AIAA-2000-4296

THE EFFECT OF SIMULATOR MOTION ON PILOT TRAINING AND EVALUATION*

Tiauw H.Go^H Massachusetts Institute of Technology, Cambridge, Massachusetts

> Judith Bürki-Cohen^I Volpe Center, U.S. Department of Transportation, Cambridge, Massachusetts

> > Nancy N. Soja³ Brookline, Massachusetts

ABSTRACT

This study empirically examined the effect of simulator platform motion on airline pilot recurrent training and evaluation. It is driven by the need for sound scientific data on the relationship between certain key modern device features and their effect on the transfer of pilot performance and behavior to and from the respective airplane. The experiment utilized an FAA qualified Level C simulator with six-degree-of-freedom synergistic motion and a wide angle high quality visual system. Experienced airline pilots were evaluated and trained in the simulator, half of them with and the other half without motion. Then the transfer of skills acquired by both groups during this training was tested in the simulator with the motion system turned on as a standin for the airplane (quasi-transfer). Every effort was made to avoid deficiencies in the research design identified in a review of prior studies, by measuring pilot stimulation and response, testing both maneuvers and pilots that are *diagnostic* of a need of motion, avoiding pilot and instructor bias, and ensuring sufficient statistical *power* to capture operationally relevant effects. The results of the analyses as well as their implications are presented in this paper.

NOTATIONS

- FAA Federal Aviation Administration
- PTS FAA Practical Test Standards

RTO Rejected Take-Off

- V_1 Take-off decision speed; the minimum speed in the take-off, following a failure of the critical engine, at which the pilot can continue the take-off and achieve the required height above the take-off surface within the take-off distance.
- V_1 cut Engine failure at or above V_1 with continued take-off
- V₂ Take-off safety speed; a speed that will provide at least the gradient of climb required by the airplane certification rules with the critical engine inoperative.
- PF Pilot Flying
- PNF Pilot Not Flying
- I/E Instructor/Evaluator
- n Sample size
- *p* Probability of null hypothesis (i.e., no effect of motion)
- *r* Pearson correlation coefficient
- STD Standard Deviation

INTRODUCTION

This research effort is part of the Federal Aviation Administration's (FAA) initiative towards promoting the availability and affordability of flight simulators for U.S. commuter airline training.² This initiative becomes even more important as the FAA is proposing a rule that would mandate the use of simulators for all air carrier training and qualification, limiting the use of the aircraft itself as a training option even for small regional airlines. However, there is a lack of sound scientific data on the relationship between

^{*} Portions of this work have been published as Ref. 1.

^H Postdoctoral Associate, Department of Aeronautics and Astronautics, Member AIAA.

^I Engineering Psychologist.

⁹ Consultant, experimental psychology.

This paper is declared a work of the U.S. Government and is not subject to copyright protection in the United States.

certain key training device features, such as platform motion cuing, and their effect on the transfer of performance to and from the airplane. This project will develop a scientific basis to assure that FAA requirements promote full transfer of pilot performance between simulator and airplane without unnecessarily driving up cost. The data will also help the FAA to evaluate air carrier proposals for the alternative use of other training equipment in lieu of full flight simulators without compromising safety objectives. The first stage of this multi-year project was a state-of-the-art review of key aspects of flight simulation, involving both FAA and Industry subject matter expert workshops^{3,4} and an extensive literature review.^{5,6,7} Based on this review, an empirical investigation of flight simulator requirements which seeks to correct deficiencies in the research design of prior studies has been initiated.

The present study empirically examined the effect of platform motion (i.e., FAA qualified Level C six-degree-of-freedom synergistic motion) in the presence of a high-level visual system (i.e., wide-angle collimated cross-cockpit) on pilot training and pilot evaluation. It addressed the questions of whether the motion provided by an FAA qualified Level C simulator affects 1) First Look evaluation of pilot performance and behavior prior to any simulator practice, 2) the course of Training in the simulator, and 3) the Transfer of training acquired during training in the simulator with or without motion to the simulator with motion as a stand-in for the airplane. The analysis also examined whether the grading criteria used by the instructors/evaluators (I/Es) were affected by the presence or absence of motion. The resolution of the experiment was also considered, i.e., the power to find the effect of motion if there is one.

