

## **APPENDIX**

Appendix A: Process Operating Data

Appendix B: Calculations

Appendix C: Raw Field Data and Calibration Data Sheets

Appendix D: Reduced Field Data Sheets

Appendix E: Sampling Log and Chain of Custody Records

Appendix F: Analytical Data Sheets

Appendix G: List of Participants



Valley Power Plant - Boiler # 3

Mercury ICR

CEM Data

November 30, 1999

Test Run #	Time	Stack Data										Boiler Data					
		S2STEMP (DEGFAHRE)	S2PCO2 (PERCENT)	S2CPFLOW (SCFH )	S2NOX#M1 (LB/MMBTU)	S2SO2#M1 (LB/MMBTU)	U3STEAM (KLBS/HR)	U3STEMP (KLBS/HR)	U3HEAT1 (MMBTU/HR)	D3CO2 (PERCENT)	D3NOX#M1 (LB/MMBTU)						
1	9:00 - 10:19	312.1	12.7	23150098	0.526	1.59	652	752.3	938	12.97	0.633						
2	12:00 - 14:17	313.1	12.3	22927015	0.545	1.61	654	754.8	923	12.90	0.647						
3	14:50 - 17:10	313.0	12.2	23082755	0.539	1.65	646	744.9	900	12.77	0.653						
	Average	312.7	12.4	23053289	0.536	1.61	651	750.7	920	12.88	0.644						

Valley Power Plant - Boiler # 3

Mercury ICR

CEM Data

November 30, 1999

Time	Stack Data							Boiler Data						
	S2STEMP (DEGFAHRE)	S2PCO2 (PERCENT)	S2CPFLOW (SCFH)	S2NOX#M1 (LB/MMBTU)	S2SO2#M1 (LB/MMBTU)	U3STEAM (KLBS/HR)	U3STEMP (KLBS/HR)	U3HEAT1 (MMBTU/HR)	D3CO2 (PERCENT)	D3NOX#M1 (LB/MMBTU)	U3STEAM (KLBS/HR)	U3STEMP (KLBS/HR)	U3HEAT1 (MMBTU/HR)	D3CO2 (PERCENT)
0:00	299.3	11.8	18425114	0.421	1.59	406	468.9	597	11.90	0.444				
1:00	292.7	11.7	17550264	0.426	1.60	393	453.3	563	11.83	0.446				
2:00	288.1	12.0	17036714	0.406	1.58	394	455.0	561	11.85	0.453				
3:00	287.3	12.0	17112364	0.405	1.56	404	466.7	570	11.79	0.454				
4:00	286.9	12.1	17366736	0.405	1.57	406	468.2	575	11.85	0.459				
5:00	289.2	12.4	19057206	0.427	1.58	461	531.4	647	12.37	0.486				
6:00	293.8	12.4	20451186	0.442	1.58	490	565.4	695	12.58	0.504				
7:00	297.6	12.6	20664826	0.447	1.57	501	578.3	716	12.66	0.509				
8:00	306.7	12.7	23213342	0.528	1.59	641	739.4	906	13.00	0.624				
9:00	312.1	12.7	23279734	0.524	1.58	651	750.7	937	12.97	0.631				
10:00	312.0	12.7	23020462	0.527	1.59	653	753.8	939	12.97	0.634				
11:00	312.0	12.6	22979474	0.533	1.59	653	754.0	942	12.66	0.635				
12:00	312.9	12.5	22932700	0.544	1.60	654	755.1	937	12.93	0.640				
13:00	313.3	12.1	22921330	0.545	1.62	654	754.5	908	12.86	0.653				
14:00	312.7	12.0	22774768	0.540	1.64	648	748.2	890	12.82	0.654				
15:00	312.9	12.1	23002266	0.541	1.65	647	746.0	898	12.77	0.653				
16:00	313.1	12.2	23163244	0.536	1.64	645	743.8	901	12.76	0.653				
17:00	312.7	12.2	22941846	0.527	1.63	607	700.8	861	12.73	0.627				
18:00	311.8	12.1	22984118	0.523	1.65	565	651.9	773	12.64	0.587				
19:00	316.4	12.1	23869440	0.524	1.65	571	658.9	798	12.55	0.576				
20:00	312.2	12.0	22412680	0.484	1.64	539	622.3	751	12.51	0.534				
21:00	305.7	11.9	20526402	0.443	1.63	478	552.0	680	12.29	0.500				
22:00	303.5	12.0	21429958	0.471	1.63	517	596.4	716	12.41	0.531				
23:00	298.9	10.4	14970989	0.415	1.53	311	358.3	433	10.62	0.461				
Average	304.3	12.1	21003632	0.483	1.60	537	619.7	758	12.43	0.556				
Maximum	316.4	12.7	23869440	0.545	1.65	654	755.1	942	13.00	0.654				
Minimum	286.9	10.4	14970989	0.405	1.53	311	358.3	433	10.62	0.444				

Hours in **BOLD** represent data used in calculating average during test run.

**Valley Power Plant - Boiler # 3**  
**Mercury ICR**  
**Operational Data**  
**November 30, 1999**

Test Run #	Time	Main Steam		Baghouse		Boiler O2 (%)	Boiler Opacity (%)	3A Pulverized		3B Pulverized		Total Pulverized Coal Feed (klb/hr)
		Flow (klb/hr)	Total Air Flow (%)	Differential Pressure (in H2O)	Pressure (in H2O)			Coal Feed (klb/hr)	Coal Feed (klb/hr)	Coal Feed (klb/hr)	Coal Feed (klb/hr)	
1	9:00 - 11:25	23MS0F80 650.2	23BA0F80 87.7	23PE0P4S 4.45	23PE0P4S 4.45	O021Z006 3.71	23BA0A90 3.8	23BYAF10 33.0	23BYBF10 34.0	23BYAF10 33.0	23BYBF10 34.0	67.0
2	12:00 - 14:17	652.0	88.0	4.75	4.75	3.70	3.3	32.8	33.9	32.8	33.9	66.6
3	14:50 - 17:10	644.3	87.7	4.50	4.50	3.73	3.0	32.0	33.4	32.0	33.4	65.4
	<b>Average</b>	<b>648.8</b>	<b>87.8</b>	<b>4.56</b>	<b>4.56</b>	<b>3.71</b>	<b>3.4</b>	<b>32.6</b>	<b>33.7</b>	<b>32.6</b>	<b>33.7</b>	<b>66.3</b>

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam		Baghouse Differential		Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal
	Flow	Total Air Flow	Pressure	Coal Feed			Coal Feed	Flow	
	23MS0F80	23BA0F80	23PE0P4S	23BYAF10			23BYBF10		
	KLBH	PERCNT	WC	KLBH			KLBH	KLBH	
ACTUAL	ACTUAL	ACTUAL	ACTUAL	ACTUAL	ACTUAL	ACTUAL	ACTUAL	CALC	
9:00:52	645	88	5.5	3.7	4	33	34	67	
9:02:05	650	87	5.5	3.7	4	33	34	67	
9:03:18	645	87	5.5	3.7	4	33	34	67	
9:04:31	650	87	5.7	3.7	4	33	34	67	
9:05:44	655	88	5.3	3.7	4	33	34	67	
9:06:57	645	87	5.3	3.7	4	33	34	67	
9:08:10	644	87	5.5	3.7	4	33	34	67	
9:09:23	650	87	5.5	3.7	4	33	34	67	
9:10:36	642	88	5.4	3.7	0	33	34	67	
9:11:49	647	87	5.1	3.7	4	33	34	67	
9:13:02	652	87	5.1	3.7	4	33	33	66	
9:14:15	647	88	5.1	3.7	4	33	34	67	
9:15:28	647	88	5.1	3.7	4	33	34	67	
9:16:41	652	88	5.3	3.7	4	33	34	67	
9:17:54	646	87	4.6	3.7	4	33	34	67	
9:19:07	652	88	4.8	3.7	4	33	34	67	
9:20:20	647	88	4.8	3.7	4	33	34	67	
9:21:33	653	87	5	3.7	4	33	34	67	
9:22:46	651	87	5	3.7	4	33	34	67	
9:23:59	646	87	4.4	3.7	4	33	34	67	
9:25:12	646	87	4.6	3.7	4	33	34	67	
9:26:25	651	87	4.6	3.7	4	33	34	67	
9:27:38	645	87	4.6	3.7	4	33	34	67	
9:28:51	646	87	4.8	3.7	4	33	34	67	
9:30:04	651	87	4.8	3.7	4	33	34	67	
9:31:17	651	87	2.3	3.7	4	33	34	67	
9:32:30	651	87	8.5	3.7	4	33	34	67	
9:33:43	651	88	4.1	3.7	6	33	34	67	
9:34:56	645	88	4.6	3.7	4	33	34	67	
9:36:09	650	88	4.6	3.7	3	33	34	67	
9:37:22	650	87	4.8	3.7	3	33	34	67	
9:38:35	657	88	7.3	3.7	3	33	34	67	
9:39:48	651	88	4.9	3.7	3	33	34	67	
9:41:01	646	88	3.7	3.7	4	33	34	67	
9:42:14	646	87	6.4	3.7	4	33	34	67	
9:43:27	651	88	4.4	3.7	4	32	34	66	
9:44:40	651	87	3.4	3.7	4	33	34	67	
9:45:53	641	87	3.9	3.7	4	33	34	67	
9:47:06	641	87	4.3	3.9	4	33	34	67	
9:48:19	647	88	4.4	3.7	4	33	34	67	
9:49:32	651	87	4.2	3.7	4	33	34	67	
9:50:45	651	88	4.2	3.7	4	33	34	67	
9:51:58	651	87	4.7	3.7	4	33	34	67	
9:53:11	651	88	6.2	3.7	4	33	35	68	
9:54:24	651	87	4.6	3.7	4	33	34	67	
9:55:37	646	88	4.8	3.7	4	33	34	67	
9:56:50	647	88	4.8	3.7	4	33	34	67	
9:58:03	647	88	4.4	3.7	4	33	34	67	
9:59:16	647	88	2.3	3.7	4	33	34	67	
10:00:29	652	88	2.1	3.9	4	33	34	67	
10:01:42	652	88	2.1	3.7	4	33	34	67	
10:02:55	652	88	4.4	3.7	4	33	34	67	
10:04:08	646	87	4.3	3.7	4	33	34	67	
10:05:21	651	87	4.3	3.7	4	33	34	67	
10:06:34	657	87	4.3	3.7	4	33	34	67	
10:07:47	656	88	4.5	3.7	4	33	34	67	

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam		Baghouse Differential		Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal Flow KLBH CALC
	Flow	Total Air Flow	Pressure	Coal Feed			Coal Feed		
	23MS0F80 KLBH ACTUAL	23BA0F80 PERCNT ACTUAL	23PE0P4S WC ACTUAL	23BYAF10 KLBH ACTUAL			23BYBF10 KLBH ACTUAL		
10:09:00	656	88	4.5	3.7	4	33	34	67	
10:10:13	651	88	3.8	3.7	3	33	34	67	
10:11:26	651	88	4.4	3.7	3	33	34	67	
10:12:39	646	88	4.4	3.7	3	33	34	67	
10:13:52	650	88	4.4	3.7	3	33	34	67	
10:15:05	650	88	4.4	3.7	3	33	35	68	
10:16:18	650	88	3.9	3.9	3	33	34	67	
10:17:31	650	88	4.2	3.9	3	33	34	67	
10:18:44	651	88	4.2	3.9	3	33	34	67	
10:19:57	651	88	4.2	3.7	3	33	34	67	
10:21:10	647	88	4.2	3.7	3	33	34	67	
10:22:23	652	88	4.6	3.7	3	33	34	67	
10:23:36	647	88	4.4	3.7	3	33	34	67	
10:24:49	652	88	4.4	3.7	3	33	34	67	
10:26:02	646	88	3.6	3.7	3	33	34	67	
10:27:15	652	88	4.4	3.7	4	33	34	67	
10:28:28	652	88	5.9	3.7	4	33	34	67	
10:29:41	652	88	4.7	3.7	4	33	34	67	
10:30:54	652	88	4.7	3.7	4	33	34	67	
10:32:07	652	88	4.8	3.7	4	33	34	67	
10:33:20	652	87	3.7	3.7	4	33	34	67	
10:34:33	652	88	3.9	3.7	4	33	34	67	
10:35:46	652	88	3.9	3.7	4	33	34	67	
10:36:59	652	88	3.9	3.7	4	33	34	67	
10:38:12	646	88	4	3.9	4	33	34	67	
10:39:25	652	88	4	3.7	4	33	34	67	
10:40:38	652	88	4.2	3.7	4	33	34	67	
10:41:51	652	88	4	3.7	4	33	34	67	
10:43:04	652	88	4.1	3.7	4	33	34	67	
10:44:17	652	88	4.1	3.7	4	33	34	67	
10:45:30	652	88	4.1	3.7	4	33	34	67	
10:46:43	658	88	4.1	3.7	4	33	34	67	
10:47:56	653	88	4.1	3.7	4	33	34	67	
10:49:09	658	88	4.1	3.7	4	33	34	67	
10:50:22	653	88	4.2	3.7	4	33	34	67	
10:51:35	647	88	3.9	3.7	4	33	34	67	
10:52:48	652	88	5.3	3.7	4	33	34	67	
10:54:01	652	88	4.3	3.7	4	33	34	67	
10:55:14	652	88	4.3	3.7	4	33	34	67	
10:56:27	652	88	4.3	3.7	4	33	34	67	
10:57:40	652	88	2	3.7	4	33	34	67	
10:58:53	652	88	2	3.7	4	33	34	67	
11:00:06	652	88	4.1	3.7	4	33	34	67	
11:01:19	652	88	4.1	3.7	4	33	34	67	
11:02:32	646	87	4.1	3.7	4	33	34	67	
11:03:45	652	88	4.0F,	,	,	,	,	,	
11:04:58	652	88	4.0F,	,	,	,	,	,	
11:06:11	652	88	4.0F,	,	,	,	,	,	
11:07:24	652	88	4.0F,	,	,	,	,	,	
11:08:37	652	88	4.0F,	,	,	,	,	,	
11:09:50	652	88	4.0F,	,	,	,	,	,	
11:11:03	652	88	4.2	3.7	4	32	34	66	
11:12:16	657	88	4.2	3.7	4	33	34	67	
11:13:29	652	89	4.2	3.7	4	33	34	67	
11:14:42	652	88	4.2	3.7	4	33	34	67	
11:15:55	653	88	4.2	3.7	4	33	34	67	

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam		Baghouse Differential		Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal
	Flow	Total Air Flow	Pressure	Coal Feed			Coal Feed	Flow	
	23MSOF80 KLBH ACTUAL	23BA0F80 PERCNT ACTUAL	23PE0P4S WC ACTUAL	23BYAF10 KLBH ACTUAL			23BYBF10 KLBH ACTUAL	KLBH CALC	
11:17:08	648	88	4.2	3.7	4	33	34	67	
11:18:21	642	88	4.2	3.7	4	33	34	67	
11:19:34	648	88	4.2	3.7	4	33	34	67	
11:20:47	648	87	4.2	3.7	4	33	34	67	
11:22:00	648	88	4.2	3.7	4	33	34	67	
11:23:13	653	88	4.7	3.7	4	33	34	67	
11:24:26	653	88	4.3	3.7	4	33	34	67	
11:25:39	653	88	4.3	3.7	4	33	34	67	
	<b>650.2</b>	<b>87.7</b>	<b>4.45</b>	<b>3.71</b>	<b>3.8</b>	<b>33.0</b>	<b>34.0</b>	<b>67.0</b>	
12:00:56	653	88	4.6	3.7	3	33	34	67	
12:02:09	653	88	4.6	3.7	3	33	34	67	
12:03:22	653	89	4.6	3.7	3	33	34	67	
12:04:35	653	89	4.6	3.7	3	33	34	67	
12:05:48	652	89	4.6	3.7	3	33	34	67	
12:07:01	652	88	4.6	3.7	3	33	34	67	
12:08:14	658	89	4.6	3.7	3	33	34	67	
12:09:27	652	88	4.6	3.7	3	33	34	67	
12:10:40	652	88	4.6	3.7	3	33	34	67	
12:11:53	652	88	4.7	3.7	3	33	34	67	
12:13:06	647	88	4.7	3.7	3	33	34	67	
12:14:19	652	88	4.7	3.9	3	33	34	67	
12:15:32	652	88	4.7	3.7	3	33	34	67	
12:16:45	652	88	4.7	3.7	3	33	34	67	
12:17:58	652	88	4.8	3.7	3	33	34	67	
12:19:11	652	88	4.8	3.7	3	33	34	67	
12:20:24	656	89	4.8	3.7	3	33	34	67	
12:21:37	651	89	4.8	3.7	3	33	34	67	
12:22:50	656	89	4.8	3.7	3	33	34	67	
12:24:03	656	89	4.8	3.7	3	33	34	67	
12:25:16	656	88	4.8	3.7	3	33	34	67	
12:26:29	650	87	4.8	3.7	3	33	36	69	
12:27:42	655	89	2.4	3.7	3	33	34	67	
12:28:55	650	87	6.3	3.7	3	33	34	67	
12:30:08	650	89	5.7	3.7	3	33	34	67	
12:31:21	655	89	5.9	3.7	3	33	34	67	
12:32:34	655	88	5.7	3.7	3	33	34	67	
12:33:47	655	88	5.7	3.7	3	33	34	67	
12:35:00	654	88	5.6	3.7	3	33	34	67	
12:36:13	648	88	5.6	3.7	3	33	34	67	
12:37:26	653	89	5.6	3.7	3	33	34	67	
12:38:39	653	89	5.6	3.7	3	32	34	66	
12:39:52	653	89	5.6	3.7	3	32	34	66	
12:41:05	653	87	5.3	3.7	3	33	34	67	
12:42:18	659	89	5.8	3.7	3	33	34	67	
12:43:31	653	89	6.5	3.7	3	33	34	67	
12:44:44	648	87	5.5	3.7	3	33	34	67	
12:45:57	648	88	5.5	3.7	3	33	34	67	
12:47:10	653	87	5.1	3.7	3	33	34	67	
12:48:23	653	89	5.4	3.7	3	33	34	67	
12:49:36	653	88	5.4	3.7	3	33	34	67	
12:50:49	653	88	5.4	3.7	3	33	34	67	
12:52:02	654	87	6.3	3.7	3	33	34	67	
12:53:15	652	88	5.4	3.7	3	33	34	67	
12:54:28	652	88	5.1	3.7	3	33	34	67	
12:55:41	652	88	5.4	3.7	3	33	34	67	
12:56:54	652	88	7.5	3.7	3	33	34	67	



Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam		Baghouse Differential		Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal
	Flow	Total Air Flow	Pressure	Coal Feed			Coal Feed	Flow	
	23MS0F80	23BA0F80	23PE0P4S	23BYAF10			23BYBF10		
	KLBH	PERCNT	WC	KLBH			KLBH	KLBH	
	ACTUAL	ACTUAL	ACTUAL			ACTUAL	ACTUAL	CALC	
12:58:07	652	88	2.4	3.7	3	33	34	67	
12:59:20	652	88	5	3.7	3	33	34	67	
13:00:33	652	88	4.6	3.7	3	33	34	67	
13:01:46	652	88	4.6	3.7	3	33	34	67	
13:02:59	652	89	4.6	3.7	3	33	34	67	
13:04:12	647	88	4.5	3.7	3	33	34	67	
13:05:25	652	88	4.1	3.7	3	33	34	67	
13:06:38	652	88	5	3.7	3	33	34	67	
13:07:51	652	88	5	3.7	3	33	34	67	
13:09:04	652	88	5	3.7	3	33	34	67	
13:10:17	652	89	4.5	3.7	4	33	34	67	
13:11:30	652	88	4.5	3.7	4	33	34	67	
13:12:43	652	88	4.5	3.7	4	32	34	66	
13:13:56	652	88	4.7	3.7	4	33	34	67	
13:15:09	652	88	4.7	3.7	4	32	34	66	
13:16:22	657	89	3.7	3.7	5	33	34	67	
13:17:35	657	89	3.7	3.7	4	33	34	67	
13:18:48	657	89	3.9	3.7	4	33	34	67	
13:20:01	652	89	3.9	3.7	4	33	34	67	
13:21:14	658	88	3.9	3.7	4	33	34	67	
13:22:27	653	88	3.9	3.7	4	33	34	67	
13:23:40	653	89	8.3	3.7	4	33	34	67	
13:24:53	652	89	6.2	3.7	4	33	34	67	
13:26:06	658	89	4.8	3.7	4	33	34	67	
13:27:19	653	88	4.9	3.7	4	33	34	67	
13:28:32	653	88	4.9	3.7	4	33	34	67	
13:29:45	653	88	4.5	3.7	4	33	34	67	
13:30:58	653	88	4.8	3.7	4	33	34	67	
13:32:11	658	88	4.8	3.7	4	33	34	67	
13:33:24	657	88	4.8	3.7	4	33	34	67	
13:34:37	657	88	4.8	3.7	4	33	34	67	
13:35:50	657	88	4.2	3.7	4	33	34	67	
13:37:03	651	89	4.5	3.7	4	33	34	67	
13:38:16	656	88	4.5	3.7	4	33	34	67	
13:39:29	656	88	4.8	3.7	4	33	34	67	
13:40:42	656	88	4.9	3.7	4	33	34	67	
13:41:55	657	88	4.7	3.7	4	33	34	67	
13:43:08	657	88	4.5	3.7	4	33	34	67	
13:44:21	651	88	4.5	3.7	4	33	34	67	
13:45:34	656	88	4.5	3.7	4	32	34	66	
13:46:47	656	88	4.8	3.7	4	33	34	67	
13:48:00	649	87	4.6	3.7	4	32	34	66	
13:49:13	649	87	4.5	3.7	3	32	34	66	
13:50:26	652	88	4.5	3.7	3	33	34	67	
13:51:39	647	87	4.5	3.7	3	32	33	65	
13:52:52	647	87	4.5	3.7	3	32	34	66	
13:54:05	647	87	4.5	3.7	3	32	33	65	
13:55:18	647	87	4	3.7	3	32	34	66	
13:56:31	647	87	4	3.7	3	32	34	66	
13:57:44	647	87	4	3.7	3	32	33	65	
13:58:57	647	87	4	3.7	3	32	33	65	
14:00:10	647	87	4.3	3.7	3	32	33	65	
14:01:23	647	87	4.4	3.7	3	32	33	65	
14:02:36	647	87	4.5	3.7	3	32	33	65	
14:03:49	647	87	4.5	3.7	3	32	33	65	
14:05:02	645	87	3.5	3.7	3	33	33	66	

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam		Baghouse Differential		Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal Flow KLBH CALC
	Flow	Total Air Flow	Pressure	Coal Feed			Coal Feed		
	23MS0F80 KLBH ACTUAL	23BA0F80 PERCNT ACTUAL	23PE0P4S WC ACTUAL	23BYAF10 KLBH ACTUAL			23BYBF10 KLBH ACTUAL		
14:06:15	650	87	4.3	3.7	3	33	34	67	
14:07:28	649	87	4.5	3.7	3	32	33	65	
14:08:41	648	87	4.5	3.7	3	32	34	66	
14:09:54	648	88	4.5	3.7	3	32	33	65	
14:11:07	648	88	4.5	3.7	3	32	33	65	
14:12:20	648	87	3.5	3.7	3	32	33	65	
14:13:33	648	88	3.5	3.7	3	32	34	66	
14:14:46	642	87	3.5	3.7	3	32	33	65	
14:15:59	648	87	3.8	3.7	3	32	34	66	
14:17:12	648	88	3.8	3.7	3	32	33	65	
	<b>652.0</b>	<b>88.0</b>	<b>4.75</b>	<b>3.70</b>	<b>3.3</b>	<b>32.8</b>	<b>33.9</b>	<b>66.6</b>	
14:50:03	647	88	4.1	3.7	3	32	33	65	
14:51:16	642	88	4.3	3.7	3	32	33	65	
14:52:29	647	88	4.3	3.7	3	32	34	66	
14:53:42	642	88	4.3	3.7	3	32	34	66	
14:54:55	647	88	4.3	3.7	3	32	34	66	
14:56:08	647	88	4.3	3.7	3	32	34	66	
14:57:21	647	88	4.3	3.7	3	32	33	65	
14:58:34	652	88	4.3	3.7	3	32	33	65	
14:59:47	646	88	4.3	3.7	3	32	33	65	
15:01:00	648	88	4.3	3.9	3	32	33	65	
15:02:13	646	88	4.3	3.9	3	32	33	65	
15:03:26	646	88	4.3	3.9	3	32	34	66	
15:04:39	646	88	4.3	3.9	3	32	33	65	
15:05:52	651	88	4.3	3.7	3	32	34	66	
15:07:05	645	88	4.3	3.7	3	32	33	65	
15:08:18	645	88	4.3	3.7	3	32	33	65	
15:09:31	645	88	4.3	3.7	3	32	33	65	
15:10:44	645	87	4.3	3.7	3	32	34	66	
15:11:57	645	88	4.3	3.7	3	32	33	65	
15:13:10	645	87	4.3	3.7	3	32	33	65	
15:14:23	645	88	4.5	3.7	3	32	33	65	
15:15:36	650	88	4.5	3.7	3	32	33	65	
15:16:49	644	87	4.5	3.7	3	32	33	65	
15:18:02	644	87	6.9	3.7	3	32	33	65	
15:19:15	644	88	7.3	3.7	3	32	34	66	
15:20:28	644	87	5.1	3.7	3	32	33	65	
15:21:41	650	87	5.3	3.7	3	32	33	65	
15:22:54	650	88	5.3	3.7	3	32	33	65	
15:24:07	650	88	4.4	3.7	3	32	34	66	
15:25:20	645	87	5	3.7	3	32	33	65	
15:26:33	645	88	5.2	3.7	3	32	34	66	
15:27:46	645	88	5.2	3.7	3	32	34	66	
15:28:59	645	88	5.2	3.7	3	32	33	65	
15:30:12	645	87	5.2	3.7	3	32	33	65	
15:31:25	645	88	5.1	3.7	3	32	33	65	
15:32:38	645	88	5.1	3.7	3	32	34	66	
15:33:51	650	88	5.1	3.7	3	32	34	66	
15:35:04	644	88	5.1	3.7	3	32	34	66	
15:36:17	644	88	5.1	3.7	3	32	34	66	
15:37:30	644	87	4.7	3.7	3	32	33	65	
15:38:43	644	88	4.9	3.7	3	32	33	65	
15:39:56	644	87	4.9	3.7	3	32	34	66	
15:41:09	644	87	4.9	3.7	3	32	33	65	
15:42:22	644	87	4.9	3.7	3	32	33	65	
15:43:35	644	87	4.2	3.7	3	32	33	65	

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam	Total Air Flow 23BA0F80 PERCNT ACTUAL	Baghouse	Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal Flow KLBH CALC
	Flow		Differential			Coal Feed	Coal Feed	
	23MS0F80 KLBH ACTUAL		Pressure 23PE0P4S WC ACTUAL			23BYAF10 KLBH ACTUAL	23BYBF10 KLBH ACTUAL	
15:44:48	643	87	4.9	3.7	3	32	34	66
15:46:01	643	87	4.7	3.7	3	32	34	66
15:47:14	643	87	4.7	3.7	3	32	33	65
15:48:27	649	87	2.3	3.7	3	32	34	66
15:49:40	649	88	1.9	3.7	4	32	33	65
15:50:53	649	88	4.4	3.7	3	32	34	66
15:52:06	642	87	4.4	3.7	3	32	34	66
15:53:19	642	88	4.4	3.7	3	32	34	66
15:54:32	648	88	4.4	3.7	3	32	33	65
15:55:45	641	87	4.4	3.9	3	32	33	65
15:56:58	641	87	4.7	3.9	3	32	33	65
15:58:11	647	87	4.7	3.7	3	32	33	65
15:59:24	647	87	4.7	3.7	3	32	34	66
16:00:37	640	87	4.4	3.7	3	32	34	66
16:01:50	645	87	4.6	3.7	3	32	33	65
16:03:03	645	87	4.4	3.7	3	32	33	65
16:04:16	645	87	4.6	3.7	3	32	33	65
16:05:29	645	88	4.6	3.7	3	32	33	65
16:06:42	640	87	3.5	3.7	3	32	33	65
16:07:55	640	87	3.7	3.7	3	32	33	65
16:09:08	645	87	3.8	3.7	3	32	33	65
16:10:21	645	88	3.8	3.7	3	32	34	66
16:11:34	645	88	3.8	3.7	3	32	33	65
16:12:47	645	88	3.8	3.7	3	32	34	66
16:14:00	645	88	3.8	3.7	3	32	34	66
16:15:13	645	88	3.8	3.7	3	32	33	65
16:16:26	644	87	8.4	3.7	3	32	33	65
16:17:39	644	87	4.6	3.7	3	32	33	65
16:18:52	649	87	4.8	3.7	3	32	34	66
16:20:05	649	87	4.6	3.7	3	32	34	66
16:21:18	644	87	4.6	3.7	3	32	33	65
16:22:31	638	87	4.4	3.7	3	32	33	65
16:23:44	644	89	4.6	3.7	3	32	34	66
16:24:57	643	88	4.6	3.9	3	32	34	66
16:26:10	643	88	4.6	3.9	3	32	33	65
16:27:23	648	88	4.6	3.9	3	32	33	65
16:28:36	643	88	4.9	3.9	3	32	33	65
16:29:49	636	88	4.7	3.9	3	32	33	65
16:31:02	641	88	4.7	3.9	3	32	34	66
16:32:15	641	88	4.7	3.9	3	33	34	67
16:33:28	641	88	4.7	3.7	3	32	33	65
16:34:41	641	88	4.7	3.7	3	32	33	65
16:35:54	647	88	4.7	3.7	3	32	33	65
16:37:07	642	88	4.5	3.7	3	32	34	66
16:38:20	642	88	4.7	3.7	3	32	34	66
16:39:33	642	88	4.7	3.7	3	32	33	65
16:40:46	642	88	4.8	3.7	3	32	33	65
16:41:59	642	88	4.5	3.7	3	32	33	65
16:43:12	642	88	4.7	3.7	3	32	34	66
16:44:25	642	88	4.7	3.7	3	32	34	66
16:45:38	642	88	2.5	3.7	3	32	33	65
16:46:51	648	88	4.6	3.7	3	32	33	65
16:48:04	647	88	4	3.7	3	32	33	65
16:49:17	641	88	4	3.9	3	32	34	66
16:50:30	641	88	4	3.7	3	32	33	65
16:51:43	642	88	4	3.7	3	32	34	66

Historical Tabular Trend 5  
30-Nov-99

Time	Main Steam	Total Air Flow 23BA0F80 PERCNT ACTUAL	Baghouse	Boiler O2 O021Z006 PCT ACTUAL	Boiler Opacity 23BA0A90 PERCNT ACTUAL	3A Pulverized	3B Pulverized	Total Coal Flow KLBH CALC
	Flow		Differential			Coal Feed	Coal Feed	
	23MSOF80		Pressure			23BYAF10	23BYBF10	
	KLBH		23PE0P4S WC ACTUAL			KLBH	KLBH	
16:52:56	636	87	4	3.7	3	32	34	66
16:54:09	642	89	4.6	3.7	3	32	33	65
16:55:22	642	88	4.6	3.7	3	32	33	65
16:56:35	642	88	4.6	3.7	3	32	33	65
16:57:48	642	88	3.7	3.7	3	32	33	65
16:59:01	648	88	4.4	3.7	3	32	34	66
17:00:14	642	88	4.4	3.9	3	32	33	65
17:01:27	642	88	4.4	3.9	3	32	33	65
17:02:40	642	88	4.6	3.7	3	32	33	65
17:03:53	642	88	4.7	3.7	3	32	33	65
17:05:06	642	88	3.7	3.7	3	32	33	65
17:06:19	642	88	3.7	3.7	3	32	33	65
17:07:32	642	87	3.7	3.7	3	32	33	65
17:08:45	642	87	3.7	3.7	3	32	33	65
17:09:58	642	87	3.7	3.7	3	32	33	65
	<b>644.3</b>	<b>87.7</b>	<b>4.50</b>	<b>3.73</b>	<b>3.0</b>	<b>32.0</b>	<b>33.4</b>	<b>65.4</b>





## SUMMARY OF RESULTS CALCULATIONS

$$V_m (\text{std}) = 17.647 \times V_m \times \left[ \frac{P_{\text{bar}} + \frac{DH}{13.6}}{(460 + T_m)} \right] \times Y$$

$$V_w (\text{std}) = 0.0471 \times V_{lc}$$

$V_{lc}$  = water + silica net

$$B_{ws} = \left[ \frac{V_w (\text{std})}{V_w (\text{std}) + V_m (\text{std})} \right]$$

$$M_d = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$M_S = M_d \times (1 - B_{ws}) + (18 \times B_{ws})$$

$$V_s = \sqrt{\frac{(T_s + 460)}{M_s \times P_s}} \times \sqrt{DP} \times C_p \times 85.49$$

- $C_p$  = pitot tube correction factor
- $P_s$  = absolute flue gas pressure
- $M_s$  = molecular weight of gas (lb/lb mole)
- $M_d$  = dry molecular weight of gas (lb/lb mole)
- $B_{ws}$  = water vapor in gas stream proportion by volume

$$A_{cfm} = V_s \times \text{Area (of stack or duct)} \times 60$$

$$D_{scfm} = A_{cfm} \times 17.647 \times \left[ \frac{P_s}{(460 + T_s)} \right] \times (1 - B_{ws})$$

$$S_{cfm} = A_{cfm} \times 17.647 \times \left[ \frac{P_s}{(460 + T_s)} \right]$$

$$S_{cfh} = S_{cfm} \times 60 \frac{\text{min}}{\text{hr}}$$

## CALCULATION FORMULAS

1. 
$$V_{m(\text{std})} = V_m Y \left( \frac{T_{\text{std}}}{T_m} \right) \left( \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{P_{\text{std}}} \right) = K_1 V_m Y \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{T_m}$$
2. 
$$V_{w(\text{std})} = V_{lc} \left( \frac{\rho_w}{M_w} \right) \left( \frac{RT_{\text{std}}}{P_{\text{std}}} \right) = K_2 V_{lc}$$
3. 
$$B_{ws} = \frac{V_{w(\text{std})}}{V_{m(\text{std})} + V_{w(\text{std})}}$$
- 4a. 
$$C_a = \frac{m_a}{V_a \rho_a}$$
- 4b. 
$$W_a = C_a V_{aw} \rho_a$$
5. 
$$C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(\text{std})})$$
6. 
$$C_{\text{acf}} = 15.43 K_i \left( \frac{m_n P_s}{V_{w(\text{std})} + V_{m(\text{std})} T_s} \right)$$
7. 
$$\%EA = \left( \frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$
8. 
$$M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO)$$
9. 
$$M_s = M_d(1 - B_{ws}) + 18.0 B_{ws}$$
10. 
$$v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$
11. 
$$Q_{\text{acfm}} = v_s A (60_{\text{sec/min}})$$
12. 
$$Q_{\text{sd}} = (3600_{\text{sec/hr}})(1 - B_{ws}) v_s \left( \frac{T_{\text{std}} P_s}{T_s P_{\text{std}}} \right) A$$
13. 
$$E \text{ (emission rate, lbs/hr)} = Q_{\text{std}} (C_s / 7000 \text{ grains/lb})$$
14. 
$$IKV = \frac{T_s V_{m(\text{std})} P_{\text{std}}}{T_{\text{std}} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(\text{std})}}{P_s v_s A_n \theta (1 - B_{ws})}$$



## NOMENCLATURE

- A = Cross-sectional area of stack or duct, ft<sup>2</sup>  
 A<sub>n</sub> = Cross-sectional area of nozzle, ft<sup>2</sup>  
 B<sub>ws</sub> = Water vapor in gas stream, proportion by volume  
 C<sub>a</sub> = Acetone blank residue concentration, g/g  
 C<sub>acf</sub> = Concentration of particulate matter in gas stream at actual conditions, gr/acf  
 C<sub>p</sub> = Pitot tube coefficient, dimensionless  
 C<sub>s</sub> = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf  
 IKV = Isokinetic sampling variance, must be .90 ≤ IKV ≤ 1.10  
 M<sub>d</sub> = Dry molecular weight of gas, lb/lb-mole  
 m<sub>n</sub> = Total amount of particulate matter collected, grams  
 M<sub>s</sub> = Molecular weight of gas, wet basis, lb/lb-mole  
 M<sub>w</sub> = Molecular weight of water, 18.0 lb/lb-mole  
 m<sub>a</sub> = Mass of residue of acetone after evaporation, grams  
 P<sub>bar</sub> = Barometric pressure at testing site, in. Hg  
 P<sub>g</sub> = Static pressure of gas, in. Hg (in. H<sub>2</sub>O/13.6)  
 P<sub>s</sub> = Absolute pressure of gas, in. Hg = P<sub>bar</sub> + P<sub>g</sub>  
 P<sub>std</sub> = Standard absolute pressure, 29.92 in. Hg  
 Q<sub>acfm</sub> = Actual volumetric gas flow rate, acfm  
 Q<sub>sd</sub> = Dry volumetric gas flow rate corrected to standard conditions, dscf/hr  
 R = Ideal gas constant, 21.85 in. Hg-ft<sup>3</sup>/°R-lb-mole  
 T<sub>m</sub> = Absolute dry gas meter temperature, °R  
 T<sub>s</sub> = Absolute gas temperature, °R  
 T<sub>std</sub> = Standard absolute temperature, 528°R  
 V<sub>a</sub> = Volume of acetone blank, ml  
 V<sub>aw</sub> = Volume of acetone used in wash, ml  
 V<sub>lc</sub> = Total volume of liquid collected in impingers and silica gel, ml  
 V<sub>m</sub> = Volume of gas sample as measured by dry gas meter, dcf  
 V<sub>m(std)</sub> = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf  
 v<sub>s</sub> = Gas velocity, ft/sec  
 V<sub>w(std)</sub> = Volume of water vapor in gas sample, corrected to standard conditions, scf  
 W<sub>a</sub> = Weight of residue in acetone wash, grams  
 Y = Dry gas meter calibration factor  
 ΔH = Average pressure differential across the orifice meter, in. H<sub>2</sub>O  
 Δp = Velocity head of gas, in. H<sub>2</sub>O  
 ρ<sub>a</sub> = Density of acetone, 0.7855 g/ml (average)  
 ρ<sub>w</sub> = Density of water, 0.002201 lb/ml  
 θ = Total sampling time, minutes  
 K<sub>1</sub> = 17.64 °R/in. Hg  
 K<sub>2</sub> = 0.04707 ft<sup>3</sup>/ml  
 K<sub>4</sub> = 0.09450/100 = 0.000945  

$$K_p = \text{Pitot tube constant, } 85.49 \frac{\text{ft}}{\text{sec}} \left[ \frac{(\text{lb/lb - mole})(\text{in. Hg})}{(^\circ\text{R})(\text{in. H}_2\text{O})} \right]^{1/2}$$
 %EA = Percent excess air  
 %CO<sub>2</sub> = Percent carbon dioxide by volume, dry basis  
 %O<sub>2</sub> = Percent oxygen by volume, dry basis  
 %CO = Percent carbon monoxide by volume, dry basis  
 %N<sub>2</sub> = Percent nitrogen by volume, dry basis  
 0.264 = Ratio of O<sub>2</sub> to N<sub>2</sub> in air, v/v  
 0.28 = Molecular weight of N<sub>2</sub> or CO, divided by 100  
 0.32 = Molecular weight of O<sub>2</sub> divided by 100  
 0.44 = Molecular weight of CO<sub>2</sub> divided by 100  
 13.6 = Specific gravity of mercury (Hg)

