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CHARGE:

- Guided by the Snowmass '96 parameter sets, explore and develop innovative concepts that will result in significant cost reductions.
- Coordinate parameter sets, infrastructure requirements for the various options, and designs with the other working groups.
- Review progress in magnet R&D (including materials and may include cryogenics, vacuum).
- Develop bases including costs for comparing different magnet designs.
 - Monitor, encourage, and coordinate progress in materials development both in academe and industry.

VLHC MAGNET WORKSHOP REVIEW OF SNOWMASS '96 PARAMETERS

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General Features of the vlhc

Snowmass '96 Machines

Parameter list

Lattice features

Interaction region

Vacuum

Cryogenics

Summary

General Features

of third-generation ($E_{CM} = 100 \text{ TeV}$) hadron colliders

1. Physics at the energy frontier: a discovery machine

2. Luminosity $> 10^{34}$ cm⁻² sec⁻¹ at two detectors

3. Based on superconducting magnet technology

4. Large scale (circumference >100 km, numbers of magnets >1000)

5. Must be as cost-effective as possible

6. Requires a conservative design approach that insures reliability at the design goals

7. Will be an internationally supported effort

Snowmass '96 Machines

Motivation: For any vlhc, the magnets are the system cost driver. New approaches are needed since a scaleup of the existing NbTi technology would be prohibitively expensive.

> Three examples were considered, all with $E_{CM}=100$ TeV, Peak luminosity= 10^{34} cm⁻²sec⁻¹

> Principal distinguishing features:

-the choice of superconducting magnet technology;
-the size of the ring;
-the role of synchrotron radiation damping;

(a) High-field-new technology:

Dipole field >12 T Circumference 100 km Synchrotron-radiation damped emittance 1.3 hr emittance damping time *The key is the conductor*

>12 T magnet requires either Nb₃Sn @4^oK or (preferably) the use of high temperature superconductor (HTS) (b) High-field-current technology:

Dipole field >9-10 T Circumference 140 km Synchrotron-radiation damped emittance 2.3 hr emittance damping time

9.5 T magnet could be implemented with NbTi @ 1.80 K. The engineering challenge is to bring down the cost and complexity of a known technology

(c) Low field (Pipetron)

Dipole field <2 T Circumference 650 km No damping

Simple, low cost superferric (1.8T) combined function "Double-C transmission line" magnet from Fermilab

Goal: 10x lower magnet cost per TeV than conventional SC Magnets





	vlhc Machine parameters								
Parameter	High field-new technology	Low Field	Units						
CM Energy	100	100	TeV						
Dipole field	12.6	1.8	Т						
Circumference	104	646	km						
Revolution frequency	2.89	.46	kHz						
Injection energy	3	3	TeV						
Synchrotron radiation damping time (horizontal amplitude)	2.6	antidamped	hr						
Equilibrium rms emittance	144.2		π nm						
Energy loss/turn	3678	526	keV						
Synchrotron radiation	189	48	kW						
power/ring									
Initial/peak luminosity	.35/1.2	1./1.	$10^{34} \text{ cm}^{-2} \text{sec}^{-1}$						
Protons/bunch	0.5	0.94	1010						
Bunch spacing	16.7	16.7	nsec						
Number of bunches	20794	129240							
Total protons/ring	1.1	12.2	10 ¹⁴						
Beam stored energy	.89	9.73	GJ						
Injected rms normalized	1.	1.	$\pi\mu\mathrm{m}$						
β*	20	20	cm						
Rms relative energy spread(collision)	15.6 (50)	39.0	10 ⁻⁶						
Total current	.05	.09	Amp						
Peak current(injection)	3.6	4.2	Amp						
<\$>	255	382	m						
Tune	65	269							
Half cell length (assumed	200	300	m						
90° cells)	200	200	***						
Beam pipe radius	1.65	1.0	cm						
Beam pipe	Cold, Cu	Warm, Al							

Arc lattice features

Cell parameters:

Phase advance: 90° Cell length: 400-500 m



e.g, n=10=>40-50 m long dipoles

Number of cells: Low field ~1300=>13000 dipoles (per ring) High field ~260=>2600 dipoles (per ring)

Beam pipe physical aperture: High field: round, 33 mm diameter Low field: oval, 20 mm diameter (short axis)