RESEARCH METHOD

The experiment used an FAA qualified Level C flight simulator, which represents a 30 passenger, three crew, turboprop airplane with wing-mounted twin engines and counter-rotating propellers. The six degree-of-freedom synergistic motion system has hydraulically actuated legs capable of a 60 inch stroke. The high quality visual system provides wide angle collimated cross-cockpit viewing with a 150 degrees horizontal and 40 degrees vertical field of view available to each pilot.

The research was conducted with regional airline pilots in recurrent training. Data were collected from 42 crews. Two experiments were combined into one experimental session in order to minimize the disruption to the host airline's training and evaluation

program, as well as to reduce pilot adaptation to a simulator configuration. Both experiments investigated the need for platform motion in simulators, focusing on different functions of the simulator. The first experiment, First Look evaluation, examined the use of simulators as *evaluation* tools of pilots' aviating skills. In other words, it assessed the degree to which a pilot's existing skills transferred from the airplane to the simulator, and whether this was affected by the motion state of the simulator. This assessment needed to occur during the very initial exposure of the crew to the simulator, so that pilots' behavior and performance would reflect their actual skills in the airplane with as little contamination as possible from potential adaptation to a particular simulator configuration. The second experiment, Training and Transfer testing, examined the use of simulators as training tools for aviating skills, skills that would eventually need to be transferred to the airplane. That is, the experiment assessed the degree to which motion affected the training of skills and, most importantly, the transfer of those skills to the airplane. Training transfer was measured by comparing the effect of training received in the simulator, with and without motion, on performance and behavior in the simulator with motion (as a stand-in for the airplane, "quasi-transfer" design).

Two test maneuvers (i.e., pilot tasks) were chosen to maximize satisfaction of criteria described in the literature as diagnostic for the detection of a motion requirement, given the constraint that the experiment was conducted in the context of an FAA approved training program. These criteria included 1) closed loop, to allow for motion to be part of the control feedback loop to the pilot; 2) unpredictable and asymmetric disturbance, to highlight an early alerting function of motion;⁸ 3) high gain and high thrust, to magnify any motion effects; 4) high workload with crosswind and low visibility, to increase the need for redundant cues such as provided by motion, out-thewindow view, instruments and sound; and 5) short duration, to prevent pilots from adjusting to a lack of cues. Engine failures on take-off with either rejected take-off (RTO) or continued take-off (V1 cut) were deemed fulfilling most of these criteria, while requiring minimum disruption to the host airline's existing training program. To prevent bias, the state of the motion system was kept concealed from all participants.

A laptop computer was programmed to control the simulator and record events with minimal I/E intervention, eliminating the need for the presence of an experimenter that might have contaminated the regular training/evaluation environment. It also enabled the I/E to focus on behavior and performance of the crew. Most importantly, it also eliminated any need to inform the I/E (or the crew) of the interest in motion and the motion state of the simulator for each maneuver, thus minimizing any bias. To prevent the pilots from guessing which maneuvers were to come during the final testing, they were given two normal take-offs without being informed about the lack of engine failures, with the motion platform still in its original configuration.

The chronology of an experimental session is explained next. First, the crews did one V1 cut followed by one RTO (First Look evaluation). Half of them did it with the motion system on (Motion group) and the other half with the motion system off (No-Motion group). Any additional training needed to reach the company standards for RTO and V1 cut came next, with motion on or off depending on group. At most, there were two additional training trials for each type of maneuver. After Training, all participants filled out a questionnaire. This was followed by two normal takeoffs with the same motion configuration. Then the crews did one last V1 cut followed by one last RTO with motion on for all crews (Transfer). After Transfer participants filled out a second testing, all questionnaire, to see whether their opinions had changed after all had experienced motion.

The stimulation of the PF by the simulator and the pilots' responses were measured by recording 78 simulator state and control input variables at a high sampling rate, resulting in a vast amount of objective data on simulator performance and pilot performance and behavior/workload. Two forms of subjective data were also collected. First, at the conclusion of each maneuver the I/E provided a grade for the justcompleted maneuver. Second, as already mentioned in the previous paragraph, at the end of the training period and again at the end of the transfer period all participants were queried on PF performance and workload as well as simulator comfort and acceptability. From this set of data, four types of results were obtained: 1) the motion stimulation at the PF station, 2) the effect of motion on the performance of the PFs as perceived by the I/Es and reflected in their grading, 3) the relationship between I/E grades and the objective measures of pilot performance/workload and whether this relationship was affected by motion; and 4) the effect of motion on measured performance and workload of the PFs, and the effect of motion on participants opinion regarding PF performance /workload and simulator comfort and acceptability.