## MERCURY CALCULATIONS

### Determination of Speciated Mercury

#### Concentration

$$\frac{\text{ug of Mercury detected} \times \frac{10^{-6} \text{ g}}{\text{ug}}}{453.6 \text{ g/lb}} = \text{lbs Mercury/sample}$$

$$\frac{\text{lbs Mercury/sample}}{V_m(\text{std})} = \text{lbs Mercury/dscf}$$

#### Emission Rates

$$\text{lbs Mercury/hr} = \text{lbs/dscf} \times \text{dscf/min} \times 60 \text{ min/hr}$$

$$\text{lbs Mercury}/10^{12} \text{ Btu} = \text{lbs/dscf} \times F_d \text{ Factor}(\text{dscf}/10^6 \text{ Btu}) \times \frac{20.9\%}{20.9\% - O_2\%} \times 10^6$$

#### Mercury Fractions

Elemental Mercury Catch – mercury collected in the acidified hydrogen peroxide (HNO<sub>3</sub>-H<sub>2</sub>O<sub>2</sub>) and potassium permanganate (H<sub>2</sub>SO<sub>4</sub>-KMnO<sub>4</sub>) impinger solutions.

Oxidized Mercury Catch – mercury collected in the aqueous potassium chloride (KCl) impinger solution.

Particle-bound Mercury Catch – mercury associated with the particulate matter collected in the front half of the sampling train.

### Determination of Mercury Available from Coal

$$\text{lbs Mercury/hr} = \frac{\text{ug Mercury}}{\text{g Coal}}(\text{dry}) \times \frac{10^{-6} \text{ g}}{\text{ug}} \times \frac{\text{lbs Coal (wet)}}{\text{hr}} \times (1 - B_{ws}) \text{ moisture corr.}$$

$$\text{lbs Mercury}/10^{12} \text{ Btu} = \frac{\text{lbs Mercury}}{\text{hr}} \div \frac{10^{12} \text{ Btu}}{\text{hr}}$$

## EMISSION RATE CALCULATIONS

A pollutant emission rate (E), expressed as pounds of pollutant per million Btu heat input from the fuel combusted can be calculated by several methods as follows:

1.  $C = C_s/7000$  where, C = pollutant concentration, lb/dscf  
 $c_s$  = pollutant concentration, grains/dscf
2. If fuel flow is monitored and the fuel combusted during the test is sampled and analyzed for gross calorific value, then:

$$E = \frac{Q_{sd} C}{\text{fuel flow rate (lb / hr) GCV}} \times 10^6$$

where, E = lbs per million Btu

GCV = gross calorific value, Btu / lb

$Q_{sd}$  = dry volumetric gas flow at standard conditions, dscf / hr

3. If an integrated gas sample is taken during the test and analyzed for %CO<sub>2</sub> or %O<sub>2</sub>, dry basis by volume, with an Orsat gas analyzer, then

$$E = C F_c \frac{100}{(\%CO_2)} \text{ or, } E = C F \frac{20.9}{(20.9 - \%O_2)} \text{ where,}$$

%CO<sub>2</sub> and %O<sub>2</sub> are expressed as percent; and, for example, for subbituminous and bituminous coals:

$F_c$  = a factor representing a ratio of the volume of carbon dioxide generated to the calorific value of the fuel combusted, 1800 scf CO<sub>2</sub>/million Btu.

F = a factor representing a ratio of the volume of dry flue gases generated to the calorific value of the fuel combusted, 9780 dscf/million Btu.

4. If fuel sample increments are taken and composited during the test and an ultimate analysis is performed and the GCV is determined, then

$$F_c = \frac{321 \times 10^3 (\%C)}{GCV} \text{ where, \%C = carbon content by weight expressed as percent}$$

$$F = \frac{[3.64 (\%H) + 1.53 (\%C) + 0.57 (\%S) + 0.14 (\%N) - 0.46 (\%O_2)]}{GVC} \times 10^6$$

where, H, C, S, N, and O are content by weight of hydrogen, carbon, sulfur, nitrogen, and oxygen (expressed as percent) respectively.

5. If fuels other than subbituminous and bituminous coals are fired, other F-factors than those above will apply; and, if combinations of different fuels are fired, the F-factors must be prorated according to the fraction of the total heat input derived from each type of fuel.







MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 1

COMPANY: WEPCO THIMBLE NO: 071 TARE WT: 3.1408  
 PLANT: Valley Power Plant FILTER NO: \_\_\_\_\_ TARE WT: \_\_\_\_\_  
 TEST LOCATION: Boiler #3 Inlet BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPRI FLUE PRESSURE in. H<sub>2</sub>O: -13.5  
 OPERATOR: D. Helm FLUE PRESSURE in. Hg ABS: 29.117  
 DATE: 11/30/99 PROBE LENGTH: 10 ft.  
 CONTROL BOX: E12 POT. NO.: E12 PROBE LINER MATERIAL: Teflon  
 METER NO.: E12 NOZZLE IDENTIFICATION NO: 8  
 METER CALIBRATION FACTOR: 0.997 CALIBRATED NOZZLE DIAMETER: 0.240  
 PITOT ID NO.: 427 A LEAK CHECK: PRE: 0.008 POST: 0.005 @ // in. Hg  
 PITOT TUBE COEFFICIENT: 0.830 DUCT SHAPE: Rectangular DIAMETER: \_\_\_\_\_  
 PORT LENGTH: 28 in. DUCT AREA: 120.33 sq. ft. L 12.8" W 9.6"  
 PORT SIZE: 6 in. DISTURBANCE UPSTREAM: \_\_\_\_\_ DOWNSTREAM: \_\_\_\_\_  
 PORT TYPE: Flange TEST LENGTH: 125 MINUTES PER POINT: 5  
 IMPINGER H<sub>2</sub>O SILICA GEL: TOTAL NUMBER OF TRAVERSE POINTS: 25  
 FINAL: 4698.9 ml/gm FINAL WT: 723.8 gm  
 INITIAL: 4597.0 ml/gm INITIAL WT: 712.4 gm  
 GAIN: 101.9 ml/gm WT. GAIN: 11.4 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 113.3  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: \_\_\_\_\_  
 SILICA GEL EXHAUSTED?: \_\_\_\_\_  
 IMPINGERS RECOVERED BY: \_\_\_\_\_  
 SILICA GEL WEIGHED BY: \_\_\_\_\_  
 PITOT LEAK CHECK: PRE  POST   
 AH@ \_\_\_\_\_  
 SAMPLES REMOVED FROM SITE BY: \_\_\_\_\_

For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9,780 F<sub>c</sub> = 1,800 Other = \_\_\_\_\_  
 Circle to indicate "Yes" or add other value if not given.

COMMENTS & NOTES

FIELD TEST DATA SHEET  
FOR ISOKINETIC SAMPLING

MOSTARDI-PLATT ASSOCIATES, INC.

PROJECT WEP CO - Valley  
TEST RUN NO. 01  
TEST LOCATION Boiler #9 - Inlet

DATE 30 Nov 99 PAGE 1 OF 2

Port-Point No.	Velocity Head (P) in. H <sub>2</sub> O	√P	Clock Time 24 hr.	Meter Volume (M <sup>3</sup> ) ft.	Office In. H <sub>2</sub> O (H)	Stack Temp (t) °F	Meter Temp. (t)		Meter Rate cfm	Pump Vacuum in. Hg	Notes	Probe Temp. °F	Filter Holder Temp. °F	Impinger Outlet Temp. °F
							Inlet °F	Outlet °F						
1-1	0.38	0.614	901	17.024	0.66	328	38	34	0.462	5	2.309	237	231	268
1-2	0.42	0.648	906	19.390	0.73	324	41	35	0.486	4	2.427	235	232	268
1-3	0.43	0.655	911	21.710	0.75	317	43	38	0.491	5	2.456	235	232	268
1-4	0.41	0.640	916	24.170	0.71	311	44	37	0.480	5	2.398	237	232	268
1-5	0.43	0.655	921	26.670	0.75	297	45	38	0.491	5	2.456	239	233	268
		0.643	926	29.020	0.72	315	42	36			29.070			
				11.906							12.046			
2-1	0.40	0.632	927	29.550	0.70	324	46	39	0.474	5	2.369	237	231	
2-2	0.43	0.657	932	31.880	0.75	320	47	39	0.491	5	2.456	236	231	
2-3	0.47	0.685	937	34.310	0.82	315	48	40	0.514	5	2.568	240	232	
2-4	0.45	0.670	942	36.980	0.78	308	48	41	0.503	5	2.513	240	232	
2-5	0.29	0.538	947	39.410	0.51	287	49	42	0.403	4	2.017	242	232	
		0.636	952	41.450	0.72	310	47	40			41.473			
				11.900							11.923			
3-1	0.46	0.678	954	41.865	0.80	330	49	42	0.508	5	2.540	232	231	
3-2	0.46	0.678	959	44.400	0.80	328	49	43	0.508	5	2.540	234	232	
3-3	0.47	0.685	1004	46.980	0.82	319	50	43	0.514	5	2.568	234	232	
3-4	0.55	0.741	1009	49.540	0.96	311	51	44	0.536	6	2.778	235	232	
3-5	0.38	0.614	1014	52.320	0.66	297	51	44	0.462	5	2.309	235	231	
		0.680	1019	54.660	0.80	317	50	43			54.600			
				12.790							12.735			
4-1	0.54	0.734	1021	55.215	0.94	330	51	45	0.551	6	2.752	235	231	
4-2	0.50	0.707	1026	58.010	0.87	325	51	46	0.530	6	2.649	236	231	
4-3	0.48	0.692	1031	60.690	0.84	320	52	46	0.519	6	2.595	236	231	
4-4	0.48	0.692	1036	63.270	0.84	313	52	46	0.519	6	2.595	237	232	
4-5	0.36	0.600	1041	65.890	0.63	288	52	46	0.450	6	2.247	238	232	
		0.685	1046	68.100	0.82	315	51	46			68.053			
				12.885							12.838			





MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 2

COMPANY: WECCO THIMBLE NO: 069 TARE WT: 3.3274  
 PLANT: Valley FILTER NO: \_\_\_\_\_ TARE WT: \_\_\_\_\_  
 TEST LOCATION: Boiler #3 BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPR FLUE PRESSURE in. H<sub>2</sub>O: -13.5  
 OPERATOR: D. Helms FLUE PRESSURE in. Hg ABS: 29.117  
 DATE: 11/30/99 PROBE LENGTH: 10 ft.  
 CONTROL BOX: E12 POT. NO.: E12  
 METER NO.: E12 PROBE LINER MATERIAL: Teflon  
 METER CALIBRATION FACTOR: 0.997 NOZZLE IDENTIFICATION NO: 8  
 PITOT ID NO.: 427A CALIBRATED NOZZLE DIAMETER: 0.240  
 PITOT TUBE COEFFICIENT: 0.830 LEAK CHECK: PRE: 0.007 POST: 0.005 @ 11 in. Hg  
 PORT LENGTH: 28 in. DUCT SHAPE: Rectangular DIAMETER: \_\_\_\_\_  
 PORT SIZE: 6 in. DUCT AREA: 120.33 sq. ft. L 12'8" W 9'6"  
 PORT TYPE: Flores DISTURBANCE UPSTREAM: \_\_\_\_\_ DOWNSTREAM: \_\_\_\_\_  
 IMPINGER H<sub>2</sub>O TEST LENGTH: 125 MINUTES PER POINT: 5  
 FINAL: 4723.3 ml/gm SILICA GEL: FINAL WT: 751.7 gm  
 INITIAL: 4626.2 ml/gm INITIAL WT: 738.5 gm  
 GAIN: 97.1 ml/gm WT. GAIN: 13.2 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 110.3  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: \_\_\_\_\_  
 SILICA GEL EXHAUSTED?: \_\_\_\_\_  
 IMPINGERS RECOVERED BY: \_\_\_\_\_  
 SILICA GEL WEIGHED BY: \_\_\_\_\_

PITOT LEAK CHECK: PRE  POST   
 ΔH@ \_\_\_\_\_  
 SAMPLES REMOVED FROM SITE BY: \_\_\_\_\_  
 For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9.780 F<sub>c</sub> = 1.800 Other = \_\_\_\_\_  
 Circle to indicate "Yes" or add other value if not given.

COMMENTS & NOTES

FIELD TEST DATA SHEET  
FOR ISOKINETIC SAMPLING

MOSTARDI-PLATT ASSOCIATES, INC.

PROJECT WEPLO - VALLEY

TEST RUN NO. #2

TEST LOCATION Boiler - #3 - JULIET

DATE 30 Nov 99

PAGE 1 OF 2

Port-Point No.	Velocity Head (P) in. H <sub>2</sub> O	√P	Clock Time 24 hr.	Meter Volume (V <sub>m</sub> ) ft <sup>3</sup>	Orifice (H) in. H <sub>2</sub> O	Stack Temp (t <sub>s</sub> ) °F	Meter Temp. (t <sub>m</sub> )		Meter Rate cfm	Pump Vacuum in. Hg	Notes	Probe Temp. °F	Filter Holder Temp. °F	Impinger Outlet Temp. °F
							Inlet °F	Outlet °F						
1-1	0.44	0.6633	1200	81.685	0.77	324	50	47	0.509	6	2.546	240	230	<680
1-2	0.43	0.6557	1205	84.190	0.77	322	52	48	0.503	7	2.516	241	231	FULLY
1-3	0.40	0.6325	1210	86.720	0.72	314	56	49	0.485	6	2.427	241	231	ICE
1-4	0.40	0.6325	1215	89.130	0.72	310	59	50	0.485	6	2.427	241	230	
1-5	0.43	0.6557	1220	91.650	0.77	296	61	52	0.503	6	2.516	242	231	
		0.6479	1225	94.150	0.754	313.6	55.6	49.2						
				12.465										
2-1	0.44	0.6633	1227	94.590	0.79	325	63	54	0.509	7	2.546	240	232	
2-2	0.48	0.6928	1232	97.170	0.86	321	63	56	0.532	7	2.659	240	231	
2-3	0.47	0.6856	1237	99.820	0.84	314	62	56	0.526	7	2.631	241	231	
2-4	0.46	0.6782	1242	102.500	0.83	309	62	55	0.521	7	2.603	241	231	
2-5	0.35	0.5916	1247	105.050	0.63	294	61	55	0.454	6	2.270	240	232	
		0.6623	1252	107.310	0.790	312.6	62.2	55.2						
				12.720										
3-1	0.45	0.6708	1254	107.600	0.81	331	62	54	0.515	7	2.574	242	232	
3-2	0.47	0.6856	1259	110.210	0.84	327	61	55	0.526	7	2.631	241	233	
3-3	0.54	0.7348	1304	112.780	0.97	320	61	56	0.564	8	2.820	242	233	
3-4	0.54	0.7348	1309	115.590	0.97	311	61	55	0.564	8	2.820	243	232	
3-5	0.33	0.5745	1314	118.420	0.59	288	60	55	0.441	6	2.205	242	231	
		0.6801	1319	120.660	0.836	315.4	61.0	55.0						
				13.060										
4-1	0.56	0.7783	1321	121.000	1.00	329	59	55	0.574	9	2.872	244	232	
4-2	0.45	0.6708	1326	123.910	0.81	324	60	55	0.515	8	2.574	245	232	
4-3	0.44	0.6633	1331	126.420	0.79	321	60	55	0.509	8	2.546	244	232	
4-4	0.58	0.7616	1336	128.990	1.04	314	60	55	0.585	9	2.923	245	231	
4-5	0.31	0.5568	1341	131.880	0.56	285	59	54	0.427	7	2.137	243	231	
		0.6862	1346	134.070	0.846	314.6	59.6	54.8						
				13.070										



MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 3

COMPANY: WEPCO THIMBLE NO: 093 TARE WT: 2.8706  
 PLANT: Valley FILTER NO: \_\_\_\_\_ TARE WT: \_\_\_\_\_  
 TEST LOCATION: Boiler #3 BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPRI FLUE PRESSURE in. H<sub>2</sub>O: -13.5  
 OPERATOR: D. Helms FLUE PRESSURE in. Hg ABS: 29.117  
 DATE: 11/30/99 PROBE LENGTH: 10 ft.  
 CONTROL BOX: E12 POT. NO.: E12  
 METER NO.: E12 NOZZLE IDENTIFICATION NO: 8  
 METER CALIBRATION FACTOR: 0.997 CALIBRATED NOZZLE DIAMETER: 0.240  
 PITOT ID NO.: 427A LEAK CHECK: PRE: 0.007 POST: 0.005 @ 11 in. Hg  
 PITOT TUBE COEFFICIENT: 0.830 DUCT SHAPE: Rectangular DIAMETER: \_\_\_\_\_  
 PORT LENGTH: 2.8 in. DUCT AREA: 120.33 sq. ft. L 12' 8" W 9' 6"  
 PORT SIZE: 6 DISTURBANCE UPSTREAM: \_\_\_\_\_ DOWNSTREAM: \_\_\_\_\_  
 PORT TYPE: Flange TEST LENGTH: 12.5 MINUTES PER POINT: 5  
 IMPINGER H<sub>2</sub>O SILICA GEL: TOTAL NUMBER OF TRAVERSE POINTS: 25  
 FINAL: 4731.0 ml/gm FINAL WT: 634.6 gm  
 INITIAL: 4630.5 ml/gm INITIAL WT: 623.2 gm  
 GAIN: 100.5 ml/gm WT. GAIN: 11.4 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 111.9  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: \_\_\_\_\_  
 SILICA GEL EXHAUSTED?: \_\_\_\_\_  
 IMPINGERS RECOVERED BY: \_\_\_\_\_  
 SILICA GEL WEIGHED BY: \_\_\_\_\_  
 PITOT LEAK CHECK: PRE  POST   
 ΔH@ \_\_\_\_\_  
 SAMPLES REMOVED FROM SITE BY: \_\_\_\_\_

COMMENTS & NOTES  
 For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9,780 F<sub>c</sub> = 1,800 Other = \_\_\_\_\_  
 Circle to indicate "Yes" or add other value if not given.









MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 1

COMPANY: WEPCo THIMBLE NO: 090 TARE WT: 3.5248  
 PLANT: Valley Power Plant FILTER NO: — TARE WT: —  
 TEST LOCATION: Boiler # 088 house BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPRI FLUE PRESSURE in. H<sub>2</sub>O: -18.0  
 OPERATOR: NS FLUE PRESSURE in. Hg ABS: —  
 DATE: 11/30/99 PROBE LENGTH: 13' ft.  
 CONTROL BOX: E51 POT. NO.: E51 PROBE LINER MATERIAL: Teflon  
 METER NO.: E51 NOZZLE IDENTIFICATION NO: #8  
 METER CALIBRATION FACTOR: 1.009 CALIBRATED NOZZLE DIAMETER: .245  
 PITOT ID NO.: 318 A LEAK CHECK: PRE: 0.00 POST: 0.00 @ 14 | 16 in. Hg  
 PITOT TUBE COEFFICIENT: 0.837 DUCT SHAPE: Rectangular DIAMETER: —  
 PORT LENGTH: 28 in. DUCT AREA: 120.83 sq. ft. L 9'6" W 12'8"  
 PORT SIZE: 6 DISTURBANCE UPSTREAM: — DOWNSTREAM: —  
 PORT TYPE: Flow TEST LENGTH: 225 MINUTES PER POINT: 5  
 IMPINGER H<sub>2</sub>O SILICA GEL:  
 FINAL: 4677.1 ml/gm FINAL WT: 808.4 gm  
 INITIAL: 4581.5 ml/gm INITIAL WT: 793.9 gm  
 GAIN: 95.6 ml/gm WT. GAIN: 14.5 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 110.1  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: —  
 SILICA GEL EXHAUSTED?: —  
 IMPINGERS RECOVERED BY: —  
 SILICA GEL WEIGHED BY: —  
 PITOT LEAK CHECK: PRE — POST —  
 ΔH@ —  
 SAMPLES REMOVED FROM SITE BY: —

For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9,780 F<sub>c</sub> = 1,800 Other = —  
 Circle to indicate "Yes" or add other value if not given.

COMMENTS & NOTES

FIELD TEST DATA SHEET  
FOR ISOKINETIC SAMPLING

MOSTARDI-PLATT ASSOCIATES, INC.

PROJECT WEPFO - Valley  
TEST RUN NO. #1  
TEST LOCATION Boiler #3 - Outlet

DATE 30 Nov 99 PAGE 1 OF 2

Port-Point No.	Velocity Head (F) in. H <sub>2</sub> O	√P	Clock Time 24 hr.	Meter Volume (V <sub>m</sub> ) ft <sup>3</sup>	Orifice (H) in. H <sub>2</sub> O	Stack Temp (t <sub>s</sub> ) °F	Meter Temp. (t <sub>m</sub> )		Pump Vacuum in. Hg	Notes	Probe Temp. °F	Filter Holder Temp. °F	Impinger Outlet Temp. °F
							Inlet °F	Outlet °F					
1-1	0.12	0.346	0900	146.168	0.237	315	37	32	8.0	1.290	246	228	268
1-2	0.44	0.663	0905	147.700	0.870	318	39	33	8.5	2.475	247	227	268
1-3	0.53	0.728	0910	149.950	1.047	318	40	34	4.5	2.720	247	227	268
1-4	0.57	0.755	0915	152.650	1.126	317	43	35	9.5	2.820	248	228	268
1-5	0.59	0.768	0920	155.510	1.166	314	46	37	9.5	2.870	247	225	268
			0925	158.350						158.343			
2-1	0.46	0.678	0930	158.350	0.909	315	47	38	9.0	2.530		225	
2-2	0.48	0.693	0935	160.600	0.949	317	50	39	9.5	2.590	250	226	
2-3	0.59	0.768	0940	163.100	1.166	317	51	40	9.5	2.870	247	229	
2-4	0.61	0.781	0945	166.350	1.205	317	55	42	10.0	2.915	246	228	
2-5	0.55	0.742	0950	169.250	1.087	312	58	43	9.5	2.770	247	228	
			0955	172.020						172.018			
3-1	0.61	0.781	1000	172.020	1.205	318	59	47	10.0	2.915	247	227	
3-2	0.63	0.794	1005	174.950	1.245	318	61	48	10.0	2.965	247	228	
3-3	0.65	0.806	1010	177.900	1.285	318	64	50	9.5	3.010	259	230	
3-4	0.54	0.735	1015	180.900	1.067	317	66	52	9.5	2.745	249	230	
3-5	0.47	0.686	1020	183.650	0.929	312	67	53	10.0	2.560	256	233	
			1025	186.220						186.213			
4-1	0.58	0.762	1030	186.220	1.146	316	67	55	9.5	2.845	247	228	
4-2	0.59	0.768	1035	189.100	1.166	318	68	57	9.5	2.870	249	229	
4-3	0.51	0.714	1040	191.900	1.008	318	64	60	9.5	2.665	249	226	
4-4	0.54	0.735	1045	194.590	1.067	317	61	60	9.0	2.745	248	227	
4-5	0.48	0.693	1050	197.200	0.949	313	63	63	9.0	2.590	246	228	
			1055	199.930						199.928			



MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 2

COMPANY: WEPCO THIMBLE NO: 091 TARE WT: 3,5580  
 PLANT: Valley FILTER NO: \_\_\_\_\_ TARE WT: \_\_\_\_\_  
 TEST LOCATION: Boiler #3 outlet BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPR I FLUE PRESSURE in. H<sub>2</sub>O: -18.0  
 OPERATOR: NS FLUE PRESSURE in. Hg ABS: \_\_\_\_\_  
 DATE: 1/30/99 PROBE LENGTH: 13' ft.  
 CONTROL BOX: E51 POT. NO.: E51 PROBE LINER MATERIAL: Teflon  
 METER NO.: E51 NOZZLE IDENTIFICATION NO: #8  
 METER CALIBRATION FACTOR: 1.009 CALIBRATED NOZZLE DIAMETER: .245  
 PITOT ID NO.: 318A LEAK CHECK: PRE: 0.0 POST: 0.0 @ 15/15 in. Hg  
 PITOT TUBE COEFFICIENT: 0.837 DUCT SHAPE: Rectangular DIAMETER: \_\_\_\_\_  
 PORT LENGTH: 28 in. DUCT AREA: 120.33 sq. ft. L 9'6" W 12'8"  
 PORT SIZE: 6 in. DISTURBANCE UPSTREAM: \_\_\_\_\_ DOWNSTREAM: \_\_\_\_\_  
 PORT TYPE: Flange TEST LENGTH: 225 MINUTES PER POINT: 5  
 IMPINGER H<sub>2</sub>O SILICA GEL: TOTAL NUMBER OF TRAVERSE POINTS: 25  
 FINAL: 4754.5 ml/gm FINAL WT: 724.3 gm  
 INITIAL: 4661.5 ml/gm INITIAL WT: 707.4 gm  
 GAIN: 93.0 ml/gm WT. GAIN: 16.9 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 109.9  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: \_\_\_\_\_  
 SILICA GEL EXHAUSTED?: \_\_\_\_\_  
 IMPINGERS RECOVERED BY: \_\_\_\_\_  
 SILICA GEL WEIGHED BY: \_\_\_\_\_  
 PITOT LEAK CHECK: PRE \_\_\_\_\_ POST \_\_\_\_\_  
 ΔH@ \_\_\_\_\_  
 SAMPLES REMOVED FROM SITE BY: \_\_\_\_\_

COMMENTS & NOTES

For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9,780 F<sub>c</sub> = 1,800 Other = \_\_\_\_\_  
 Circle to indicate "Yes" or add other value if not given.

FIELD TEST DATA SHEET  
FOR ISOKINETIC SAMPLING

MOSTARDI-PLATT ASSOCIATES, INC.

PROJECT WPCO - Valley  
TEST RUN NO. #2  
TEST LOCATION Boiler #3 - Outlet

DATE 30-Nov-99 PAGE 1 OF 2

Port-Point No.	Velocity Head (F) in. H <sub>2</sub> O	√P	Clock Time 24 Hr.	Meter Volume (V <sub>m</sub> ) ft <sup>3</sup>	Orifice (H) in. H <sub>2</sub> O	Stack Temp (t <sub>s</sub> ) °F	Meter Temp. (t <sub>m</sub> )		Meter Rate cfm	Pump Vacuum in. Hg	Notes	Probe Temp. °F	Filter Holder Temp. °F	Impinger Outlet Temp. °F
							Inlet °F	Outlet °F						
1-1	0.59	0.768	1200	212.630	1.166	318	63	73	0.574	6.5	2.870	235	230	<680
1-2	0.58	0.762	1205	215.500	1.146	318	64	75	0.569	6.0	2.845	237	233	FULLY
1-3	0.98	0.616	1210	218.400	0.757	318	67	77	0.460	6.0	2.300	247	235	ICED
1-4	0.27	0.520	1215	220.600	0.534	318	68	78	0.388	6.0	2.045	248	234	
1-5	0.30	0.548	1220	222.600	0.583	313	68	77	0.409	5.5	2.22.585	247	233	
			1225	224.630							2.24.630	246	232	
2-1	0.58	0.762	1230	224.630	1.146	316	64	76	0.569	7.0	2.845	250	229	
2-2	0.60	0.775	1235	227.470	1.186	320	66	77	0.579	7.0	2.895	257	233	
2-3	0.84	0.735	1240	230.100	1.067	320	64	75	0.549	6.0	2.745	250	231	
2-4	0.52	0.721	1245	233.150	1.028	320	66	76	0.538	7.0	2.690	250	231	
2-5	0.46	0.678	1250	235.800	0.909	314	67	75	0.506	6.5	2.530	250	232	
			1255	238.335							2.38.335			
3-1	0.74	0.860	1257	238.335	1.462	316	66	75	0.642	7.5	3.210	249	231	
3-2	0.68	0.825	1302	241.600	1.344	320	67	76	0.616	8.0	3.080	250	232	
3-3	0.68	0.825	1307	244.720	1.344	320	66	74	0.616	8.5	3.080	251	233	
3-4	0.65	0.806	1312	247.700	1.285	318	67	73	0.602	8.0	3.010	249	233	
3-5	0.52	0.721	1317	250.700	1.028	315	68	75	0.538	8.0	2.690	250	232	
			1322	253.410							2.53.405			
4-1	0.48	0.693	1324	253.410	0.949	319	68	75	0.518	8.0	2.590	249	231	
4-2	0.50	0.707	1329	255.950	0.988	320	66	75	0.530	8.0	2.650	249	230	
4-3	0.60	0.775	1334	258.650	1.186	320	63	74	0.579	7.5	2.895	249	230	
4-4	0.64	0.800	1339	261.550	1.265	318	65	73	0.597	7.5	2.985	249	229	
4-5	0.60	0.775	1344	264.500	1.186	315	64	72	0.579	7.5	2.895	250	232	
			1349	267.430							2.67.425			



MOSTARDI-PLATT ASSOCIATES, INC.  
TEST SUPPORT DATA

TEST RUN NO. 3

COMPANY: WEPco THIMBLE NO: 097 TARE WT: 3.2432  
 PLANT: Valley FILTER NO: \_\_\_\_\_ TARE WT: \_\_\_\_\_  
 TEST LOCATION: Unit 3 Outlet BAROMETRIC PRESSURE in. Hg: 30.11  
 CLIENT: EPR FLUE PRESSURE in. H<sub>2</sub>O: -18.0  
 OPERATOR: NS FLUE PRESSURE in. Hg ABS: \_\_\_\_\_  
 DATE: 11/30/99 PROBE LENGTH: 13' ft.  
 CONTROL BOX: E51 POT. NO.: E51 PROBE LINER MATERIAL: Teflon  
 METER NO.: E51 NOZZLE IDENTIFICATION NO: #8  
 METER CALIBRATION FACTOR: 1.009 CALIBRATED NOZZLE DIAMETER: 0.245  
 PITOT ID NO.: 318A LEAK CHECK: PRE: 0.0 POST: 0.0 @ 15/15 in. Hg  
 PITOT TUBE COEFFICIENT: 0.837 DUCT SHAPE: Rectangular DIAMETER: \_\_\_\_\_  
 PORT LENGTH: 28 in. DUCT AREA: 120.33 sq. ft. L 9'6" W 12'8"  
 PORT SIZE: 8 DISTURBANCE UPSTREAM: \_\_\_\_\_ DOWNSTREAM: \_\_\_\_\_  
 PORT TYPE: Flange TEST LENGTH: 225 MINUTES PER POINT: 5  
 IMPINGER H<sub>2</sub>O SILICA GEL: TOTAL NUMBER OF TRAVERSE POINTS: 25  
 FINAL: 4734.9 ml/gm FINAL WT: 804.3 gm  
 INITIAL: 4631.0 ml/gm INITIAL WT: 789.8 gm  
 GAIN: 103.9 ml/gm WT. GAIN: 14.5 gm  
 TOTAL H<sub>2</sub>O COLLECTED: 118.4  
 DESCRIPTION OF IMPINGER H<sub>2</sub>O: \_\_\_\_\_  
 SILICA GEL EXHAUSTED?: \_\_\_\_\_  
 IMPINGERS RECOVERED BY: \_\_\_\_\_  
 SILICA GEL WEIGHED BY: \_\_\_\_\_  
 PITOT LEAK CHECK: PRE \_\_\_\_\_ POST \_\_\_\_\_  
 ΔH@ \_\_\_\_\_  
 SAMPLES REMOVED FROM SITE BY: \_\_\_\_\_

For computer data entry: Supervisor, please complete.  
 Do you want to enter a fuel analysis? Y  N   
 What value do you want to use? F = 9,780 F<sub>c</sub> = 1,800 Other = \_\_\_\_\_  
 Circle to indicate "Yes" or add other value if not given.

COMMENTS & NOTES

FIELD TEST DATA SHEET  
FOR ISOKINETIC SAMPLING

MOSTARDI-PLATT ASSOCIATES, INC.

PROJECT WEPCO - Valley

TEST RUN NO. #3

TEST LOCATION Boiler #3 - OUTLET

DATE 30 Nov 99 PAGE 1 OF 2

Port-Point No.	Velocity Head (F) in. H <sub>2</sub> O	√P	Clock Time 24 hr.	Meter Volume (V <sub>m</sub> ) ft <sup>3</sup>	Orifice (H) In. H <sub>2</sub> O	Stack Temp (G) °F	Meter Temp. (t <sub>m</sub> )		Meter Rate cfm	Pump Vacuum in. Hg	Notes	Probe Temp. °F	Filter Holder Temp. °F	Impinger Outlet Temp. °F
							Inlet °F	Outlet °F						
1-1	0.44	0.663	1450	80.8	0.87	318	58	67	0.50	8.0	2.50	254	230	<680
1-2	0.43	0.656	1455	83.50	0.85	318	58	66	0.49	8.0	2.45	251	230	Fully
1-3	0.51	0.714	1500	85.80	1.008	318	56	65	0.54	8.5	2.70	254	230	ICED
1-4	0.54	0.735	1505	88.40	1.067	318	55	64	0.55	9.0	2.75	253	231	
1-5	0.60	0.775	1510	91.20	1.186	317	54	62	0.58	8.5	2.90	252	230	
			1515	94.10							94.10			
2-1	0.48	0.693	1519	94.10	0.948	318	49	55	0.52	9.0	2.6	250	227	
2-2	0.49	0.700	1524	96.70	0.968	318	50	53	0.53	9.0	2.65	250	226	
2-3	0.62	0.787	1529	99.30	1.225	319	49	52	0.59	8.5	2.95	247	228	
2-4	0.62	0.787	1534	102.30	1.225	318	49	49	0.59	9.5	2.95	247	230	
2-5	0.60	0.775	1539	105.25	1.186	321	49	47	0.58	11.0	2.90	247	229	
			1544	108.15							108.15			
3-1	0.72	0.844	1548	108.15	1.423	319	50	46	0.64	9.0	3.2	247	230	
3-2	0.74	0.860	1553	111.35	1.462	318	51	46	0.65	9.0	3.25	250	229	
3-3	0.74	0.860	1558	114.65	1.462	319	48	46	0.65	8.5	3.25	251	230	
3-4	0.70	0.837	1603	112.85	1.383	320	50	46	0.63	8.5	3.15	250	228	
3-5	0.56	0.748	1608	121.00	1.107	314	51	45	0.56	10.0	2.80	250	230	
			1613	123.80							123.80	249		
4-1	0.57	0.755	1617	123.80	1.126	318	51	45	0.59	10.5	2.85	249	226	
4-2	0.60	0.775	1622	126.650	1.186	318	51	45	0.58	10.5	2.90	250	227	
4-3	0.54	0.735	1627	129.580	1.067	318	49	45	0.55	10.5	2.75	245	228	
4-4	0.52	0.721	1632	132.30	1.028	318	52	47	0.54	11.0	2.70	250	227	
4-5	0.49	0.700	1637	135.00	0.968	314	50	45	0.53	9.5	2.65	250	226	
			1642	137.65							137.65			





### PITOT TRAVERSE DATA

Project: WEPCO Valley

Location: Unit 3 Outlet

Date: 11/29/99

Test No: 1 - Prelim

Time: \_\_\_\_\_

Point No.	ΔP	√ΔP	t <sub>s</sub>	α	Point No.	ΔP	√ΔP	t <sub>s</sub>	α
1-1	.55	0.7416	311	5°	5-1	.38	0.6164	310	15°
-2	.52	0.7211	312	10°	-2	.42	0.6481	314	15°
-3	.37	0.6082	312	10°	-3	.49	0.7000	314	15°
-4	.27	0.5196	310	13°	-4	.53	0.7280	314	15°
-5	.28	0.5292	310	8°	-5	.52	0.7211	311	15°
2-1	.61	0.7810	312	5°					
-2	.51	0.7141	313	10°					
-3	.46	0.6782	314	10°					
-4	.48	0.6928	313	8°					
-5	.42	0.6481	313	8°					
3-1	.50	0.7071	312	5°					
-2	.58	0.7616	314	10°					
-3	.57	0.7550	314	10°					
-4	.52	0.7211	314	8°					
-5	.48	0.6928	312	10°					
4-1	.41	0.6403	312	5°					
-2	.52	0.7211	314	10°					
-3	.53	0.7280	314	5°					
-4	.52	0.7211	314	10°					
-5	.54	0.7348	313	8°					

