beta)$ can be estimated in simple cases.



Other estimates for the reminder

If computable a priori bounds are impossible to obtain or the previous estimate is too pessimistic, then we can take as an estimate for the reminder the second derivative of $\psi(\beta)$ computed in the worst-direction $\delta\beta^*$: $\mathcal{R} \approx \frac{1}{2}D_{\beta}^2\psi(\beta_0)(\delta\beta^*,\delta\beta^*)$

Implies the computation of $w = D_{\beta}u(\beta_0)(\delta\beta^*)$ which satisfies

$$B(eta,w,v) = -\int_D
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Alternatively: sample at random some perturbations $\delta\beta^{(j)}$,
 j = 1, ..., M and compute $\mathcal{R} \approx \max_{j=1,...,M} \frac{1}{2} D_{\beta}^2 \psi(\beta_0) (\delta\beta^{(j)}, \delta\beta^{(j)})$.
 Implies the solution of M additional problems.



Uncertainty in load and boundary cond.s

It can be done in a similar way as for the coefficients. Observe that for a linear problem and linear Q.o.I, the reminder \mathcal{R} vanishes.



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 $\Delta Q = \varepsilon \|\varphi_0\|_{L^2(D)}.$

Uncertainty in the load [Babuška-N-Tempone, 2005]:

uncertainty set

$$\mathcal{A}_f \equiv \{f=f_0+\delta f: \; \|\delta f\|_{L^2(D)} \leq arepsilon\}$$

uncertainty bound

worst perturbation $\delta f^* = arepsilon arphi_0 \| arphi_0 \|_{L^2(D)}$



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Uncertainty in the load [Babuška-N-Tempone, 2005]:

uncertainty set $\mathcal{A}_f \equiv \{f = f_0 + \delta f : \|\delta f\|_{L^2(D)} \le \varepsilon\}$ uncertainty bound $\Delta Q = \varepsilon \|\varphi_0\|_{L^2(D)}.$ worst perturbation $\delta f^* = \varepsilon \varphi_0 / \|\varphi_0\|_{L^2(D)}$

Uncertainty in Dirichlet boundary conditions [Babuška-N-Tempone, 07]:

uncertainty set $\mathcal{A}_g \equiv \{g = g_0 + \delta g : |\delta g(x)| \leq \varepsilon_g(x)\}$ uncertainty bound $\Delta Q = \int_{\Gamma_D} |\xi_0| \varepsilon_g(x) dx$ worst perturbation $\delta g^* = \operatorname{sign}(\xi_0) \varepsilon_g(x).$



Assume we compute primal and dual finite element solutions u_{0h} and φ_{0h} .

What has to be verified?



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What has to be verified?

a) The computation of the quantity of interest Q_{0h} based on the FE solution. We used Dual Weighted Residual error estimators.



Assume we compute primal and dual finite element solutions u_{0h} and φ_{0h} .

What has to be verified?

- a) The computation of the quantity of interest Q_{0h} based on the FE solution. We used Dual Weighted Residual error estimators.
- b) The computation of the linear uncertainty bound ΔQ_h^{lin} based on the FE solution. Need both a priori and a posteriori error bounds.

In [Babuška-N-Tempone '05] we proved that

$$|\Delta Q^{lin} - \Delta Q^{lin}_h| \leq C \left(\|u_0 - u_{0h}\|_{H^1} + \|arphi_0 - arphi_{0h}\|_{H^1}
ight)$$



c) A posteriori control on the accuracy in the computation of

$$\Delta Q_h^{lin} = \sum_{i=1}^m \int_D \left| \frac{\partial (F-G)}{\partial \beta_i} (\beta_0; u_{0h}, \varphi_{0h}) \right| \varepsilon_i \, dx.$$

The function $\left|\frac{\partial (F-G)}{\partial \beta_i}\right| \varepsilon_i$ is not regular, in general (has surfaces of non differentiability). We have used adaptive integration. FromSlide2

d) Check the accuracy of the estimate for the reminder. How to do it properly is an open question.