MOTION STIMULATION PROVIDED BY THE TEST SIMULATOR

For the test simulator, the actually measured roll and longitudinal accelerations followed the airplane model fairly well given the limitations inherent to all simulators. For vertical acceleration, however, the motion system of the test simulator did not respond much to the command provided by the equations of motion. This is especially true for V_1 cut maneuvers. However, because the engine failures used in our experiment do not produce much vertical acceleration, the lack of vertical acceleration cuing may not be very important.

More important, however, is the finding that failure-induced lateral acceleration was not well represented by the motion system of the test simulator. Not only was it greatly attenuated, but visual inspection of the measured response does not lead to an easy distinction of failure-induced lateral acceleration, unlike the response derived from the equations of motion (relatively high peak shortly after engine failure).⁷ This may represent a significant deficiency in pilot stimulation, because lateral acceleration may act as a useful cue for proper failure recognition and for initiation of appropriate response. Further research, however, still need to be done to examine the importance of lateral versus other cues in failure recognition.

I/E GRADES

The grade distribution obtained by the two groups at First Look evaluation and Transfer is depicted in Fig. 1. The possible grades were 1 (unsatisfactory), 2 (FAA Practical Test Standards (PTS)⁹), 3 (company standards), and 4 (excellent). The experimental sessions appeared to have been effective in simulating a real training session in that the crews' performance improved across the session. Specifically, combining the two motion groups (or looking at them individually), the grades for RTOs and V₁ cuts improved across the training trials. This was even stronger for the V₁ cuts, which elicited lower grades than the RTOs during First Look, but caught up by Transfer.

Platform motion had no effect on the grades that were provided by the I/Es at any time for either the RTO or the V_1 cut or for the normal take-offs. That is, platform motion did not affect First Look evaluation in the simulator, nor did it affect the grades at Transfer to the simulator with motion. The latter was true when comparing the group means and the number of low vs. high grades in each group (i.e., grades of 3 and 4 vs. grades of 1 and 2). However, on V_1 cut at Transfer the crews which previously had motion did receive more grades of 2 than the crews who had not previously had motion, and fewer grades of 1 (none actually). Despite this single effect of motion, there was no effect of motion on the course of Training or on the amount of Training required before reaching the criterion needed to move onto Transfer for either of the maneuvers. For the complete statistical analyses, see Ref. 7.



MEASURED PERFORMANCE AND WORKLOAD OF PILOT FLYING

From the 78 variables recorded in the experiment, a set of criterion measures was derived for determining whether or not motion had an effect on training and evaluation of the tested pilot task. These performance were categorized into and workload/behavior measures. Performance measures reflect a pilot's control precision and efficiency in handling the airplane by measurements such as flight path deviations and reaction time. Workload/behavior measures describe how a pilot uses the controls by measurement of control inputs. A guide to the determination of the measures was provided by the PTS and by the company standards of the host airline itself. An additional goal was to capture performance and workload immediately after the engine failure, because disturbance motion was expected to act as an alerting cue to the pilots that would enhance early performance. The list of the measures can be seen in Ref. 7. Most of the measures were computed over the 15 second time

period following an engine failure. Exceptions include measures of reaction times and Time to Reach 400 ft Altitude. In general, lower numerical values of the measures indicate better performance or lower workload.

The effect of motion on First Look evaluation, Transfer of training to the simulator, Training progress, and improvement from last training trial to Transfer testing was examined. Because the I/Es shared the motion platform with the pilots, and thus might have been affected by the motion status of the simulator in their grading criteria, the relationship between I/E grades and the objective measures was examined by performing regression analyses. In addition to determining whether the presence or absence of motion influenced which measures I/Es considered for grading, these analyses helped to determine criterion measures.

In this paper, only measures that are either listed in the PTS, were used by the instructors for grading, or showed an effect of motion are discussed. See Ref. 7 for a full report on all the analyses. For each measure, the statistical power was determined (i.e., the smallest effect that could be detected given the idiosyncratic variability between crews with a probability of .80). The power of the experiment was found to be sufficient to capture any operationally relevant effects.

<u>Relationship Between Objective Measures and I/E</u> <u>Grades</u>

Linear and logistic regression analyses on the relationship between the grades and the objective measures were used to infer the I/Es' grading criteria and whether the platform motion had an affect on these criteria. Although the logistic regression was considered to be more appropriate for cases involving ordinal data (like the grading system used here), the results of both regression analyses were quite similar. The regression models obtained were not meant to model I/E's decision process in determining the grades, which is actually very complex. They were only used to examine whether any available measures contributed to the I/E's grading criteria.