P<sub>bar</sub> \_\_\_\_\_ "Hg Static \_\_\_\_\_ "H<sub>2</sub>O P<sub>a</sub> \_\_\_\_\_ "Hg P<sub>s</sub> \_\_\_\_\_ "Hg Pitot ID 535A C<sub>p</sub> 0.836 Temp. ID E51  
 $0.44 \times 13.0$  %CO<sub>2</sub> = \_\_\_\_\_  $\sqrt{\Delta P}$  \_\_\_\_\_ t<sub>s</sub> \_\_\_\_\_ °F T \_\_\_\_\_ °R Flue Area \_\_\_\_\_ ft<sup>2</sup>  
 $0.32 \times 6.0$  %O<sub>2</sub> = + \_\_\_\_\_ Duct Dimensions \_\_\_\_\_  
 $0.28 \times 81.0$  %N<sub>2</sub> = + \_\_\_\_\_ B<sub>ws</sub> 0.10 1 - B<sub>ws</sub> 0.90 Disturbance: Upstream \_\_\_\_\_  
 ( \_\_\_\_\_ Md x \_\_\_\_\_ 1-B<sub>ws</sub>) + (18 x \_\_\_\_\_ B<sub>ws</sub>) = \_\_\_\_\_ (Ms) Downstream \_\_\_\_\_  
 $v_s = 85.49 \times C_p \times \sqrt{\frac{(_____ ) T_s \text{ °R}}{Ms \times P_s}} \times \sqrt{\Delta P} = _____$  ft/sec (Vs)  
 Q<sub>acfm</sub> = \_\_\_\_\_ Vs x \_\_\_\_\_ Flue Area x 60 = \_\_\_\_\_ acfm Port Length \_\_\_\_\_ Inches  
 Q<sub>dscfm</sub> = 17.647 x ACFM x  $\frac{P_s}{T_s \text{ °R}}$  = \_\_\_\_\_ SCFM  
 Q<sub>dscfm</sub> = 17.647 x ACFM x  $\frac{P_s}{T_s \text{ °R}} \times (1-B_{ws}) = _____$  DSCFM  
 Pre-test leak check  "H<sub>2</sub>O  
 Post-test leak check  "H<sub>2</sub>O

55

Data Taken By: \_\_\_\_\_  
 Field Engineer / Test Technician

## CALIBRATION PROCEDURES

### PITOT TUBES

The pitot tubes used during this test program are fabricated according to the specification described and illustrated in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A, Methods 1 through 5 as published in the *Federal Register*, Volume 42, No. 160; hereafter referred to by the appropriate method number. The pitot tubes comply with the alignment specifications in Method 2, Section 4; and the pitot tube assemblies are in compliance with specifications in the same section.

Pitot tube assemblies are calibrated in accordance with Method 2, Section 4, against a standard hemispherical pitot utilizing a wind tunnel meeting the specification in Method 2, Section 4.1.2.

### NOZZLES

The nozzles are measured according to Method 5, Section 5.1.

### TEMPERATURE SENSING DEVICES

The potentiometer and thermocouples are calibrated against a mercury thermometer in a calibration well. Alternatively, readings are checked utilizing a NBS traceable millivolt source.

### DRY GAS METERS

The test meters are calibrated according to Method 5, Section 5.3 and "Procedures for Calibrating and Using Dry Gas Volume Meters as Calibration Standards" by P.R. Westlin and R.T. Shigehara, March 10, 1978.

### ANALYTICAL BALANCE

The accuracy of the analytical balance is checked with Class S, Stainless Steel Type 303 weights manufactured by F. Hopken and Son, Jersey City, New Jersey.

### Pitot Tube Calibration Data

Calibration Pitot Tube: Type: HEMI STD Size (OD): 1/4" Pitot ID #: 16018

Type "S" Pitot Tube ID Number 427 (1/4") Cp(std) = 0.99

Calibration Date: 12/4/1997 Performed By: M. McIntyre

P <sub>std</sub> , (in.) H <sub>2</sub> O		A-Side Calibration		
Set Value	Read Value	P <sub>s</sub> , (in.) H <sub>2</sub> O	C <sub>p(S)</sub> <sup>a</sup>	DEV. <sup>b</sup>
0.25	0.27	0.39	0.829	0.001
0.55	0.55	0.78	0.830	0.000
0.85	0.85	1.20	0.831	0.001
1.00	1.05	1.50	0.828	0.002
2.00	2.00	2.85	0.829	0.001
3.00	3.00	4.25	0.832	0.002
<b>Average</b>			0.830	0.001

P <sub>std</sub> , (in.) H <sub>2</sub> O		B-Side Calibration		
Set Value	Read Value	P <sub>s</sub> , (in.) H <sub>2</sub> O	C <sub>p(S)</sub> <sup>a</sup>	DEV. <sup>b</sup>
0.25	0.26	0.37	0.830	0.001
0.55	0.55	0.78	0.830	0.001
0.85	0.85	1.20	0.831	0.001
1.00	1.05	1.50	0.828	0.003
2.00	2.00	2.80	0.837	0.005
3.00	3.00	4.25	0.832	0.000
<b>Average</b>			0.831	0.002

$$\overline{C_p}(A) - \overline{C_p}(B) = 0.001 \quad (\text{must be } \leq 0.01)$$

$${}^a C_{p(S)} = C_{p(std)} \sqrt{\frac{\Delta P_{std}}{\Delta P_s}}$$

$${}^b \text{DEV} = C_{p(S)} - \overline{C_p}, \quad (\text{must be } \leq 0.01)$$

### Pitot Tube Calibration Data

Calibration Pitot Tube: Type: Hemi Std. Size (OD): 0.25 Pitot ID #: 160-18

Type "S" Pitot Tube ID Number 318 Cp(std) = 0.99

Calibration Date: 9/8/95 Performed By: BR/BDL

P <sub>std</sub> , (in.) H <sub>2</sub> O		A-Side Calibration		
Set Value	Read Value	P <sub>s</sub> , (in.) H <sub>2</sub> O	C <sub>p(S)</sub> <sup>a</sup>	DEV. <sup>b</sup>
0.25	0.24	0.34	0.832	0.006
0.55	0.55	0.76	0.842	0.005
0.85	0.84	1.20	0.828	0.009
1.00	0.99	1.40	0.833	0.005
2.00	1.90	2.60	0.846	0.009
3.00	2.90	4.00	0.843	0.006
<b>Average</b>			0.837	0.006

P <sub>std</sub> , (in.) H <sub>2</sub> O		B-Side Calibration		
Set Value	Read Value	P <sub>s</sub> , (in.) H <sub>2</sub> O	C <sub>p(S)</sub> <sup>a</sup>	DEV. <sup>b</sup>
0.25	0.24	0.34	0.832	0.005
0.55	0.55	0.77	0.837	0.000
0.85	0.84	1.20	0.828	0.008
1.00	0.99	1.40	0.833	0.004
2.00	1.90	2.60	0.846	0.010
3.00	2.90	4.00	0.843	0.007
<b>Average</b>			0.836	0.006

$$\bar{C}_p(A) - \bar{C}_p(B) = 0.001 \quad (\text{must be } \leq 0.01)$$

$${}^a C_{p(S)} = C_{p(std)} \sqrt{\frac{\Delta P_{std}}{\Delta P_s}}$$

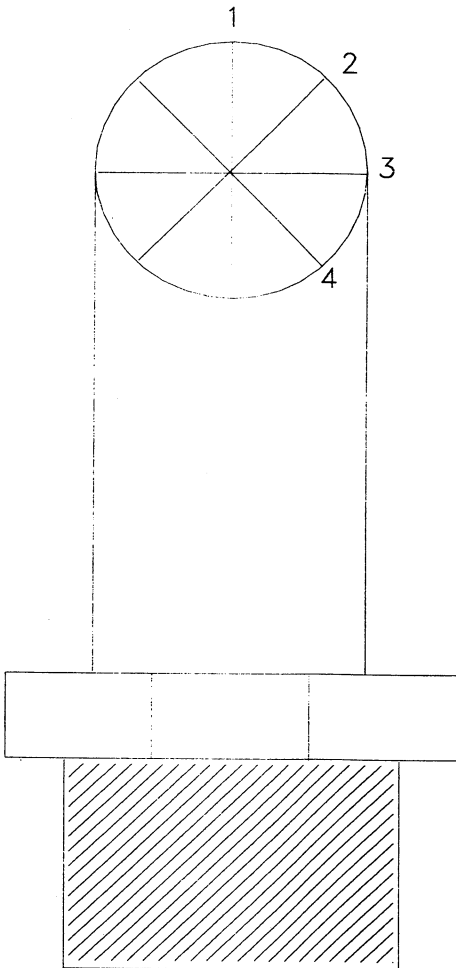
$${}^b \text{DEV} = C_{p(S)} - \bar{C}_p, \quad (\text{must be } \leq 0.01)$$

# Nozzle Calibration

Date: 11/29/00

Nozzle ID No.: Set No.8

Analyst: DSM



**Pre Test**                      **Post Test**

<u>0.240</u>	1	✓
<u>0.239</u>	2	✓
<u>0.240</u>	3	✓
<u>0.239</u>	4	✓

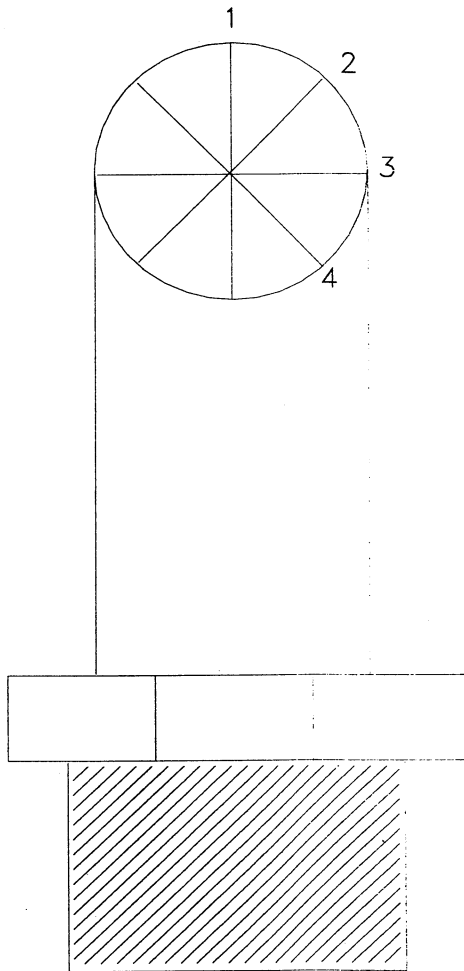
Average
<u>0.240</u>

# Nozzle Calibration

Date: 11/29/00

Nozzle ID No.: Set No.8

Analyst: DSM



**Pre Test**                      **Post Test**

0.246    1                      ✓

0.245    2                      ✓

0.244    3                      ✓

0.244    4                      ✓

<b>Average</b>
<u>0.245</u>

**STACK TEMPERATURE SENSOR CALIBRATION DATA FORM  
(FOR K-TYPE THERMOCOUPLES)**

EPA Control Module Number: E12

Name: Rich Russ

Ambient Temperature: 63 °F

Date: 11-12-99

Model 1061; S/N: A20821

Reference Source (T/C Calibrator): Transmation, Inc.

Date of Calibration Verification: 10/18/94

Primary Standards Directly Traceable to  
National Institute of Standards and Technology (NIST)

Reference <sup>a</sup> Source Temperature, (°F)	Test Thermometer Temperature, (°F)	Temperature Difference, <sup>b</sup> %
50	49	0.196
100	99	0.179
150	149	0.164
200	199	0.152
250	249	0.141
300	300	0.000
350	350	0.000
400	400	0.000
450	450	0.000
500	500	0.000
550	550	0.000
600	600	0.000
650	650	0.000
700	700	0.000
800	800	0.000
900	900	0.000
1000	1000	0.000
1100	1100	0.000
1200	1200	0.000

<sup>a</sup>Every (50°F) for each reference point.

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460



**STACK TEMPERATURE SENSOR CALIBRATION DATA FORM  
(FOR K-TYPE THERMOCOUPLES)**

EPA Control Module Number: E12

Name: Rich Russ

Ambient Temperature 68 °F

Date: 12-09-99

Model 1061; S/N: A20821

Reference Source (T/C Calibrator): Transmation, Inc.

Date of Calibration Verification: 10/18/94

Primary Standards Directly Traceable to  
National Institute of Standards and Technology (NIST)

Reference <sup>a</sup> Source Temperature, (°F)	Test Thermometer Temperature, (°F)	Temperature Difference, <sup>b</sup> %
50	50	0.000
100	100	0.000
150	150	0.000
200	200	0.000
250	250	0.000
300	300	0.000
350	350	0.000
400	400	0.000
450	450	0.000
500	500	0.000
550	550	0.000
600	600	0.000
650	650	0.000
700	700	0.000
800	800	0.000
900	900	0.000
1000	1000	0.000
1100	1101	0.064
1200	1201	0.060

<sup>a</sup>Every (50°F) for each reference point.

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

**STACK TEMPERATURE SENSOR CALIBRATION DATA FORM  
(FOR K-TYPE THERMOCOUPLES)**

EPA Control Module Number: E51

Name: Rich Russ

Ambient Temperature 67 °F

Date: 11-03-99

Model 1061; S/N: A20821

Reference Source (T/C Calibrator): Transmation, Inc.

Date of Calibration Verification: 10/18/94

Primary Standards Directly Traceable to  
National Institute of Standards and Technology (NIST)

Reference <sup>a</sup> Source Temperature, (°F)	Test Thermometer Temperature, (°F)	Temperature Difference, <sup>b</sup> %
50	51	0.196
100	101	0.179
150	151	0.164
200	201	0.152
250	251	0.141
300	300	0.000
350	350	0.000
400	400	0.000
450	450	0.000
500	500	0.000
550	550	0.000
600	600	0.000
650	650	0.000
700	700	0.000
800	800	0.000
900	900	0.000
1000	1000	0.000
1100	1100	0.000
1200	1200	0.000

<sup>a</sup>Every (50°F) for each reference point.

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

**STACK TEMPERATURE SENSOR CALIBRATION DATA FORM  
(FOR K-TYPE THERMOCOUPLES)**

EPA Control Module Number: E51

Name: Rich Russ

Ambient Temperature 67 °F

Date: 12-08-99

Model 1061; S/N: A20821

Reference Source (T/C Calibrator): Transmation, Inc.

Date of Calibration Verification: 10/18/94

Primary Standards Directly Traceable to  
National Institute of Standards and Technology (NIST)

Reference <sup>a</sup> Source Temperature, (°F)	Test Thermometer Temperature, (°F)	Temperature Difference, <sup>b</sup> %
50	51	0.196
100	101	0.179
150	151	0.164
200	201	0.152
250	251	0.141
300	301	0.132
350	351	0.123
400	401	0.116
450	451	0.110
500	501	0.104
550	551	0.099
600	601	0.094
650	650	0.000
700	700	0.000
800	800	0.000
900	900	0.000
1000	1000	0.000
1100	1100	0.000
1200	1200	0.000

<sup>a</sup>Every (50°F) for each reference point.

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

METER BOX CALIBRATION

Dry Gas Meter No. E12  
 Standard Meter No. 3623851  
 Standard Meter (Yr) 1.0063

Date: 11-12-99  
 Calibrated By: Rich Russ  
 Barometric Pressure: 29.64

Formula Protection Password: MPA

Run Number	Orifice Setting in H2O Chg (H)	Standard Meter Gas Volume Vr	Dry Meter Gas Volume Vd	Standard Meter Temp. F tr	Dry Gas Meter Inlet Temp. F tdi	Dry Gas Meter Outlet Temp. F tdo	Dry Gas Meter Avg. Temp. F td	Time Min.	Time Sec.	Y	Chg (H@)
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Final		37.364	27.363	66	66	64					
Initial		32.330	22.311	66	68	65					
Difference	1	5.034	5.052	66	67	64.5	65.75	18	35	0.995	1.533
Final		42.574	32.608	66	67	64					
Initial		37.513	27.508	66	66	64					
Difference	2	5.061	5.100	66	66.5	64	65.25	12	12	0.990	1.636
Final		26.366	16.331	66	70	65					
Initial		21.317	11.249	66	68	64					
Difference	3	5.049	5.082	66	69	64.5	66.75	10	21	0.993	1.651
Final		48.141	38.198	67	71	65					
Initial		42.813	32.850	66	67	64					
Difference	4	5.328	5.348	66.5	84	64.5	74.25	9	32	1.009	1.598
Final		53.436	43.510	68	74	66					
Initial		48.323	38.378	67	70	65					
Difference	5	5.113	5.132	67.5	72	65.5	68.75	8	3	0.996	1.673
Final		31.899	21.853	66	72	65					
Initial		26.766	16.721	66	69	65					
Difference	6	5.133	5.132	66	70.5	65	67.75	6	17	0.999	1.679

Average 0.997 1.628

METER BOX CALIBRATION

Dry Gas Meter No. E12 Date: 12-09-99  
 Standard Meter No. 677191 Calibrated By: Rich Russ  
 Standard Meter (Yr) 0.9991 Barometric Pressure: 30.04

Formula Protection Password: MPA

Run Number	Orifice Setting in H2O Chg (H)	Standard Meter Gas Volume Vr	Dry Meter Gas Volume Vd	Standard Meter Temp. F tr	Dry Gas Meter Inlet Temp. F tdi	Dry Gas Meter Outlet Temp. F tdo	Dry Gas Meter Avg. Temp. F td	Time Min.	Time Sec.	Y	Chg (H@)
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Final		55.361	70.756	68	71	70					
Initial		50.319	65.714	68	72	71					
Difference	1	0.20	5.042	68	71.5	70.5	71	18	50	1.005	1.545
Final		60.549	75.956	69	73	70					
Initial		55.535	70.935	68	71	70					
Difference	2	0.50	5.014	68.5	72	70	71	12	2	1.002	1.598
Final		50.172	65.559	68	73	71					
Initial		45.160	60.505	68	72	71					
Difference	3	0.70	5.012	68	72.5	71	71.75	10	18	0.997	1.635
Final		65.851	81.242	69	75	71					
Initial		60.835	76.229	69	73	70					
Difference	4	0.90	5.016	69	84	70.5	77.25	8	59	1.014	1.586
Final		71.165	86.550	70	76	71					
Initial		66.126	81.512	69	74	70					
Difference	5	1.20	5.039	69.5	75	70.5	72.75	7	52	1.003	1.623
Final		100.217	15.607	68	76	70					
Initial		95.187	10.579	68	77	70					
Difference	6	2.00	5.030	68	76.5	70	73.25	6	11	1.005	1.666

Average 1.005 1.609

## VOLUME METERING SYSTEM FIELD AUDIT

Date: 11-12-99

Name: Rich Russ

EPA Control Module No.: E12

Ambient Temperature: 68 °F

Calibration (Y): 0.997

Barometric Pressure: 29.64 "Hg

Delta H: 1.628

#VALUE!