Numerical Results – Heat transfer



	$\Big(-{ m div}(eta abla u)=0,$	in $D\subset \mathbb{R}^3$
Į	u=0,	on $\Gamma_1 \cup \Gamma_2$
	$eta \; \partial_n u = 1$	on Γ_3
	$ig eta \partial_n u = 0$	$\partial D \setminus \Gamma_{1,2,3}$

u: temperature; β : conductivity;

 $eta_{inclusion} = 50 * eta_{material}$



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u: temperature; β : conductivity;

 $eta_{inclusion} = 50*eta_{material}$

• Q.o.I: outward flux on Γ_1 . $Q(\beta, u(\beta)) = -\int_{\Gamma_1} \beta \partial_n u(\beta) dS$. • Uncertainty characterization:

 $eta \in \mathcal{A}_eta \equiv \{eta \in L^\infty(D), \; |eta(x) - eta_0(x)| \leq arepsilon_eta(x), \; \; orall x \in D\}$



Numerical Results – heat transfer



primal solution



dual solution

 $Q(\beta_0) = 0.597 {\pm} 1\%$

Mesh adapted w.r.t. a goal-oriented error estimator; 7535 \mathbb{Q}^2 FE.



Numerical Results – heat transfer

Uncertainty in conductivity coefficient: $\frac{|\beta(x) - \beta_0(x)|}{\beta_0(x)} \leq 10\%$.

$$\Delta Q_h^{lin} = 0.0446 = 7.47\%\,Q(eta_0,u(eta_0))$$


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Worst distribution β^* of the conductivity coefficient in the material (left) and the inclusion (right).



Numerical Results – heat transfer

Sensitivity function





Numerical Results – heat transfer

The following computable bound can be obtained

$$|\mathcal{R}| \leq |u_0|_{E,eta_0} |arphi_0|_{E,eta_0} \left(1 + \left\|rac{eta_0}{eta_{min}}
ight\|_{L^\infty}^rac{1}{arphi} arphi_{L^\infty}^rac{eta_0}{eta_{min}}
ight\|_{L^\infty}^rac{eta_0}{arphi_{min}}
ight\|_{L^\infty}^2}$$

where ε is the relative maximum perturbation: $\varepsilon = \sup_{\delta\beta} \|\delta\beta/\beta_0\|_{L^{\infty}(D)}$.

$$egin{aligned} \Delta Q_h^{lin} &= 0.0446 = 7.47\%\,Q(eta_0,u(eta_0)) \ \mathcal{R} < 6.5arepsilon^2 + O(arepsilon^3) pprox 0.065, & ext{for }arepsilon = 0.1 \end{aligned}$$



Numerical results – Linear elasticity



Quantities of interest:

$$egin{aligned} Q_1(\mathrm{u}) &= rac{1}{|S|} \int_S u_z \ dS \ Q_2(\mathrm{u}) &= rac{1}{|S/2|} \int_{S/2} u_y \ dS \end{aligned}$$



Numerical results – Linear elasticity



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Uncertainty:

coefficients: $\mathcal{A}_{\beta} \equiv \{ |E(x) - E_0| \leq \varepsilon_E; |\nu(x) - \nu_0| \leq \varepsilon_{\nu}, \forall x \in D \}$

load: $\mathcal{A}_{\mathcal{L}} \equiv \{g \in [L^2(S)]^3 \ s.t. \ \|g_i - g_{0i}\|_{L^2(S)} \le \varepsilon_{g_i}, \ i = 1, 2 \text{ or } 3\}$ we can also impose constraints such as $\int_S (g_i - g_{0i}) = 0.$



Numerical results – linear elasticity

Uncertainty characterization of material properties:

$$|E(x) - E_0| \le 1\% E_0 \qquad |
u(x) -
u_0| \le 8\%
u_0$$

Quantity of Interest	$\Delta Q^{lin}/Q$	\mathcal{R}/Q	$1/2D_eta^2\psi/Q$
$Q_1 = -7.3613510^{-4}$	1.536%	>15%	0.027%
$Q_2 = 5.3964 10^{-5}$	1.594%	>27.6%	0.016%



Numerical results – linear elasticity, Q_1



Worst distribution of E (left) and ν (right).





Sensitivity functions α^{E} (left) and α^{ν} (right).