For RTOs, regardless of whether the platform motion was on or off, the measures of lateral and heading deviations played an important role in predicting I/E grades. For V_1 cuts, the results of the regression analyses suggest that the platform motion status may affect grading. In both motion-on and motion-off conditions, lateral measures seemed to affect I/E grades. However, the level of importance of other types of measures in the I/Es' grading criteria depended on the status of the platform motion. Notably, longitudinal measures appeared to matter mainly when the platform motion was on.

Given that I/Es may have used different grading criteria dependent on motion status, the effect of motion on grades before Transfer testing may have been masked. This appears to be a possibility at least for V_1 cuts, where the No-Motion pilots would have been able to get away with worse performance on longitudinal measures. Later findings from the objective data analysis, however, showed that the differences in the longitudinal performance between the two groups were negligible. Moreover, the regression models obtained accounted for only a small portion of the variance in the grades. These findings render the possibility that differences between the grades assigned to the two groups were masked unlikely.

First Look Evaluation, RTOs

As shown in Fig. 2,[&] the presence of motion significantly improved yaw performance of the pilots (indicated by Integrated Yaw Activity, which is the integral of the absolute yaw rate for 15 seconds after engine failure). No effects of motion, however, were found on any other performance or workload measures, including performance in heading and lateral deviations (Fig. 2), which strongly related to I/E grades. This indicates that the presence of motion did not affect First Look evaluation of RTOs in any operationally relevant manner.

First Look Evaluation, V1 Cuts

No statistically significant differences for either performance or workload measures were found between groups as a function of motion for First Look evaluation of V₁ cuts, although the Motion group was found to control pitch angle marginally more steadily than the No-Motion group (p < .1) (Fig. 3). Physically, however, this difference was less than one degree in average STD. Moreover, this slight advantage in pitch angle control was not accompanied by improvements in any of the other longitudinal performance measures. This, together with the fact that there was practically no simple correlation between STD Pitch Angle of Motion pilots and grades (r^2 =.01), and even the stepwise regression model selecting three more longitudinal measures accounts for no more than 30 percent of the variance in the grades, suggests that the platform motion would not affect what grades PFs achieve

[&] In this and subsequent figures, numbers next to data points refer to sample size.

during First Look evaluation. This result also validates the subjective grade results presented earlier.









Training Transfer, RTOs

Training Transfer was tested for all crews on the simulator with motion activated as a stand-in for the airplane. Despite the fact that the Motion crews were trained and tested on the same simulator configuration, they did not do any better than the No-Motion crews with any RTO performance and workload measure. Additionally, the power of the experiment was generally higher after training, and still no effects of prior motion were found. One *caveat* is that for heading control, although there was no difference between the two groups, more No-Motion crews improved than Motion crews between the last training and the Transfer testing (Fig. 4). This may indicate an effect of adding motion, although during Transfer testing the two groups performed at the same level (as just described).



Fig. 4 RTO Last Training vs. Transfer: Directional Control Performance

Training Transfer, V₁ Cuts

In terms of performance, the most notable differences between the two groups were on Integrated Airspeed Exceedance (the integral of the absolute airspeed deviation outside the (0,+5 knots) band from the recommended V₂) and STD Pitch Angle. The Motion group controlled airspeed better (p=.006) at the expense of increased STD Pitch Angle (p=.025) (Fig. 5). Physically this can be interpreted as the Motion group controlling airspeed more successfully by adjusting pitch angle more aggressively than the No-

Motion group. Note that speed control is critical in V₁ cuts, because it involves safety (e.g. for clearing obstacle and maintaining a margin above stall speed). The Motion group also displayed higher Integrated Yaw Activity compared to the No-Motion group (p=.024) (Fig. 6). However, this did not appear to result in any differences in heading control or other directional performance measures. No other statistically significant performance differences were found.