Run No.	Time	Gas Meter Reading/Gas Meter Temperature			Yc (Calculated)
	(Minutes)	(Cubic Feet)	Inlet (°F)	Outlet (°F)	
1	0	48.680	75	67	0.999
	10	56.257	78	69	
	Vm=	7.577	Avg.= 72.25	532.25	
2	0	56.257	78	69	1.002
	10	63.824	79	70	
	Vm=	7.567	Avg.= 74.00	534.00	
3	0	63.824	79	70	1.006
	10	71.365	80	71	
	Vm=	7.541	Avg.= 75.00	535.00	

$$Y_c = \frac{10}{V_m} \sqrt{\frac{P_{bar}}{0.0319 T_m}}$$

Limit: 0.97Y <Yc< 1.03Y

Limit: 0.967 <Yc< 1.027

$$\text{Calc. Delta H @} = \frac{0.0319 (\text{Delta H})(T_m)(100)}{P_{bar}(Y^2)(V_m^2)} \quad (\text{From Calibration Data}) = 1.909$$

METER BOX CALIBRATION

Dry Gas Meter No. E51  
 Standard Meter No. 3623851  
 Standard Meter (Yr) 1.0063

Date: 11-03-99  
 Calibrated By: Rich Russ  
 Barometric Pressure: 29.38

Formula Protection Password: MPA

Run Number	Orifice Setting in H2O Chg (H)	Standard Meter Gas Volume Vr	Dry Meter Gas Volume Vd	Standard Meter Temp. F tr	Dry Gas Meter Inlet Temp. F tdi	Dry Gas Meter Outlet Temp. F tdo	Dry Gas Meter Avg. Temp. F td	Time Min.	Time Sec.	Chg (H@)
1	0.20	79.160	85.107	67	72	70				
		74.125	80.070	67	70	69				
		5.035	5.037	67	71	69.5	70.25	19	31	1.005
		91.537	97.454	67	77	70				
		85.621	91.519	67	76	70				
2	0.50	5.916	5.935	67	76.5	70	73.25	14	52	1.007
		73.972	79.915	66	73	69				
		68.946	74.879	66	70	69				
		5.026	5.036	66	71.5	69	70.25	10	50	1.004
		98.281	104.170	67	74	69				
		92.351	98.271	67	72	69				
		5.930	5.899	67	73	69	71	11	22	1.011
		104.915	10.738	67	75	69				
		98.435	4.338	67	72	69				
		6.480	6.400	67	73.5	69	71.25	10	42	1.018
		85.266	91.184	67	79	70				
		79.545	85.488	67	72	70				
		5.721	5.696	67	75.5	70	72.75	7	23	1.010

Run Number	Orifice Setting in H2O Chg (H)	Standard Meter Gas Volume Vr	Dry Meter Gas Volume Vd	Standard Meter Temp. F tr	Dry Gas Meter Inlet Temp. F tdi	Dry Gas Meter Outlet Temp. F tdo	Dry Gas Meter Avg. Temp. F td	Time Min.	Time Sec.	Chg (H@)
3	0.70	79.160	85.107	67	72	70				
		74.125	80.070	67	70	69				
		5.035	5.037	67	71	69.5	70.25	19	31	1.005
		91.537	97.454	67	77	70				
		85.621	91.519	67	76	70				
		5.916	5.935	67	76.5	70	73.25	14	52	1.007
		73.972	79.915	66	73	69				
		68.946	74.879	66	70	69				
		5.026	5.036	66	71.5	69	70.25	10	50	1.004
		98.281	104.170	67	74	69				
		92.351	98.271	67	72	69				
		5.930	5.899	67	73	69	71	11	22	1.011
		104.915	10.738	67	75	69				
		98.435	4.338	67	72	69				
		6.480	6.400	67	73.5	69	71.25	10	42	1.018
		85.266	91.184	67	79	70				
		79.545	85.488	67	72	70				
		5.721	5.696	67	75.5	70	72.75	7	23	1.010

Average 1.009 1.814

METER BOX CALIBRATION

Dry Gas Meter No. E51 Date: 12-08-99  
 Standard Meter No. 3623851 Calibrated By: Rich Russ  
 Standard Meter (Yr) 1.0063 Barometric Pressure: 29.53

Formula Protection Password: MPA

Run Number	Orifice Setting in H2O Chg (H)	Standard Meter Gas Volume Vr	Dry Meter Gas Volume Vd	Standard Meter Temp. F tr	Dry Gas Meter Inlet Temp. F tdi	Dry Gas Meter Outlet Temp. F tdo	Dry Gas Meter Avg. Temp. F td	Time Min.	Time Sec.	Chg (H@)
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Final		65.880	34.702	65	73	70				
Initial		60.875	29.615	65	74	70				
Difference	1	5.005	5.087	65	73.5	70	71.75	19	33	0.996
Final		71.201	40.097	65	75	70				
Initial		66.035	34.850	65	72	70				
Difference	2	5.166	5.247	65	73.5	70	71.75	13	7	0.996
Final		60.742	29.484	65	76	70				
Initial		55.724	24.446	64	74	69				
Difference	3	5.018	5.038	64.5	75	69.5	72.25	10	54	1.009
Final		76.537	45.474	65	78	70				
Initial		71.519	40.405	65	75	70				
Difference	4	5.018	5.069	65	76.5	70	73.25	9	44	1.003
Final		81.757	50.730	65	79	71				
Initial		76.744	45.692	65	77	70				
Difference	5	5.013	5.038	65	78	70.5	74.25	8	18	1.010
Final		87.073	56.096	65	82	71				
Initial		82.020	51.002	65	77	70				
Difference	6	5.053	5.094	65	79.5	70.5	75	6	37	1.006
Average										1.819



## VOLUME METERING SYSTEM FIELD AUDIT

Date: 11-03-99

Name: Rich Russ

EPA Control Module No.: E51

Ambient Temperature: 69 °F

Calibration (Y): 1.009

Barometric Pressure: 29.38 "Hg

Delta H: 1.814

Run No.	Time	Gas Meter Reading/Gas Meter Temperature			Yc (Calculated)
	(Minutes)	(Cubic Feet)	Inlet (°F)	Outlet (°F)	
1	0	16.740	72	68	1.019
	10	24.189	75	68	
	Vm=	7.449	Avg.= 70.75	530.75	
2	0	24.189	74	68	1.026
	10	31.596	77	68	
	Vm=	7.407	Avg.= 71.75	531.75	
3	0	31.596	76	68	1.018
	10	39.061	77	68	
	Vm=	7.465	Avg.= 72.25	532.25	

$$Y_c = \frac{10}{V_m} \sqrt{\frac{P_{bar}}{0.0319 T_m}}$$

Limit: 0.97Y <Yc< 1.03Y

Limit: 0.979 <Yc< 1.039

$$\text{Calc. Delta H @} = \frac{0.0319 (\text{Delta H})(T_m)(100)}{P_{bar}(Y^2)(V_m^2)} \quad (\text{From Calibration Data}) = 1.945$$



## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	1	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Inlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	D. Helm				
CONTROL BOX:	E-12				
METER NO.:	E-12				
METER CALIBRATION FACTOR:	0.997				
PITOT ID NO.:	427A				
PITOT TUBE COEFFICIENT:	0.830				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)		30.11		in. Hg.	
STATIC PRESSURE		-13.5		in. H2O	
FLUE PRESSURE (Ps)		29.12		in. Hg. abs.	
PROBE LENGTH:		10		ft.	
PROBE LINER MATERIAL:		Teflon			
NOZZLE IDENTIFICATION NO.:		#8			
CALIBRATED NOZZLE DIAMETER:		0.240 in.			
LEAK CHECK		PRE:		0.008	
		POST:		0.005 @ 11 in. Hg.	
DUCT SHAPE:		Circular		DIA. Feet	
		Rectangular		12.6666 Feet	
DUCT AREA:		120.3327 sq. ft.			
TEST LENGTH:		125		min.	
MINUTES PER POINT:		5			
TOTAL NUMBER OF TRAVERSE POINTS:		25			



## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 1

**Location:** Boiler #3 Baghouse Inlet

SILICA GEL FINAL WT.: 723.80 grams  
 SILICA GEL INITIAL WT.: 712.40 grams  
 DIFFERENCE: 11.40

FINAL IMPINGER WATER: 4698.90 mls.  
 INITIAL IMPINGER WATER: 4597.00 mls.  
 DIFFERENCE: 101.90

TOTAL WATER GAIN: 113.30

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.060		0.000000060
PROBE WASH:	0.002		0.000000002
	<b>Particle-bound Total:</b>		0.000000062
KCl:	2.096		0.000002096
	<b>Oxidized Total:</b>		0.000002096
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	1.330		0.000001330
KMNO <sub>4</sub> :	0.439		0.000000439
	<b>Elemental Total:</b>		0.000001769

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.40			11.40
Oxygen:	6.60			6.60

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:** Wisconsin Electric Power Company

**Date:** 11/30/99

**Test Run:** 1

**Stack or Duct No.:** Boiler #3 Baghouse Inlet

**Start Time:** 9:01

**Stop Time:** 11:13

<b>Pb:</b>	30.11	Inches Hg
<b>Static</b>	-13.50	Inches H2O
<b>Ps:</b>	29.12	Inches Hg Abs.
<b>Vlc:</b>	113	ml + grams
<b>Mn:</b>	0.0000	gm
<b>Test Time:</b>	125	minutes
<b>% O2:</b>	6.60	%
<b>% CO2:</b>	11.40	%
<b>% N2:</b>	82.00	%
<b>Delta H:</b>	0.76	Inches H2O
<b>Cp:</b>	0.830	Dimensionless - pitot
<b>Tm:</b>	45.60	°F
<b>Sqrt P:</b>	0.657	Inches H2O
<b>Ts:</b>	314.56	°F
<b>Vm:</b>	61.546	Cubic Feet
<b>Dn:</b>	0.240	Inches - nozzle
<b>As:</b>	120.33	Sq. Feet
<b>Yd:</b>	0.997	Mcf
<b>CF:</b>	N/A	Process tons/hr
<b>Heat Input:</b>	N/A	MM BTU/hr
<b>Fd:</b>	N/A	dscf/10 <sup>6</sup> Btu
<b>Fc:</b>	N/A	scf/10 <sup>6</sup> Btu

<b>Vmstd:</b>	64.606	cubic feet (dry)
<b>Vwstd:</b>	5.336	cubic feet (wet)
<b>Bwo:</b>	0.076	
<b>Md:</b>	30.088	lb/lb-mole (dry)
<b>Ms:</b>	29.166	lb/lb-mole (wet)
<b>Excess Air (%)</b>	43.860	
<b>Vs:</b>	44.513	fps
<b>ACFM:</b>	321379.	
<b>DSCFM:</b>	196932.	
<b>WSCFM:</b>	213199	
<b>%I:</b>	100.6	isokinetic variance
<b>GR/ACF:</b>	---	
<b>GR/DSCF:</b>	---	
<b>lbs/hr</b>	---	
<b>lbs/ton prod.:</b>	N/A	
<b>lbs/MM BTU:</b>	N/A	Heat Input
<b>lbs/MM BTU:</b>	N/A	O2 Basis
<b>lbs/MM BTU:</b>	N/A	CO2 Basis

## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	2	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Inlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	D. Helm				
CONTROL BOX:	E-12				
METER NO.:	E-12				
METER CALIBRATION FACTOR:	0.997				
PITOT ID NO.:	427A				
PITOT TUBE COEFFICIENT:	0.830				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)			30.11 in. Hg.		
STATIC PRESSURE			-13.5 in. H2O		
FLUE PRESSURE (Ps)			29.12 in. Hg. abs.		
PROBE LENGTH:			10 ft.		
PROBE LINER MATERIAL:			Teflon		
NOZZLE IDENTIFICATION NO.:			8		
CALIBRATED NOZZLE DIAMETER:			0.240 in.		
LEAK CHECK			PRE: 0.007 POST: 0.005 @ 11 in. Hg.		
DUCT SHAPE:			Circular		
DUCT AREA:			120.3327 sq. ft.		
DUCT SHAPE:			Circular		
DUCT DIA.:			12.6666 Feet		
DUCT AREA:			120.3327 sq. ft.		
TEST LENGTH:			125 min.		
MINUTES PER POINT:			5		
TOTAL NUMBER OF TRAVERSE POINTS:			25		





## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 2

**Location:** Boiler #3 Baghouse Inlet

**SILICA GEL FINAL WT.:** 751.70 grams  
**SILICA GEL INITIAL WT.:** 738.50 grams  
**DIFFERENCE:** 13.20

**FINAL IMPINGER WATER:** 4723.30 mls.  
**INITIAL IMPINGER WATER:** 4626.20 mls.  
**DIFFERENCE:** 97.10

**TOTAL WATER GAIN:** 110.30

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.057		0.000000057
PROBE WASH:	0.025		0.000000025
		<b>Particle-bound Total:</b>	0.000000082
KCl:	2.216		0.000002216
		<b>Oxidized Total:</b>	0.000002216
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	0.362		0.000000362
KMNO <sub>4</sub> :	0.306		0.000000306
		<b>Elemental Total:</b>	0.000000668

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.40			11.40
Oxygen:	6.60			6.60

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:** Wisconsin Electric Power Company

**Date:** 11/30/99

**Test Run:** 2

**Stack or Duct No.:** Boiler #3 Baghouse Inlet

**Start Time:** 12:00

**Stop Time:** 14:13

<b>Pb:</b>	30.11	Inches Hg
<b>Static</b>	-13.50	Inches H2O
<b>Ps:</b>	29.12	Inches Hg Abs.
<b>Vlc:</b>	110	ml + grams
<b>Mn:</b>	0.0000	gm
<b>Test Time:</b>	125	minutes
<b>% O2:</b>	6.60	%
<b>% CO2:</b>	11.40	%
<b>% N2:</b>	82.00	%
<b>Delta H:</b>	0.80	Inches H2O
<b>Cp:</b>	0.830	Dimensionless - pitot
<b>Tm:</b>	56.26	°F
<b>Sqrt P:</b>	0.664	Inches H2O
<b>Ts:</b>	313.84	°F
<b>Vm:</b>	63.719	Cubic Feet
<b>Dn:</b>	0.240	Inches - nozzle
<b>As:</b>	120.33	Sq. Feet
<b>Yd:</b>	0.997	Mcf
<b>CF:</b>	N/A	Process tons/hr
<b>Heat Input:</b>	N/A	MM BTU/hr
<b>Fd:</b>	N/A	dscf/10 <sup>6</sup> Btu
<b>Fc:</b>	N/A	scf/10 <sup>6</sup> Btu

<b>Vmstd:</b>	65.513	cubic feet (dry)
<b>Vwstd:</b>	5.195	cubic feet (wet)
<b>Bwo:</b>	0.073	
<b>Md:</b>	30.088	lb/lb-mole (dry)
<b>Ms:</b>	29.200	lb/lb-mole (wet)
<b>Excess Air (%)</b>	43.860	
<b>Vs:</b>	44.933	fps
<b>ACFM:</b>	324413.	
<b>DSCFM:</b>	199585.	
<b>WSCFM:</b>	215412	
<b>%I:</b>	100.6	isokinetic variance
<b>GR/ACF:</b>	---	
<b>GR/DSCF:</b>	---	
<b>lbs/hr</b>	---	
<b>lbs/ton prod.:</b>	N/A	
<b>lbs/MM BTU:</b>	N/A	Heat Input
<b>lbs/MM BTU:</b>	N/A	O2 Basis
<b>lbs/MM BTU:</b>	N/A	CO2 Basis

## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	3	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Inlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	D. Helm				
CONTROL BOX:	E-12				
METER NO.:	E-12				
METER CALIBRATION FACTOR:	0.997				
PITOT ID NO.:	427A				
PITOT TUBE COEFFICIENT:	0.830				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)		30.11 in. Hg.			
STATIC PRESSURE		-13.5 in. H2O			
FLUE PRESSURE (Ps)		29.12 in. Hg. abs.			
PROBE LENGTH:		10 ft.			
PROBE LINER MATERIAL:		Teflon			
NOZZLE IDENTIFICATION NO.:		8			
CALIBRATED NOZZLE DIAMETER:		0.240 in.			
LEAK CHECK		PRE: 0.007		POST: 0.005 @ 11 in. Hg.	
DUCT SHAPE:		Circular		DIA. 9.5 Feet	
DUCT AREA:		Rectangular		12.6666 Feet 120.3327 sq. ft.	
TEST LENGTH:		125 min.			
MINUTES PER POINT:		5			
TOTAL NUMBER OF TRAVERSE POINTS:		25			



## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 3

**Location:** Boiler #3 Baghouse Inlet

SILICA GEL FINAL WT.: 634.60 grams  
 SILICA GEL INITIAL WT.: 623.20 grams  
 DIFFERENCE: 11.40

FINAL IMPINGER WATER: 4731.00 mls.  
 INITIAL IMPINGER WATER: 4630.50 mls.  
 DIFFERENCE: 100.50

TOTAL WATER GAIN: 111.90

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.046		0.000000046
PROBE WASH:	0.014		0.000000014
	<b>Particle-bound Total:</b>		0.000000060
KCl:	1.806		0.000001806
	<b>Oxidized Total:</b>		0.000001806
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	0.570		0.000000570
KMNO <sub>4</sub> :	0.413		0.000000413
	<b>Elemental Total:</b>		0.000000983

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.50			11.50
Oxygen:	6.50			6.50

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:** Wisconsin Electric Power Company

**Date:** 11/30/99

**Test Run:** 3

**Stack or Duct No.:** Boiler #3 Baghouse Inlet

**Start Time:** 14:50

**Stop Time:** 17:02

<b>Pb:</b>	30.11	Inches Hg
<b>Static</b>	-13.50	Inches H2O
<b>Ps:</b>	29.12	Inches Hg Abs.
<b>Vlc:</b>	112	ml + grams
<b>Mn:</b>	0.0000	gm
<b>Test Time:</b>	125	minutes
<b>% O2:</b>	6.50	%
<b>% CO2:</b>	11.50	%
<b>% N2:</b>	82.00	%
<b>Delta H:</b>	0.76	Inches H2O
<b>Cp:</b>	0.830	Dimensionless - pitot
<b>Tm:</b>	50.80	°F
<b>Sqrt P:</b>	0.650	Inches H2O
<b>Ts:</b>	313.64	°F
<b>Vm:</b>	62.385	Cubic Feet
<b>Dn:</b>	0.240	Inches - nozzle
<b>As:</b>	120.33	Sq. Feet
<b>Yd:</b>	0.997	Mcf
<b>CF:</b>	N/A	Process tons/hr
<b>Heat Input:</b>	N/A	MM BTU/hr
<b>Fd:</b>	N/A	dscf/10 <sup>6</sup> Btu
<b>Fc:</b>	N/A	scf/10 <sup>6</sup> Btu