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Numerical results – linear elasticity, Q_2



Worst distribution of E (left) and ν (right).





Sensitivity functions α^{E} (left) and α^{ν} (right).



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Numerical results – linear elasticity

Uncertainty characterization of the load $\ensuremath{\mathrm{g}}$: let

$$arepsilon_x = arepsilon_y = 1\% \|g_z\|_{L^2(S)}, \qquad arepsilon_z = 5\% \|g_z\|_{L^2(S)}$$

set $\tilde{\mathbf{g}} = [\frac{g_x}{\varepsilon_x}, \frac{g_y}{\varepsilon_y}, \frac{g_z}{\varepsilon_z}]^T$. Perturbation set:

first case:

second case:

$$egin{aligned} \mathcal{A}_{\mathcal{L}}^1 &\equiv \{\mathrm{g} = \mathrm{g}_0 + \delta \mathrm{g}: ~ \|\widetilde{\delta \mathrm{g}}\|_{[L^2(S)]^3} \leq 1 \} \ \mathcal{A}_{\mathcal{L}}^2 &\equiv \{\mathrm{g} \in \mathcal{A}_{\mathcal{L}}^1, ~ \int_S \delta \mathrm{g} = 0 \} \end{aligned}$$

	$\Delta Q_1/Q_1$	$\Delta Q_2/Q_2$
$\mathcal{A}^1_\mathcal{L}$	5.007%	5.003%
$\mathcal{A}_{\mathcal{L}}^2$	0.085%	0.12%



Numerical results – linear elasticity



Worst distribution of the load for the set $\mathcal{A}^1_{\mathcal{L}}$



Numerical Results – groundwater flow problem



- $\Gamma = \Gamma_{up} \cup \Gamma_{dw}$: upper and lower surf.
- Σ : lateral surf.
- β : permeability



Numerical Results – groundwater flow problem



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- Σ : lateral surf.
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Mathematical Model

 $\left\{ egin{aligned} \mathrm{div}(oldsymbol{eta}
abla p) &= 0 & ext{in } D \ p &= 0 & ext{on } \Gamma_{up} \ p &= oldsymbol{g} & ext{on } \Gamma_{dw} \ eta \partial_n p &= 0 & ext{on } \Sigma \end{aligned}
ight.$



- well model: 5ft diameter hole with permeability 20 times larger.

- Q.o.I: extraction rate from the well: $Q(p) = \int_{well} \beta
abla p \cdot n$

● Primal and dual solutions computed with Q_1 finite elements, 14K dofs on a goal oriented mesh. Q(p) = 497.4 with a discretization error smaller than 5%

- Perturbation in permeability coeff: max. 10% pointwise
- Perturbation in boundary pressure on the bottom: 10% pointwise



primal and dual solutions





Pressure in the domain

Dual solution



primal and dual solutions





Enlargement around the well (zoom x 16)

Dual solution



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primal and dual solutions





Enlargement around the well (zoom x 16)

Enlargement around the well (zoom x 16)



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flux on the bottom and top surfaces



Тор



flux on the bottom and top surfaces



Top: enlargement x16



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flux on the bottom and top surfaces





Top: enlargement x16

Bottom



Uncertainty analysis

Pert. in permeability: $\Delta Q^{lin} = 4.83 (1\% Q)$ (error in quadrature formula < 1%). The estimate for the Reminder is too pessimistic in this case.

Pert. in boundary pressure: $\Delta Q = 51 \ (10\% Q)$ (no error in quadrature formula)



Conclusions

- The Worst-Case Scenario can be easily computed, for certain classes of infinite dimensional perturbations in coefficients and loads, by postprocessing the solutions of the primal and dual problems computed for the nominal values of the parameters
- The WCS analysis can be set at the continuous level. Allows for rigorous convergence results of the finite element solution to the theoretical bounds.
- We have shown how the WCS approach fits nicely in a Verification and Validation framework.
- We have proposed an effective way to compute the worst-case scenario for perturbations in Dirichlet boundary conditions, by the use of Lagrange multipliers.
- How to obtain good (guaranteed) bounds for the reminder is still an open question in many applications.