Fig. 5 V1 Cut Transfer: Longitudinal Performance

With regard to workload during V_1 cuts, the Motion group had fewer wheel reversals than the No-Motion group (p=.059), whereas the No-Motion group had fewer pedal reversals than the Motion group (p=.008) (Fig. 7). The increased number of Wheel Reversals of the No-Motion group was not accompanied by any lateral performance differences. The increased number of pedal reversals of the Motion group, however, was accompanied by an increase in Integrated Yaw Activity, as was discussed earlier. The difference was not apparent at First Look, nor did a combined Analysis of Variance (ANOVA) of Motion/No-Motion by First Look vs. Transfer find a significant interaction, probably due to the variability in number of pedal reversals for the Motion group during First Look. The questionnaire data indicated that the Motion group felt the pedal was less like the airplane than the No-Motion group did.

Although a few statistically significant differences between the groups trained with and

without motion were found during V_1 cut Transfer testing, the size of these differences on average were only about 1.5 knots exceedance per second for airspeed, half a degree RMS for pitch angle deviation, and half a degree per second for yaw rate. Such differences are very small compared to about 110 knots desired nominal airspeed and about 10 degrees nominal pitch angle during climb, and may be considered operationally irrelevant.



Fig. 6 V1 Cut Transfer: Directional Performance

Training Progress, RTOs

No statistically significant differences in improvement from first to last training trial were found between groups for any of the measures (all p>.2). This suggests that the platform motion did not affect the training progress of the pilots.

Also, the overall number of crews (Motion and No-Motion) improving in lateral performance and workload measures was significant for most measures, with the exception of Integrated Yaw Activity with no overall improvement and pedal reversals, which actually increased after training. When looking at the groups separately for these two measures, neither of the groups shows any improvement or deterioration. This confirms that the pilots generally did improve during training regardless of the motion status of the simulator.



Fig. 7 V₁ Cut Transfer: Wheel and Pedal Reversals

Training Progress, V₁ Cuts

The course of training for V₁ cuts reflected the Transfer results. For longitudinal control during V₁ cuts, motion improved Training progress for speed control (Integrated Airspeed Exceedance), but at the cost of pitch angle control (STD Pitch Angle) (Fig. 8). Progress in directional control (i.e., RMS Heading Deviation, Integrated Heading Exceedance, and Maximum Heading Deviation) was also negatively affected by the presence of motion during Training (p<.1). The Training progress on lateral control was not affected by the presence or absence of motion. Also, there was no difference for workload between the two motion groups.

The data indicate that the No-Motion group improved on more measures than the Motion group. While Motion crews improved in Integrated Airspeed Exceedance and STD Column Position only, the No-Motion crews improved in Integrated Bank Angle Exceedance, Heading Deviation, Time to Reach 400 ft Altitude, and STD Pitch Angle. During Transfer, however, the No-Motion group surpassed the Motion group only with steadier pitch angle and yaw activity; and the actual size of these differences was very small.

The above discussion indicates that the training without motion was at least as effective as the training with motion, and the earlier results on Transfer show that although some differences were found in

training progress between the two groups, they did not translate into operationally relevant differences during Transfer.



Fig. 8 V₁ Cut First vs. Last Training: Longitudinal Performance

QUESTIONNAIRE DATA

Each of the PFs and PNFs was given two questionnaires (i.e., one after Training and one after Transfer) that each had six questions (i.e., control precision, workload, gaining proficiency, simulator comfort and acceptability). Each I/E was also given two questionnaires, each with five questions (i.e., the same questions as above, but without acceptability). PFs responded always with reference to themselves. PNFs and I/Es referred to the PFs, with the exception of comfort and, for the PNF, acceptability.

Despite all of these questions, only four differences were found between the Motion and No-Motion crews. 1) After Training, the PNFs from the No-Motion crews rated the control precision of the PFs better than the PNFs from the Motion crews did. 2) The PFs from the No-Motion crews, once transferred to the simulator with motion, rated their control precision higher than their motion-trained counterparts. This is possibly because of the contrast between the added motion and the lack of motion they had been experiencing. 3) In contrast, after Transfer, the I/Es gave higher ratings for performance to the PFs from the Motion group than to the PFs from the No-Motion group. 4) Looking across both questionnaires, the PFs from the No-Motion crews gave better ratings to the simulator for training ("gaining proficiency") than the PFs from the Motion crews.

All together the subjective responses of the pilots and the I/Es did not indicate that the motion used in this study had any impact on the PFs' performance. It also had very minimal impact on the pilots' perception of their own performance, workload, ability to gain proficiency, comfort, or their acceptability of the simulator.