<b>Vmstd:</b>	64.821	cubic feet (dry)
<b>Vwstd:</b>	5.270	cubic feet (wet)
<b>Bwo:</b>	0.075	
<b>Md:</b>	30.100	lb/lb-mole (dry)
<b>Ms:</b>	29.190	lb/lb-mole (wet)
<b>Excess Air (%)</b>	42.910	
<b>Vs:</b>	44.027	fps
<b>ACFM:</b>	317870.	
<b>DSCFM:</b>	195247.	
<b>WSCFM:</b>	211122	
<b>%I:</b>	101.8	isokinetic variance
<b>GR/ACF:</b>	---	
<b>GR/DSCF:</b>	---	
<b>lbs/hr</b>	---	
<b>lbs/ton prod.:</b>	N/A	
<b>lbs/MM BTU:</b>	N/A	Heat Input
<b>lbs/MM BTU:</b>	N/A	O2 Basis
<b>lbs/MM BTU:</b>	N/A	CO2 Basis

## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	1	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Outlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	N. Smith				
CONTROL BOX:	E-51				
METER NO.:	E-51				
METER CALIBRATION FACTOR:	1.009				
PITOT ID NO.:	318A				
PITOT TUBE COEFFICIENT:	0.837				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)		30.11		in. Hg.	
STATIC PRESSURE		-18		in. H2O	
FLUE PRESSURE (Ps)		28.79		in. Hg. abs.	
PROBE LENGTH:		13		ft.	
PROBE LINER MATERIAL:		Teflon			
NOZZLE IDENTIFICATION NO.:		#8			
CALIBRATED NOZZLE DIAMETER:		0.245		in.	
LEAK CHECK		PRE: 0.000		POST: 0.000 @ 16 in. Hg.	
DUCT SHAPE:		Circular		DIA. 9.5 Feet	
DUCT AREA:		Rectangular		12.6666 Feet 120.3327 sq. ft.	
TEST LENGTH:		125		min.	
MINUTES PER POINT:		5			
TOTAL NUMBER OF TRAVERSE POINTS:		25			





## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 1

**Location:** Boiler #3 Baghouse Outlet

SILICA GEL FINAL WT.: 808.40 grams  
 SILICA GEL INITIAL WT.: 793.90 grams  
 DIFFERENCE: 14.50

FINAL IMPINGER WATER: 4677.10 mls.  
 INITIAL IMPINGER WATER: 4581.50 mls.  
 DIFFERENCE: 95.60

TOTAL WATER GAIN: 110.10

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.183		0.000000183
PROBE WASH:	0.000		0.000000000
			<b>Particle-bound Total:</b>
			0.000000183
KCl:	3.086		0.000003086
			<b>Oxidized Total:</b>
			0.000003086
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	0.339		0.000000339
KMNO <sub>4</sub> :	0.280		0.000000280
			<b>Elemental Total:</b>
			0.000000619

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.20			11.20
Oxygen:	6.80			6.80

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:** Wisconsin Electric Power Company  
**Date:** 11/30/99  
**Test Run:** 1  
**Stack or Duct No.:** Boiler #3 Baghouse Outlet  
**Start Time:** 9:00  
**Stop Time:** 11:25

Pb:	30.11	Inches Hg
Static	-18.00	Inches H2O
Ps:	28.79	Inches Hg Abs.
Vlc:	110	ml + grams
Mn:	0.0000	gm
Test Time:	125	minutes
% O2:	6.80	%
% CO2:	11.20	%
% N2:	82.00	%
Delta H:	1.00	Inches H2O
Cp:	0.837	Dimensionless - pitot
Tm:	53.98	°F
Sqrt P:	0.704	Inches H2O
Ts:	316.12	°F
Vm:	65.732	Cubic Feet
Dn:	0.245	Inches - nozzle
As:	120.33	Sq. Feet
Yd:	1.009	Mcf
CF:	N/A	Process tons/hr
Heat Input:	N/A	MM BTU/hr
Fd:	N/A	dscf/10 <sup>6</sup> Btu
Fc:	N/A	scf/10 <sup>6</sup> Btu

Vmstd:	68.733	cubic feet (dry)
Vwstd:	5.186	cubic feet (wet)
Bwo:	0.070	
Md:	30.064	lb/lb-mole (dry)
Ms:	29.218	lb/lb-mole (wet)
Excess Air (%)	45.797	
Vs:	48.391	fps
ACFM:	349382.	
DSCFM:	212638.	
WSCFM:	228682	
%I:	95.1	isokinetic variance
GR/ACF:	---	
GR/DSCF:	---	
lbs/hr	---	
lbs/ton prod.:	N/A	
lbs/MM BTU:	N/A	Heat Input
lbs/MM BTU:	N/A	O2 Basis
lbs/MM BTU:	N/A	CO2 Basis

## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	2	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Outlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	N. Smith				
CONTROL BOX:	E-51				
METER NO.:	E-51				
METER CALIBRATION FACTOR:	1.009				
PITOT ID NO.:	318A				
PITOT TUBE COEFFICIENT:	0.837				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)		30.11		in. Hg.	
STATIC PRESSURE		-18		in. H2O	
FLUE PRESSURE (Ps)		28.79		in. Hg. abs.	
PROBE LENGTH:		13		ft.	
PROBE LINER MATERIAL:		Teflon			
NOZZLE IDENTIFICATION NO.:		8			
CALIBRATED NOZZLE DIAMETER:		0.245 in.			
LEAK CHECK		PRE:		0.000	
		POST:		0.000 @ 15 in. Hg.	
DUCT SHAPE:		Circular		DIA. Feet	
		Rectangular		12.6666 Feet	
DUCT AREA:		120.3327 sq. ft.			
TEST LENGTH:		125 min.			
MINUTES PER POINT:		5			
TOTAL NUMBER OF TRAVERSE POINTS:		25			



## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 2  
**Location:** Boiler #3 Baghouse Outlet

**SILICA GEL FINAL WT.:** 724.30 grams  
**SILICA GEL INITIAL WT.:** 707.40 grams  
**DIFFERENCE:** 16.90

**FINAL IMPINGER WATER:** 4754.50 mls.  
**INITIAL IMPINGER WATER:** 4661.50 mls.  
**DIFFERENCE:** 93.00

**TOTAL WATER GAIN:** 109.90

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.068		0.000000068
PROBE WASH:	0.000		0.000000000
		<b>Particle-bound Total:</b>	0.000000068
KCl:	2.386		0.000002386
		<b>Oxidized Total:</b>	0.000002386
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	0.478		0.000000478
KMNO <sub>4</sub> :	0.164		0.000000164
		<b>Elemental Total:</b>	0.000000642

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.00			11.00
Oxygen:	6.70			6.70

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:**            **Wisconsin Electric Power Company**

**Date:**                **11/30/99**

**Test Run:**           **2**

**Stack or Duct No.:** **Boiler #3 Baghouse Outlet**

**Start Time:**        **12:00**

**Stop Time:**        **14:17**

<b>Pb:</b>	<b>30.11</b>	<b>Inches Hg</b>
<b>Static</b>	<b>-18.00</b>	<b>Inches H2O</b>
<b>Ps:</b>	<b>28.79</b>	<b>Inches Hg Abs.</b>
<b>Vlc:</b>	<b>110</b>	<b>ml + grams</b>
<b>Mn:</b>	<b>0.0000</b>	<b>gm</b>
<b>Test Time:</b>	<b>125</b>	<b>minutes</b>
<b>% O2:</b>	<b>6.70</b>	<b>%</b>
<b>% CO2:</b>	<b>11.00</b>	<b>%</b>
<b>% N2:</b>	<b>82.30</b>	<b>%</b>
<b>Delta H:</b>	<b>1.05</b>	<b>Inches H2O</b>
<b>Cp:</b>	<b>0.837</b>	<b>Dimensionless - pitot</b>
<b>Tm:</b>	<b>69.32</b>	<b>°F</b>
<b>Sqrt P:</b>	<b>0.725</b>	<b>Inches H2O</b>
<b>Ts:</b>	<b>317.64</b>	<b>°F</b>
<b>Vm:</b>	<b>67.730</b>	<b>Cubic Feet</b>
<b>Dn:</b>	<b>0.245</b>	<b>Inches - nozzle</b>
<b>As:</b>	<b>120.33</b>	<b>Sq. Feet</b>
<b>Yd:</b>	<b>1.009</b>	<b>Mcf</b>
<b>CF:</b>	<b>N/A</b>	<b>Process tons/hr</b>
<b>Heat Input:</b>	<b>N/A</b>	<b>MM BTU/hr</b>
<b>Fd:</b>	<b>N/A</b>	<b>dscf/10<sup>6</sup> Btu</b>
<b>Fc:</b>	<b>N/A</b>	<b>scf/10<sup>6</sup> Btu</b>

<b>Vmstd:</b>	<b>68.778</b>	<b>cubic feet (dry)</b>
<b>Vwstd:</b>	<b>5.176</b>	<b>cubic feet (wet)</b>
<b>Bwo:</b>	<b>0.070</b>	
<b>Md:</b>	<b>30.028</b>	<b>lb/lb-mole (dry)</b>
<b>Ms:</b>	<b>29.186</b>	<b>lb/lb-mole (wet)</b>
<b>Excess Air (%)</b>	<b>44.586</b>	
<b>Vs:</b>	<b>49.931</b>	<b>fps</b>
<b>ACFM:</b>	<b>360499.</b>	
<b>DSCFM:</b>	<b>219014.</b>	
<b>WSCFM:</b>	<b>235497</b>	
<b>%I:</b>	<b>92.4</b>	<b>isokinetic variance</b>
<b>GR/ACF:</b>	<b>---</b>	
<b>GR/DSCF:</b>	<b>---</b>	
<b>lbs/hr</b>	<b>---</b>	
<b>lbs/ton prod.:</b>	<b>N/A</b>	
<b>lbs/MM BTU:</b>	<b>N/A</b>	<b>Heat Input</b>
<b>lbs/MM BTU:</b>	<b>N/A</b>	<b>O2 Basis</b>
<b>lbs/MM BTU:</b>	<b>N/A</b>	<b>CO2 Basis</b>

## ONTARIO HYDRO METHOD TEST SUPPORT DATA

PROJECT NO.:	94805	TEST RUN NO.:	3	TEST DATE:	11/30/99
CUSTOMER:	Wisconsin Electric Power Company				
PLANT:	Valley Power Plant				
TEST LOC.:	Boiler #3 Baghouse Outlet				
CLIENT:	Electric Power Research Institute				
OPERATOR:	N. Smith				
CONTROL BOX:	E-51				
METER NO.:	E-51				
METER CALIBRATION FACTOR:	1.009				
PITOT ID NO.:	318A				
PITOT TUBE COEFFICIENT:	0.837				
PORT LENGTH:	28 in.				
PORT SIZE:	6 in.				
PORT TYPE:	Flange				
BAROMETRIC PRESSURE (Pb)		30.11 in. Hg.			
STATIC PRESSURE		-18 in. H2O			
FLUE PRESSURE (Ps)		28.79 in. Hg. abs.			
PROBE LENGTH:		13 ft.			
PROBE LINER MATERIAL:		Teflon			
NOZZLE IDENTIFICATION NO.:		8			
CALIBRATED NOZZLE DIAMETER:		0.245 in.			
LEAK CHECK		PRE: 0.000		POST: 0.000 @ 15 in. Hg.	
DUCT SHAPE:		Circular		DIA. Feet	
DUCT AREA:		Rectangular		12.6666 Feet	
TEST LENGTH:		125 min.		120.3327 sq. ft.	
MINUTES PER POINT:		5			
TOTAL NUMBER OF TRAVERSE POINTS:		25			





## MOISTURE, DILUENT AND MERCURY DATA

**Company** Wisconsin Electric Power Compa **Date:** 11/30/99 **Test Run:** 3  
**Location:** Boiler #3 Baghouse Outlet

**SILICA GEL FINAL WT.:** 804.30 grams  
**SILICA GEL INITIAL WT.:** 789.80 grams  
**DIFFERENCE:** 14.50

**FINAL IMPINGER WATER:** 4734.90 mls.  
**INITIAL IMPINGER WATER:** 4631.00 mls.  
**DIFFERENCE:** 103.90

**TOTAL WATER GAIN:** 118.40

ITEM	MERCURY (UG)	=	NET WT. (G)
FILTER:	0.006		0.000000006
PROBE WASH:	0.000		0.000000000
		<b>Particle-bound Total:</b>	0.000000006
KCl:	3.086		0.000003086
		<b>Oxidized Total:</b>	0.000003086
HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> :	0.773		0.000000773
KMNO <sub>4</sub> :	0.070		0.000000070
		<b>Elemental Total:</b>	0.000000843

Orsat Analysis	1	2	3	Average
Carbon Dioxide:	11.20			11.20
Oxygen:	6.70			6.70

# ONTARIO HYDRO METHOD DATA ENTRY FORM

## Field Data/Calculated Data

**Company:** Wisconsin Electric Power Company

**Date:** 11/30/99

**Test Run:** 3

**Stack or Duct No.:** Boiler #3 Baghouse Outlet

**Start Time:** 14:50

**Stop Time:** 17:10

<b>Pb:</b>	30.11	Inches Hg
<b>Static</b>	-18.00	Inches H2O
<b>Ps:</b>	28.79	Inches Hg Abs.
<b>Vlc:</b>	118	ml + grams
<b>Mn:</b>	0.0000	gm
<b>Test Time:</b>	125	minutes
<b>% O2:</b>	6.70	%
<b>% CO2:</b>	11.20	%
<b>% N2:</b>	82.10	%
<b>Delta H:</b>	1.09	Inches H2O
<b>Cp:</b>	0.837	Dimensionless - pitot
<b>Tm:</b>	50.72	°F
<b>Sqrt P:</b>	0.737	Inches H2O
<b>Ts:</b>	317.76	°F
<b>Vm:</b>	69.250	Cubic Feet
<b>Dn:</b>	0.245	Inches - nozzle
<b>As:</b>	120.33	Sq. Feet
<b>Yd:</b>	1.009	Mcf
<b>CF:</b>	N/A	Process tons/hr
<b>Heat Input:</b>	N/A	MM BTU/hr
<b>Fd:</b>	N/A	dscf/10 <sup>6</sup> Btu
<b>Fc:</b>	N/A	scf/10 <sup>6</sup> Btu

<b>Vmstd:</b>	72.889	cubic feet (dry)
<b>Vwstd:</b>	5.577	cubic feet (wet)
<b>Bwo:</b>	0.071	
<b>Md:</b>	30.060	lb/lb-mole (dry)
<b>Ms:</b>	29.203	lb/lb-mole (wet)
<b>Excess Air (%)</b>	44.743	
<b>Vs:</b>	50.751	fps
<b>ACFM:</b>	366420.	
<b>DSCFM:</b>	222318.	
<b>WSCFM:</b>	239327	
<b>%I:</b>	96.5	isokinetic variance
<b>GR/ACF:</b>	---	
<b>GR/DSCF:</b>	---	
<b>lbs/hr</b>	---	
<b>lbs/ton prod.:</b>	N/A	
<b>lbs/MM BTU:</b>	N/A	Heat Input
<b>lbs/MM BTU:</b>	N/A	O2 Basis
<b>lbs/MM BTU:</b>	N/A	CO2 Basis





## *Project Summary-Samples Received Report*

<i>Project</i>	<i>Client</i>	<i>Unit</i>		
94805	WEPCO	VALLEY-MILWAUKEE,WI		
<i>Project</i>	<i>Sample</i>	<i>Sample Point</i>	<i>Date Received</i>	<i>Analyte Detail</i>
94805	001	INL FILTER T1	12/1/1999	Mercury
94805	002	INL FILTER T2	12/1/1999	Mercury
94805	003	INL FILTER T3	12/1/1999	Mercury
94805	004	INL HNO3 RNS T1	12/1/1999	Mercury
94805	005	INL HNO3 RNS T2	12/1/1999	Mercury
94805	006	INL HNO3 RNS T3	12/1/1999	Mercury
94805	007	INL KCL IMP T1	12/1/1999	Mercury
94805	008	INL KCL IMP T2	12/1/1999	Mercury
94805	009	INL KCL IMP T3	12/1/1999	Mercury
94805	010	IN HNO3/H2O2 T1	12/1/1999	Mercury
94805	011	IN HNO3/H2O2 T2	12/1/1999	Mercury
94805	012	IN HNO3/H2O2 T3	12/1/1999	Mercury
94805	013	INL KMNO4 IM T1	12/1/1999	Mercury
94805	014	INL KMNO4 IM T2	12/1/1999	Mercury
94805	015	INL KMNO4 IM T3	12/1/1999	Mercury
94805	016	OUT FILTER T1	12/1/1999	Mercury
94805	017	OUT FILTER T2	12/1/1999	Mercury
94805	018	OUT FILTER T3	12/1/1999	Mercury
94805	019	OUT HNO3 RNS T1	12/1/1999	Mercury
94805	020	OUT HNO3 RNS T2	12/1/1999	Mercury
94805	021	OUT HNO3 RNS T3	12/1/1999	Mercury
94805	022	OUT KCL IMP T1	12/1/1999	Mercury
94805	023	OUT KCL IMP T2	12/1/1999	Mercury
94805	024	OUT KCL IMP T3	12/1/1999	Mercury
94805	025	OUT HNO3/H2O2-1	12/1/1999	Mercury
94805	026	OUT HNO3/H2O2-2	12/1/1999	Mercury

*Monday, March 06, 2000*

<i>Project</i>	<i>Sample</i>	<i>Sample Point</i>	<i>Date Received</i>	<i>Analyte Detail</i>
94805	027	OUT HNO3/H2O2-3	12/1/1999	Mercury
94805	028	OUT KMNO4 IM T1	12/1/1999	Mercury
94805	029	OUT KMNO4 IM T2	12/1/1999	Mercury
94805	030	OUT KMNO4 IM T3	12/1/1999	Mercury
94805	031	FLD BL INL KCL	12/1/1999	Mercury
94805	032	F/B INHNO3/H2O2	12/1/1999	Mercury
94805	033	FLD BL IN KMNO4	12/1/1999	Mercury
94805	034	FLD BL OUT KCL	12/1/1999	Mercury
94805	035	F/B HNO3/H2O2	12/1/1999	Mercury
94805	036	F/B OUTL KMNO4	12/1/1999	Mercury
94805	037	BLANK:QRTZ FLT	12/1/1999	Mercury
94805	038	BLANK:QRTZ FLT	12/1/1999	Mercury
94805	039	BLANK:QRTZ FLT	12/1/1999	Mercury
94805	040	REAG BL HNO3	12/1/1999	Mercury
94805	041	REAG BL KCL	12/1/1999	Mercury
94805	042	R/BL HNO3/H2O2	12/1/1999	Mercury
94805	043	REAG BL KMNO4	12/1/1999	Mercury
94805	044	R/BL HYDROXYLAM	12/1/1999	Mercury
94805	045	COAL SAMPLE T1	12/1/1999	Chlorine
94805	045	COAL SAMPLE T1	12/1/1999	Ultimate/Proximate on Coal
94805	045	COAL SAMPLE T1	12/1/1999	Mercury
94805	046	COAL SAMPLE T2	12/1/1999	Mercury
94805	046	COAL SAMPLE T2	12/1/1999	Chlorine
94805	046	COAL SAMPLE T2	12/1/1999	Ultimate/Proximate on Coal
94805	047	COAL SAMPLE T3	12/1/1999	Ultimate/Proximate on Coal
94805	047	COAL SAMPLE T3	12/1/1999	Mercury
94805	047	COAL SAMPLE T3	12/1/1999	Chlorine
94805	048	ASH SAMPLE T1	12/1/1999	Mercury
94805	048	ASH SAMPLE	12/1/1999	Chlorine