Maximum beam size at 3 TeV injection: 1.2 mm (95%)

The cell length/aperture tradeoff:

Cell length L:

 $L \propto \frac{\gamma_I}{\mathcal{E}_n} r_{GF}^2, r_{GF} \propto d_c^2$

 $r_{GF}^{="\text{good-field" radius}}$ d_c =coil diameter γ_I =injection gamma=3000 \mathcal{E}_n =normalized emittance at injection

Longer cells are cheaper: fewer correctors, quadrupoles, spools; larger dispersion, so reduced strength chromatic sextupoles, for increased dynamic aperture

BUT

requires larger $r_{GF} =$ larger coil diameter, more expensive magnets

Additional constraints:

Low field: smaller apertures run into beam stability problems very rapidly

High field: cells longer than about 600 m have equilibrium emittance

$\mathcal{E}_{x} \propto B^{3}L^{3}$

larger than $1\pi \mu m$.

Interaction Region

Snowmass example design (Wei, Peggs, Goderre)



β^{max}=64 km

Triplet field quality required:

0.5 units of b5 @ 10 mm, without correction, end and body separate need shimming and/or lumped correctors C1,C2,C3

May need local chromatic correction

Synchrotron radiation power: 100 W Radiation from the IP: 6 kW

 β^* limited by the crossing angle To go below 10 cm: Need crab crossing system and local chromatic correction

Interaction Region

FLAT BEAMS

(Peggs, Harrison, Pilat, Syphers)

If the vertical dispersion and the linear coupling are well-controlled in the arcs, the vertical emittance will damp to a value much smaller than the horizontal emittance, resulting *in flat beams* as in an electron storage ring. Such beams have several advantages in IR design over round beams.

The final focus optics can be a doublet, rather than a triplet

The peak beta function is typically x10 smaller, for the same β^* , than with round beam triplet optics=> field quality demands in the final focus quads are relaxed

Long-range tune shifts (mostly vertical) occuring before the beams separate tend to be smaller

Vacuum

(W. Turner)

High Field

Synchrotron radiation power: 190 kW Beam lifetime ($\tau_{pp} = 32$ hrs)

Ringwide average vacuum requirement for τ_{gas}~5τ_{pp}: 1.8 nTorr RTE CO



Needs a liner with distributed cryosorber at 10-15° K to intercept synchrotron radiation and pump photodesorbed gases

Design simplifies if magnets use HTS at ~10-15°K liner can be integrated to magnet bore tube

Magnets above~15° K: H₂ is no longer cryosorbed, liner must be cooled separately from the magnet Magnets at ~1.8° K: no cryosorber needed



Vacuum

Requires the use of a distributed pumping system integrated with the magnets-as in an electron synchrotron.

Lumped pumps for nonreactive CH₄ also required every 20 m

Cryogenics (MacAshan, Mazur)

Table III: Comparison of Cryogenic Systems for Different RLHC Magnets										
Collider Magnet	Ring	Nº of	Total Heat Load					Ideal	Wall-	
Operating	Size	Station	at nominal temperature					Pwr	Plug	
Temperature		(inc. 1	(kilowatts)						Power	
		IR)								
	km		1.8 K	4.5 K	20 K	50 K	Lead	MW	MW	
							S			
Low Field							(g/s)			
NbTi, 4.5-5.0	646	9	0	247	0	0	200	17.2	66	
Nb3Sn, 4.5-6.5	646	9	0	242	0	0	200	12.3	47	
HTS, 20-25 K	646	9	0	0	242	0	200	3.7	14	
High Field										
NbTi, 1.8 K	138	20	115	413	0	1644	920	45	180	
Nb3Sn, 4.5 K	104	18	0	66	420	1080	940	18	72	
HTS, 25 K	104	18	0	15	590	1080	940	14	54	

Summary

Snowmass vlhc parameters:

100 TeV CM Peak luminosity>10³⁴ cm⁻²sec⁻¹

High field machine:

~100 km circumference radiation damped beam dynamics 12.5 T cold bore magnets 190 kW synchrotron radiation power Flat beam collisions: doublet IR optics

Low field machine:

~650 km circumference conventional (proton) beam dynamics 2 T warm bore magnets 50 kW synchrotron radiation power Round beam collisions: triplet IR optics