CONCLUSIONS AND RECOMMENDATIONS

The results of this study indicate that the motion provided by the test simulator, which may or may not be typical of other FAA qualified Level C flight simulators, does not, in an operationally significant way for the tasks tested, affect either First Look evaluation, Training progress, or Transfer of training acquired in the simulator with or without motion to the simulator with motion. It also doesn't consistently affect the PFs', PNFs', and I/Es' subjective perception of the PFs' performance, workload, and training, or of their own comfort in the simulator. Neither does it affect the acceptability of the simulator to the PF.

Two *caveats* have to be kept in mind, however. First, the simulator used in this study may not have provided sufficient motion stimulation to be effective. The measurements indicate that the simulator may have failed to provide lateral acceleration cuing representative of the aircraft for the test maneuvers (RTO and V_1 cut).

A second *caveat* is that the current study used the simulator with motion as a stand-in for the airplane. Although some may believe that this quasi-transfer design needs to be validated, others say that high-level simulators have been validated as a stand-in for the airplane by many years of use of the simulator for total flight training. Also, given that the motion-trained group transferred to the same simulator configuration that they had been trained in, whereas the No-Motion group transferred to a configuration that was new to them (i.e., the motion configuration), the Motion group should have had an advantage. Based on the quasitransfer results, it is unlikely that it would have had a greater advantage transferring to an airplane.

Clearly additional steps must be taken to determine the extent to which it may or may not be appropriate to draw generalizations from these results. These should include a comparison of the objective measures from the motion system used in this experiment with such measures taken from other FAA qualified Level C simulators to determine whether or not the motion used in the present study is representative. This should be followed by an investigation on whether operationally relevant effects of motion would be found with a simulator where the motion is manipulated to assure that it is representative of the airplane for the maneuvers selected. Additional maneuvers that may be diagnostic and a different pilot population should be tested as well. Ideally, some validation of the quasi-transfer design with a real airplane would also be undertaken.

ACKNOWLEDGMENTS

This work was funded by the Office of the Chief Scientist for Human Factors of the Federal Aviation Administration, AAR-100. The FAA Program Manager was Dr. Eleana Edens. The manager of the FAA Advanced Qualification Program Dr. Thomas Longridge identified the need for this work. We thank them for their guidance throughout the project.

The opinions expressed are those of the authors and not necessarily those of the Department of Transportation, the Federal Aviation Administration, or the U.S. Government.

REFERENCES

- Bürki-Cohen, J., Boothe, E.M., Soja, N.N., DiSario, R.D., Go, T., and Longridge, T., "Simulator Fidelity—The Effect of Platform Motion," proceedings of the Royal Aeronautical Society conference on Flight Simulation—The Next Decade, London, May 2000.
- Longridge, T., Ray, P., Boothe, E.M., and Bürki-Cohen, J., "Initiative Towards More Affordable Flight Simulators for U.S. Commuter Airline Training," paper presented at the Royal Aeronautical Society Conference on Training— Lowering the Cost, Maintaining the Fidelity, London, May 1996.
- 3. Transcript[#] of the Joint FAA/Industry Symposium on Level B Airplane Simulator Aeromodel

Validation Requirements, Washington Dulles Airport Hilton, March 13-14, 1996.

- Transcript[#] of the Joint FAA/Industry Symposium on Level B Airplane Simulator Motion Requirements, Washington Dulles Airport Hilton, June 19-20, 1996.
- Bürki-Cohen, J., Soja, N., and Longridge, T., "Simulator Fidelity Requirements: The Case of Platform Motion," paper presented at the International Training and Education Conference and Exhibition, Lausanne, Switzerland, 1998.
- Bürki-Cohen, J., Soja, N., and Longridge, T., "Simulator Platform Motion—The Need Revisited," The International Journal of Aviation Psychology, Vol. 8, No. 3, 1998, pp. 293-317.
- Bürki-Cohen, J., Soja, N.N., Go, T.H., Boothe, E.M., DiSario, R., and Jo, Y.J., "Simulator Fidelity: The Effect of Platform Motion," Report No. DOT/FAA/RD-00/XX, in preparation.
- 8. Gundry, J., "Man and Motion Cues," paper presented at the Third Flight Simulation Symposium, London, April, 1976.
- Federal Aviation Administration, "Airline Transport Pilot and Type Rating Practical Test Standards," FAA-S-8081-5B, U.S. Government Printing Office, Washington, D.C., July 1995.

[#] Available in electronic format from Dr. Thomas Longridge, Advanced Qualification Program Manager, AFS-230, tel. (703) 661-0275