Monday, March 06, 2000







# LABORATORY REPORT



TEI Analytical, Inc.  
 7177 N. Austin  
 Niles, IL 60714-4617  
 847-647-1345

PREPARED FOR:

PAGE 1 of 3

Frank Jarke  
 Mostardi-Platt Associates, Inc.  
 945 Oaklawn Avenue  
 Elmhurst, IL 60126

Report #: 38837 Corrected  
 Report Date: 2/24/00  
 Sample Received:  
 1/3/00 15:45

TEI	94805	Type	Total ug	mg/kg	Date	%RSD	Lin.Reg.	Blank	CPI	MS	MSD
38837	001	Filter		0.019	1/24/2000	0.298	0.99999	0.11	97.1	97.1	101
38838	002	Filter		0.017	1/24/2000	0.976	0.99999	0.11	97.1	97.1	101
38839	003	Filter		0.016	1/24/2000	0.39	0.99999	0.11	97.1	97.1	101
38840	004	HNO3	<0.003		2/23/2000	7.53	1	NA	98	117	117
38841	005	HNO3	0.025		2/23/2000	4.54	1	NA	98	117	117
38842	006	HNO3	0.014		2/23/2000	1.37	1	NA	98	117	117
38843	007	KCl	2.1		2/3/2000	2.58	0.99997	0.232	93.2	111	95
38844	008	KCl	2.22		2/3/2000	0.341	0.99997	0.232	93.2	111	95
38845	009	KCl	1.81		2/3/2000	0.491	0.99997	0.232	93.2	111	95
38846	010	H2O2	1.33		1/18/2000	0.913	0.99992	0.116	94.5	118	114
38847	011	H2O2	0.362		1/18/2000	0.26	0.99992	0.116	94.5	118	114
38848	012	H2O2	0.57		1/24/2000	0.918	0.99999	0.116	97.1	97.1	101
38849	013	KMnO4	0.447		2/23/2000	5.12	1	0.031	97.4	100	86
38850	014	KMnO4	0.314		2/23/2000	5.1	1	0.031	97.4	100	86
38851	015	KMnO4	0.421		2/23/2000	2.53	1	0.031	97.4	100	86
38852	016	Filter		0.052	1/24/2000	0.47	0.99999	0.11	97.1	97.1	101
38853	017	Filter		0.019	1/24/2000	0.099	0.99999	0.11	97.1	97.1	101
38854	018	Filter		<0.004	1/24/2000	1.44	0.99999	0.11	97.1	97.1	101
38855	019	HNO3	<0.003		2/23/2000	3.73	1	NA	98	117	117
38856	020	HNO3	<0.003		2/23/2000	4.18	1	NA	98	117	117
38857	021	HNO3	<0.003		2/23/2000	5.09	1	NA	98	117	117
38858	022	KCl	3.09		2/3/2000	0.172	0.99997	0.232	93.2	111	95
38859	023	KCl	2.39		2/3/2000	0.206	0.99997	0.232	93.2	111	95
38860	024	KCl	3.09		2/3/2000	0.277	0.99997	0.232	93.2	111	95
38861	025	H2O2	0.339		2/3/2000	1.96	0.99997	0.116	95.2	120	117
38862	026	H2O2	0.478		2/3/2000	0.813	0.99997	0.116	95.2	120	117
38863	027	H2O2	0.773		2/3/2000	0.5	0.99997	0.116	95.2	120	117

*Gayle E. O'Neill*  
 Gayle E. O'Neill, Ph.D.

# LABORATORY REPORT



TEI Analytical, Inc.  
7177 N. Austin  
Niles, IL 60714-4617  
847-647-1345

PREPARED FOR:

PAGE 2 of 3

Frank Jarke  
Mostardi-Platt Associates, Inc.  
945 Oaklawn Avenue  
Elmhurst, IL 60126

Report #: 38837 Corrected  
Report Date: 2/24/00  
Sample Received:  
1/3/00      15:45

TEI	94805	Type	Total ug	mg/kg	Date	%RSD	Lin.Reg.	Blank	CPI	MS	MSD
38864	028	KMnO4	0.288		2/23/2000	1.71	1	0.031	97.4	100	86
38865	029	KMnO4	0.172		2/23/2000	1.57	1	0.031	97.4	100	86
38866	030	KMnO4	0.078		2/23/2000	4.15	1	0.031	97.4	100	86
38867	031	KCl	0.388		2/3/2000	0.893	0.99997	0.232	93.2	111	95
38868	032	H2O2	0.279		2/3/2000	0.031	0.99997	0.116	93.2	120	117
38869	033	KMnO4	0.074		2/23/2000	43.4	1	0.031	97.4	100	86
38870	034	KCl	0.363		2/3/2000	0.756	0.99997	0.232	93.2	111	95
38871	035	H2O2	0.235		2/3/2000	0.351	0.99997	0.116	93.2	120	117
38872	036	KMnO4	0.075		2/23/2000	12.7	1	0.031	97.4	100	86
38873	037	Filter		<0.004	1/24/2000	3.11	0.99999	0.11	97.1	97.1	101
38874	038	Filter		<0.004	1/24/2000	0.335	0.99999	0.11	97.1	97.1	101
38875	039	Filter		0.024	1/24/2000	0.537	0.99999	0.11	97.1	97.1	101
38876	040	HNO3	<0.003		2/23/2000	2.54	1	NA	98	117	117
38877	041	KCl	0.004		2/23/2000	54.7	1	NA	98	117	117
38878	042	H2O2	<0.007		2/3/2000	2.88	0.99997	0.116	95.2	120	117
38879	043	KMnO4	0.008		2/23/2000	2.49	1	0.031	97.4	100	86
38880	044	NH2OH	<0.003		2/23/2000	2.62	1	NA	97.4	117	117

*Gayle E. O'Neill*  
\_\_\_\_\_  
Gayle E. O'Neill, Ph.D.

# LABORATORY REPORT



TEI Analytical, Inc.  
7177 N. Austin  
Niles, IL 60714-4617  
847-647-1345

PREPARED FOR:

PAGE 3 of 3

Frank Jarke  
Mostardi-Platt Associates, Inc.  
945 Oaklawn Avenue  
Elmhurst, IL 60126

Report #: 38837 Corrected  
Report Date: 2/24/00  
Sample Received:  
1/3/00 15:45

## Mercury (Ontario Hydro Method)

The QAPP called for the analysis of all samples in duplicate with every tenth sample run in triplicate. To simplify the instrument setup, we chose to run all samples, blanks, standards, matrix spikes and matrix spike duplicates in triplicate. The reported %RSD is for the triplicate measurements.

All sample results are reported as total micrograms in the sample received by the laboratory, with the exception of the filter samples. The filter sample results are expressed as mg/kg.

The instrument was calibrated at least daily with a blank and four standards. The Lin.Reg. column in this report represents the linear regression coefficient obtained during the calibration.

The laboratory method blank is reported in ug/l in the Blank column of this report. For samples requiring only addition of Hydroxylamine Hydrochloride, NA is entered in this column. No laboratory method blanks were applicable for these samples.

The CPI column presents the % Recovery of an independent standard (obtained from CPI). The calibration curve was prepared in our laboratory from Mercuric Chloride in accordance with EPA Method 7470.

The MS and MSD columns present the % Recovery of the Matrix Spikes and Matrix Spike Duplicates.

  
Gayle E. O'Neill, Ph.D.



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ADDRESS ALL CORRESPONDENCE TO:  
16130 VAN DRUNEN RD.  
SOUTH HOLLAND, IL 60473  
TEL: (708) 331-2900  
FAX: (708) 333-3060

December 14, 1999

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample reported to us Coal

MPA Sample No: 94805-045

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108390

Page 1 of 2

### PROXIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.70	XXXXX
% Ash	7.19	7.88
% Volatile	34.16	37.42
% Fixed Carbon	<u>49.95</u>	<u>54.70</u>
	100.00	100.00
Btu/lb	12159	13318
% Sulfur	0.78	0.85
MAF Btu		14457

### ULTIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.70	XXXXX
% Carbon	68.68	75.22
% Hydrogen	4.46	4.89
% Nitrogen	1.54	1.69
% Sulfur	0.78	0.85
% Ash	7.19	7.88
% Oxygen (diff)	<u>8.65</u>	<u>9.47</u>
	100.00	100.00
CHLORIDE ug/g	113	124

### METHODS

Moisture: ASTM D 3302; Ash: ASTM D 3174; Volatile: ASTM D 3175; Fixed Carbon: Calculated Value; ASTM D 3172  
Btu/lb: ASTM 3286; Sulfur: ASTM D 4239 (Method C); Carbon, Hydrogen & Nitrogen: ASTM D 5373; Chloride: ASTM D 4208

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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December 14, 1999

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample reported to us Coal

MPA Sample No: 94805-045

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108390

Page 2 of 2

	<u>Dry Basis, ug/g</u>	<u>MDL, ug/g</u>
Mercury, Hg	0.07	0.01
	<u>Expected</u>	<u>Observed</u>
SARM 1157	0.05	0.05
NIST 1630A	0.11	0.10

MDL Denotes Method Detection Limit

METHOD

Mercury: ASTM D 3684

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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FAX: (708) 333-3060

December 14, 1999

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample  
reported to us Coal

MPA Sample No: 94805-046

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108391

Page 1 of 2

### PROXIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.35	xxxxxx
% Ash	7.17	7.82
% Volatile	34.03	37.13
% Fixed Carbon	<u>50.45</u>	<u>55.05</u>
	100.00	100.00
Btu/lb	12161	13269
% Sulfur	0.78	0.85
MAF Btu		14395

### ULTIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.35	xxxxxx
% Carbon	68.93	75.21
% Hydrogen	4.53	4.94
% Nitrogen	1.53	1.67
% Sulfur	0.78	0.85
% Ash	7.17	7.82
% Oxygen (diff)	<u>8.71</u>	<u>9.51</u>
	100.00	100.00
CHLORIDE ug/g	123	134

### METHODS

Moisture: ASTM D 3302; Ash: ASTM D 3174; Volatile: ASTM D 3175; Fixed Carbon: Calculated Value; ASTM D 3172  
Btu/lb: ASTM 3286; Sulfur: ASTM D 4239 (Method C); Carbon, Hydrogen & Nitrogen: ASTM D 5373; Chloride: ASTM D 4208

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Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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December 14, 1999

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample  
reported to us Coal

MPA Sample No: 94805-046

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108391

Page 2 of 2

	<u>Dry Basis, ug/g</u>	<u>MDL, ug/g</u>
Mercury, Hg	0.07	0.01
	<u>Expected</u>	<u>Observed</u>
SARM 1157	0.05	0.05
NIST 1630A	0.11	0.10

MDL Denotes Method Detection Limit

METHOD

Mercury: ASTM D 3684

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample  
reported to us Coal

MPA Sample No: 94805-047

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108392

Page 1 of 2

### PROXIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.91	xxxxxx
% Ash	6.50	7.14
% Volatile	33.62	36.91
% Fixed Carbon	<u>50.97</u>	<u>55.95</u>
	100.00	100.00
Btu/lb	12257	13456
% Sulfur	0.84	0.92
MAF Btu		14491

### ULTIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>
% Moisture	8.91	xxxxxx
% Carbon	68.70	75.42
% Hydrogen	4.50	4.94
% Nitrogen	1.53	1.68
% Sulfur	0.84	0.92
% Ash	6.50	7.14
% Oxygen (diff)	<u>9.02</u>	<u>9.90</u>
	100.00	100.00
CHLORIDE ug/g	114	125

### METHODS

Moisture: ASTM D 3302; Ash: ASTM D 3174; Volatile: ASTM D 3175; Fixed Carbon: Calculated Value; ASTM D 3172  
Btu/lb: ASTM 3286; Sulfur: ASTM D 4239 (Method C); Carbon, Hydrogen & Nitrogen: ASTM D 5373; Chloride: ASTM D 4208

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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December 14, 1999

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample reported to us Coal

MPA Sample No: 94805-047

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received December 3, 1999

P.O. No. 22688

Analysis Report No. 71-108392

Page 2 of 2

	<u>Dry Basis, ug/g</u>	<u>MDL, ug/g</u>
Mercury, Hg	0.07	0.01
	<u>Expected</u>	<u>Observed</u>
SARM 1157	0.05	0.05
NIST 1630A	0.11	0.10

MDL Denotes Method Detection Limit

METHOD  
Mercury: ASTM D 3684

105  
Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.  
*[Signature]*  
South Holland Laboratory



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FAX: (708) 333-3060

February 22, 2000

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample  
reported to us Ash

MPA Sample No: 94805-048

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received February 10, 2000

P.O. No. 23037

Analysis Report No. 71-114323

Page 2 of 2

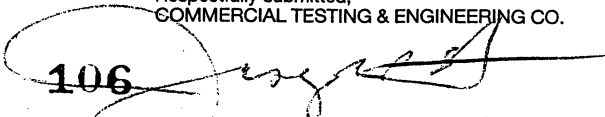
	<u>Dry Basis, ug/g</u>	<u>MDL, ug/g</u>
Mercury, Hg	0.05	0.01
	<u>Expected</u>	<u>Observed</u>
SARM 1157	0.05	0.05
NIST 1630A	0.11	0.10

MDL Denotes Method Detection Limit

METHOD

Mercury: ASTM D 3684

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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TEL: (708) 331-2900  
FAX: (708) 333-3060

February 22, 2000

MOSTARDI-PLATT ASSOCIATES, INC  
945 Oaklawn Avenue  
Elmhurst, IL 60126  
Attn: Frank Jarke

Sample identification by  
Mostardi-Platt Assoc., Inc.

Kind of sample  
reported to us Ash

MPA Sample No: 94805-048

Sample taken at -----

Sample taken by Mostardi-Platt Assoc., Inc.

Date sampled November 30, 1999

Date received February 10, 2000

P.O. No. 23037

Analysis Report No. 71-114323

Page 1 of 2

Dry Basis

% Chloride 0.02

METHOD

Chloride: ASTM D 4208

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

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**Final Results**

April 18, 2000

Set Number: 49978

Request Date: Tuesday, March 28, 2000

Fund#: 4694

Due Date: Tuesday, April 11, 2000

PI: Carolyn Lillemoen

Set Description: ICR Coal Samples

Contact Person: C. Lillemoen

Sample	49978-01
	AB82383 PW #32 Mill
	Mercury 0.15 µg/g
	49978-02 AB82384 PW #32 Mill
	Mercury 0.15 µg/g
	49978-03 AB82385 PW #32 Mill
	Mercury 0.15 µg/g
	49978-04 AB82386 PW #41 Mill
	Mercury 0.13 µg/g
	49978-05 AB82387 PW #41 Mill
	Mercury 0.13 µg/g
	49978-06 AB82388 PW #41 Mill
	Mercury 0.13 µg/g
	49978-07 AB82389 VA #3A FDR
	Mercury 0.0092 µg/g
	49978-08 AB82390 VA #3B FDR
	Mercury 0.013 µg/g
	49978-09 AB82391 VA #3 FDR
	Mercury 0.015 µg/g
	49978-10 AB 82383 PW#32 Mill microwave digestion
	Mercury 0.186 µg/g
	49978-11 AB 82391 VA #3 FDR microwave digestion
	Mercury 0.014 µg/g

Coal samples 49978-01 through 49978-09 were analyzed for total Hg using EPA Method 7473; "Mercury in Solids and Solutions by Thermal Decomposition Amalgamation and Atomic Absorption Spectrophotometry". The instrument used for the analysis was the DMA-80a (Milestone, Inc.)

For comparison, samples 49978-01 and 49978-09 were renumbered 49978-10 and 49978-11 respectively, and prepared using EPA Method 3052; "Microwave Assisted Acid Digestion of Siliceous and Organically Based Matrices". The microwave used for the digestion was a MDS2100 (CEM Corporation). The digested samples were analyzed using EPA Method 7471a; "Mercury in Solid or Semisolid Wastes by Cold Vapor Atomic Absorption Spectroscopy". The instrument used for analysis was a M6000a Mercury Analyzer (CETAC Technologies, Inc.)

Distribution CML Date 4/18/00

**Final Results**

April 18, 2000

Set Number: 49973

Request Date: Tuesday, March 21, 2000

Fund#: 4694

Due Date: Tuesday, April 04, 2000

PI: Carolyn Lillemoen

Set Description: ICR Fly Ash

Contact Person: C. Lillemoen

Sample 49973-01

49973-01 WEPCO-Port Washington ESP Ash #94606-054

Mercury 0.621 µg/g

49973-02 WEPCO-Milwaukee Ash #94805-049

Mercury 0.0363 µg/g

Sample 49973-01 and 49973-02 were prepared using EPA Method 3051; "Microwave Assisted Acid Digestion of Siliceous and Organically Based Matrices". The microwave used for the digestion was a MDS2100 (CEM Corporation). The digested samples were analyzed using EPA Method 7471a; "Mercury in Solid or Semisolid Wastes by Cold Vapor Atomic Absorption Spectroscopy". The instrument used for analysis was a M6000a Mercury Analyzer (CETAC Technologies, Inc.)

Distribution CML Date 4/18/00



## LIST OF PARTICIPANTS

<u>Name</u>	<u>Organization</u>	<u>Project Role</u>
Ms. Brenda Bergemann .....	WEPCO .....	Plant Coordinator
Mr. Paul Chu .....	EPRI .....	Program Manager
James R. Platt .....	Mostardi Platt .....	Vice President
John Wendell .....	Mostardi Platt .....	Laboratory Chemist
Dave Agbakoba .....	Mostardi Platt .....	Test Technician
Chris Christensen .....	Mostardi Platt .....	Test Technician
Dave Helm .....	Mostardi Platt .....	Test Technician
Norm Smith .....	Mostardi Platt .....	Test Technician
Gayle O'Neill, Ph.D. ....	TEI Analytical, Inc. ....	Speciated Hg Sample Analysis
Joseph Houser .....	CTE .....	Coal Sample Analysis
Dennis Laudal .....	EERC .....	Coal/Ash Sample Analysis