References

- [BNT-Numer.Math.05] Worst-case scenario analysis for elliptic problems with uncertainty, Numer. Math., 101(2005), pp. 185–219.
- [BNT-Eurodyn 05] Worst-case scenario analysis for elliptic PDE's with uncertainty, Proceeding of EURODYN 2005
- [BNT-07] Propagating uncertainty from boundary conditions in elliptic equations via a worst scenario analysis, in preparation.



Other types of perturbation sets (I)

a) Correlated coefficients

 $\mathcal{A}_eta = \{ \deltaeta \in [L^\infty(D)]^m, \ \ (eta)(x) \in \Sigma(x) \subset \mathbb{R}^m, \ orall x \in D \}$

where $\Sigma(x)$ is a convex polygon, piecewise smooth w.r.t. x.



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where $\Sigma(x)$ is a convex polygon, piecewise smooth w.r.t. x.

 \implies in each element *K* of the mesh we have to solve a linear constrained optimization problem to find the maximum over the set Σ .



uncorrelated coefficients







correlated coefficients

Other types of perturbation sets (II)

b) Smoother perturbations

We could use a penalization approach: find the worst perturbation $\delta\beta^*$ s.t.

$$\deltaeta^* = rgmax_{\deltaeta\in\mathcal{A}-eta_0} \left\{ < D_eta\psi(eta_0), \deltaeta > -rac{1}{2}\sum_{i=1}^m
ho_i \|\deltaeta_i\|_{H^1(D)}^2
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 \implies this problem is no longer separable in x. Implies a greater computational effort.



Much easier: u is linear (affine) with respect to the load; the dual solution does not depend on the load.



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We consider the parameter set

 $\mathcal{A}_{\mathcal{L}} \equiv \{\mathcal{L} = \mathcal{L}_0 + \delta \mathcal{L}: \ \delta \mathcal{L} \in W', \qquad \|\delta \mathcal{L}\|_{W'} \leq \varepsilon\}$

for some Banach spaces $W \supseteq V_0$ (typically $W = L^q$).



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Uncertainty in the Dirichlet boundary cond.

The first Fréchet derivative of ψ w.r.t. the boundary datum g is

$$< D_eta \psi(g_0), \delta g> = \int_{\Gamma_D} \xi_0 \, \delta g$$

where ξ is the *dual flux*. All the higher derivatives vanish.



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Worst Scenario bound [BNT 07]: if the dual flux is at least in $L^1(\Gamma_D)$.

a)
$$\Delta Q = \sup_{g \in \mathcal{A}_g} |\psi(g) - \psi(g_0)| \leq \int_{\Gamma_D} \left| \xi_0 \right| arepsilon_g(x) \, dx$$

worst perturbation $\delta g^* = \operatorname{sign}(\xi_0) \varepsilon_g(x)$.



b)



Details on adaptive integration

Build a sequence of adapted meshes $h_q[k], \ k = 1, 2, ...$

for each element $n=1,2,\ldots,N[k]$,

- compute the integral $I_n = \int_{K_n} \left| rac{\partial (F-G)}{\partial eta_i} \right| arepsilon_i$
- uniformly *h*-refine the element, recompute the integral and use the difference as error indicator $r_n[k]$
- if $r_n[k] > rac{TOL}{N[k]}$ then

mark the element for refinement

- end if

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refine the marked elements

(Convergence proof in "Moon-Von Schwerin-Szepessy-Tempone '04")



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The final mesh is well suited to represent the worst per-




Numerical computation of the dual flux

If one computes the finite element dual solution $\varphi_0^h \in V_h$ with strong imposition of the boundary conds., the dual flux can be reconstructed as: find $\xi_0^h \in V_h(\Gamma_D)$ s.t.

 $\int_{\Gamma_D} \xi_0^h \, \mu_h = Q_1(\beta, E(\mu_h)) - B(\beta; E(\mu_h), \varphi_h), \quad \forall \mu_h \in V_h(\Gamma_D)$

where $E(\mu_h)$ is an arbitrary extension of μ_h inside the domain.



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● For a quasi-uniform mesh and $\xi \in L^2(\Gamma_D)$, one has sub-optimal
rate of convergence [BNT - 05]